DEUTSCHES ELEKTRONEN-SYNCHROTRON DESY

DESY SR-74/7 May 1974

Ĵ

...

DESY-Bibliothek 16, JULI 1974

Optical Constants from the Far Infrared to the X-Ray Region: Mg, Al, Cu, Ag, Au, Bi, C, and Al₂O₃

by

H.-J. Hagemann, W. Gudat, and C. Kunz

2 HAMBURG 52 · NOTKESTIEG 1



DEUTSCHES ELEKTRONEN-SYNCHROTRON DESY DESY SR-74/7

May 1974

建建学习

PRSY-Bibliothek 16. JULI 1974

Optical Constants from the Far Infrared to the X-Ray Region:

Mg, Al, Cu, Ag, Au, Bi, C, and Al₂O₃ な問題を知ら Anostick

by 🧠

H.-J. Hagemann, W. Gudat, and C. Kunz

2 HAMBURG 5 2 · NOTKESTIEG 1

÷ - DESY SR-74/7 May 1974

.

1

1

1

Optical Constants from the Far Infrared to the X-Ray Region: Mg, Al, Cu, Ag, Au, Bi, C, and Al₂O₃

by

H.-J. Hagemann, W. Gudat, and C. Kunz

-• ŧ_ -1 • •

• <u>:</u> •

2

Optical Constants from the Far Infrared to the X-Ray Region:

Mg, Al, Cu, Ag, Au, Bi, C, and Al₂O₃

H.-J. Hagemann⁺, W. Gudat, and C. Kunz

7

Deutsches Elektronen-Synchrotron DESY, 2 Hamburg 52, W.-Germany

The transmissivity of the light metals Mg and Al, the noble metals Cu, Ag and Au, the semimetal Bi, evaporated Carbon and of Aluminumoxid has been determined in the photon energy range from 13 eV to 150 eV. The experiments were performed using the DESY electron synchrotron as a light source and a special monochromator in combination with a two-beam optical densitometer. The data cover the critical region around 40 eV where ordinary monochromators show weak performance. The results were combined with excisting data in the adjacent energy region. A consistent set of optical constants between 10^{-3} eV and 10^{6} eV was obtained by Kramers-Kronig-analysis. Five different sum rules were applied to each set of data. This is a compilation of optical data on a few standard substances. It was directly stimulated by three technical achievements at the DESY synchrotron radiation⁵⁸ laboratory. We have developed (1) a two beam optical densitometer⁵⁹ which in combination with a fixed-exit-slit grazing incidence monochromator⁶⁰ allowed for an accurate measurement of the transmissivity of thin films between 13 and 150 eV photon energy with one instrument. This energy range covers the critical region from 30 to 50 eV where normal incidence monochromators are low in intensity and ordinary grazing incidence monochromators suffer from the superposition of higher order radiation. We have developed (2) a method to prepare very thin films down to below 100 Å. This was necessary because of the high absorption coefficients in this energy range. And (3) an on-line data processing system⁶¹ with a digitizer and a curve-plotter enabled us to handle measured spectra and spectra taken from the literature in an easy way. Especially the rapid Kramers-Kronig transformation routine^{62,63} was very important for this project.

٩.

With our measurements we were able to close a gap in the spectrum of optical constants (o.c.) in a region where a large number of electrons contribute to the optical behaviour. Interpolations in this region of the spectrum can be misleading. This becomes especially clear from the pioneering paper of Philipp and Ehrenreich⁶⁴ who calculated the optical constants of Al over an extended energy range for the first time using experimental results together with interpolations. Their sum rule check revealed a serious lack of oscillator strength. This was corrected for by a subsequent measurement in the region of the Al 2p transitions¹, 30.

- 2 -

In the wavelength region from the intrared down to the ultraviolet accurate measurements of the normal incidence reflectance can be performed while at even shorter wavelengths due to the rapid decrease of the reflectivity and due to the increasing importance of surface roughness only transmission measurements are feasible.

In order to join optical constants obtained from reflectivity measurements to those obtained from transmission measurements a repeated Kramers-Kroniganalysis has to be applied. It was frequently necessary to join the two regions by a smooth interpolation. We have stated in all cases in the text which manipulations were made. We have attempted to consider all the relevant data found in the literature. Although we have tried to make a careful selection of the data used for our final curve we are aware of the arbitrariness of our choice in several instances.

We are especially worried about the very large peak values of the absorption coefficient of several substances which we obtain from our measurements. The values are higher than those found in the literature in the overlapping regions. We were unable to find any systematic errors in our measurements which could explain this behaviour, especially since most errors as from stray light and from higher order radiation tend to diminish the apparent absorption coefficients. We therefore fitted the final curve to our data in this region and only by doing so we obtained the correct number of electrons from the sum rules.

In the case of gold, however, this set of optical data leads to a normal incidence reflectivity of 26 % at 22.5 eV while it is 16 % according to apparently reliable measurements¹⁰. This is the most serious discrepancy which

- 3 -

shows up in our data and which we cannot explain satisfactorily. Because of the large technical importance of gold as a reflecting coating we have constructed an alternative set of optical constants which fits better to the reflectivity results. Clearly such discrepancies have to be clarified by further experiments.

Even with these remarks of precaution we feel that a set of Kramers-Kronig consistent optical constants could be very useful in several respects. There are the technical applications as for example optical coatings for reflectors in the normal and grazing incidence regions, reflecting polarizers, the use as filter materials and substrates for thin samples. It is generally interesting to see the interpendence of various optical quantities like R, μ , ϵ_1 , ϵ_2 , n, k, $-Im_{\hat{\epsilon}}^{1}$ for real materials. Further we have evaluated several sum rules⁶⁵ with the help of these optical functions because they are a good test of the quality of the data and also because some of them like the sum rules on n-1 and on $\mu(n-1)$ have not yet been tested on realistic optical functions over such a wide energy range. Finally, since the complex dielectric constant contains information on the electronic structure of the materials, the data can serve for a qualitative and quantitative comparison with theories. As for an example noteworthy structures which are not yet explained show up in the spectra of the three noble metals Cu, Ag and Au in the energy range 10 - 40 eV. In this paper we limit ourselves to presenting the optical data.

In the following Section 2 we describe details of the film preparation and the measuring technique. Section 3 gives a general description of the Kramers-Kronig transformation used and finally Section 4 containes in a standarized presentation the origin and the way of composing the data as they were used

- 4 -

in the Kramers-Kronig-analysis. This is followed by the list of references which because of technical reasons is not arranged in the usual order. Then we give a section of tables of the optical functions which will be useful if precise data are needed for secondary calculations. The last table gives a survey on the tests of the sum rules. Finally all optical functions are presented as graphs together with results of measurements. Three figures at the beginning of the figure section deal with the experimental procedure while the last nine figures show the evaluation of the sum rules. In all sections of this paper the order of presentation of the different materials is according to the order given in the title.

- 5 -

2. Experimental method

2.1 Film preparation

Because of the generally large absorption coefficients in the spectral region investigated the film thickness ranged from below 100 Å to 600 Å. The films were prepared by vacuum evaporation from resistance heated boats (Mg, Cu, Ag, Au, Bi) or from an e-gun (A1, C, Al_2O_3). The vacuum during evaporation was around $5 \cdot 10^{-7}$ Torr. The evaporation rate (10 - 50 Å/sec) and the thickness of the sample were controlled by an oscillating quartz monitor and recorded automatically as a function of time. The shutter protecting the sample was opened only after an equilibrium rate was attained.

The quartz oscillator was calibrated with a Tolanski interferometer by evaporating films of thicknesses in the order of ~ 2800 Å. This gives an nominal error of the thickness measurement of ~ 1.5 %. Because of the discrepancies with the results on Au, mentioned already in the introduction, we applied in this case also the weighing method and transmittance measurements in the visible. Within the errors of each method all results were in agreement.

The films were supported by a copper screen with a separation of the holes of 34μ and 75 % transmissivity. The mesh was smeared with a solution of 2.5 % collodium in amylacetate. After drying, the collodion forms a thin continuous substrate. The evaporant was condensed onto this substrate. Afterwards the collodion was dissolved thoroughly. When preparing very thin films or when using materials which tend to oxidize we have protected and supported the films by evaporating a three layered sandwich without breaking the vacuum: the material investigated was covered by 50 Å thick carbon layers on both sides. The efficiency of this protection was proved⁴⁵ with Pr, which is an easily oxidizing material. The measuring method allowed

- 6 -

for a cancellation of the effect of the copper screen and the carbon layers by using a carbon sample of equivalent thickness in the second beam of the two-beam optical densitometer (see below). Further details of the film preparation can be found in Ref. 45.

In the case of Al it was necessary to perform an additional measurement with Al evaporated onto carbon substrates <u>in situ</u> in an ultra-high vacuum system. The pressure was about 10^{-9} Torr during evaporation. In this case the film thickness could not be reliably measured and the absorption coefficient had to be fitted to a general curve at one photon energy.

2.2 Measuring procedure

2

The monochromator used is a complicated instrument which is described in great detail elsewhere⁶⁰. Here we only mention those of its features which are important for the present experiments. The monochromator gives off a light beam in a fixed direction which has a point focus at the fixed exit slit. Higher order radiation is efficiently suppressed over the whole energy range of operation. A thin surface layer of carbon develops on the optical components because of the action of synchrotron light. This proved to be favorable for the suppression of higher order radiation when the instrument was used in the so called "non-parallel mode". A deviation from parallelity of premirror and grating⁶⁰ of 1° was used for photon energies in the range 21 eV - 150 eV and a deviation of 2.7° was used in the range of energies the resolution was in the order of 1:500.

Figure I shows the arrangement of the two beam optical densitometer behind the exit slit of the monochromator. After passing a filter (see below and

- 7 -

Fig. 2a) the beam hits a rotating mirror MI at a grazing angle of 4° . The reflected beam passes through sample 1 and hits the cathode of an open photomultiplier at a grazing angle of 15° . The cathode is coated with a thin layer of KCl which has a high yield in the low energy region of the spectrum. When the mirror is rotated to the open segment the beam is reflected by a fixed mirror M2 and transmits a reference sample 2 (in our application an empty mesh or a mesh covered with a carbon film). The signals of the two detectors D₁ and D₂ are electronically divided. The instrument is described in detail elsewhere.⁵⁹

Figure 2b shows in its bottom part the spectrum with empty sample positions. The central part shows as an example an original spectrum of a VAl₃ alloy film compared with a vanadium film of equivalent vanadium density. The upper part gives the 'reciprocal transmittance' of this VAl₃ film (actually the 'reciprocal transmittance of Al in the VAl₃') as it was corrected for the apparative characteristics (bottom curve). The upper curve has a calibrated linear energy scale. The example is taken from an application of this method to the measurement of alloys.⁴⁵

Figure 2a shows the result of inserting different filters into the primary beam (Fig. 1). The Al filter reduces stray light and higher orders between 36 and 72 eV which results in a reduced apparent transmissivity. Pr is a quite good filter material between 60 eV and 100 eV. Due to its very strong absorption peak setting in above 120 eV, the primary intensity is decreased with this filter by several orders of magnitude. This explains the deviation around 130 eV of the curve measured with filter from that measured without filter. Sb has a high transmissivity at low photon energies. The agreement of the curves with and without the Sb filter is a good indication of low stray-light and low higher-order contributions in this energy region.

- 8 -

3. Kramers-Kronig-analysis

The Kramers-Kronig-relations connect the real and imaginary part of certain complex functions describing the optical behaviour of solids⁶⁴⁻⁶⁶. The relation most useful for evaluating reflectance measurements in the low energy region connects the phase angle $\Theta(\omega_0)$ with an integral over the reflectance $R(\omega)$

$$\Theta(\omega_{0}) = -\frac{\omega_{0}}{\pi} P \int_{0}^{1} d\omega \frac{\ln R(\omega)}{\omega^{2} - \omega_{0}^{2}}$$
(1)

where P denotes the Cauchy principal value of the integral and ω the angular frequency of the radiation. If the polarization and the incident angle of the radiation are known the dielectric functions can be calculated elementarily^{63,67}.

While reflection measurements are used in the infrared visible and near vacuum ultraviolet regions absorption is usually measured from the far vacuum ultraviolet down to the x-ray region. As long as the reflectivity of the samples used is small (more accurately⁶⁸: R << 1, k²<<n²) the absorption coefficient μ can simply be calculated from the transmittance T and the thickness d of the sample by applying:

$$\mu(\omega_{o}) = -\frac{1}{d} \ln T(\omega_{o}) = \frac{2\omega_{o}}{c} k(\omega_{o}), \qquad (2)$$

The real part n of the complex refractive index $\hat{n} = n+ik$ is obtained by the Kramers-Kronig-relation

$$n(\omega_{o}) = 1 + \frac{c}{\pi} P \int_{0}^{\infty} d\omega \frac{\mu(\omega)}{\omega^{2} - \omega_{o}^{2}}$$
(3)

If the transmittance of a thin foil is measured in a region where reflectance is still important, the relation

$$\Theta_{\rm T}(\omega_{\rm o}) = -\frac{\omega_{\rm o}}{\pi} P \int_{0}^{1} d\omega \frac{\ln T(\omega)}{\omega^{2} - \omega_{\rm o}^{2}} + \frac{\omega_{\rm o}}{c} d \qquad (4)$$

holds^{63,69} (the sign convention used here is different from that in Ref. 69. \hat{n} is determined from T and Θ_{T} by the iterative solution of an implicit system of equations^{63,70}:

$$T_{EX} - T(n,k) = 0$$
$$\Theta_{T} - \Theta(n,k) = 0$$

with⁷¹
$$T(n,k) = 16 \cdot \frac{n^2 + k^2}{c^2 + b^2}$$
 (5)
 $\Theta(n,k) = \arctan(\frac{kC+nd}{kb-nC})$ (5)
 $C = e^M \{ ((n+1)^2 + k^2) \cos N + 2k(n+1) \sin N \}$
 $-e^{-M}_{\{((n-1)^2 - k^2) \cos N - 2k(n-1) \sin N \}}$
 $D = -e^M \{ ((n+1)^2 - k^2) \sin N - 2k(n+1) \cos N \}$
 $+e^{-M}_{\{((n-1)^2 - k^2) \sin N + 2k(n-1) \cos N \}}$
 $M = \frac{\omega}{c} \cdot k \cdot d = N = \frac{\omega}{c} \cdot n \cdot d$

 T_{EX} is the experimentally determined transmittance and c the speed of light. The Kramers-Kronig-relations (1), (3) and (4) are value for insulators as well as for metals⁶⁵.

In order to obtain a complete set of optical constants for the entire energy range the following procedures were applied:

If the directly measured absorption coefficient could be matched to μ -values which were available from other experiments in the low energy region, Kramers-Kronig-analysis was performed with the total absorption spectrum (Eq. 3).

• 2

÷

If the infrared, the visible- and near UV-region only measured reflectivities were available, first the Kramers-Kronig-relation Eq. (1) was used with these data, extrapolated to higher energies. Together with the measured absorption in the high energy region a total absorption spectrum was constructed with some interpolations.

If the reflectance is high - as for Au and Ag in the intermediate range between 13 eV and 50 eV - a total transmittance spectrum was constructed and the Kramers-Kronig-relation Eq. 4 was applied. In this case an alternative method was tested which did not make use of Eq. 4. In the first step μ_o and k_o is calculated from the measured transmittance $T_{EX}(Eq. 2)$ neglecting the reflectance⁷². Then n_o was calculated from Eq. 3 and the transmittance $T(n_o,k_o)$ of a thin absorbing and reflecting layer^{71,75} was determined according to Eq. 5. A better approximation of the absorption coefficient is then given by

$$\mu_1 = 2\mu_0 + \frac{1}{d} \ln T(n_0, k_0)$$

This procedure was repeated until T_{EX} and the calculated T(n,k) coincided. In all cases this was achieved with sufficient accuracy by the first corrected μ and the n was determined from it by Eq. 3.

The analysis of the data was carried through by using the interactive online data processing system at DESY⁶¹⁻⁶³ consisting of a PDP 8e as an intelligent terminal with several convenient input-output and storing features connected to an IBM-computer 360/75.

4. Results

In this section the results of our measurements and calculations of the optical constants (o.c.) are given. Figures 3-34 show graphs of the absolute values of the o.c. on a logarithmic energy scale. The o.c. are tabulated in the Tables 1-9. The abbreviations used in the description of the way in which we have composed the data from different sources are as follows:

a (B) "a" type of data given in publication, "B" method (in most cases measuring technique) used to obtain "a"

Especially:

Type of data "a"

	R	reflectance in percent or absolute values
	k	imaginary part of the refractive index
	μ	absorption coefficient, $\mu = \frac{2\omega}{c} k$
	μ/ρ	absorption coefficient divided by the density of the material
	۵	photon attenuation cross section in barn/atom
ê=e	ε ₁ +iε ₂	complex dielectric constant

Method "B"

DrP	Drude parameters of the material in the free electron approxi-
	mation obtained from reflectivity measurements; we have calculated
	μ from the elementary Drude formulas

R reflectivity measurements at near normal incidence

T transmissivity measurements at normal incidence

KrKr published results of Kramers-Kronig-analysis (calculated from reflectance spectra)

 $R(\alpha_i)$ reflectivity measurements at various angles α_i

cp compilation of total attenuation cross sections by J.H. Hubbell⁴. The contributions from compton effect and pair production have been subtracted by a linear extrapolation of the logarithmic plots at the highest energies Ell ellipsometry

EL	characterístic	energy-loss	of	electrons
			<u> </u>	

 $T(\alpha_i, P)$ transmissivity at various angles with polarized light

During the evaluation of the spectra it turned out that for some substances the μ -values calculated from our transmission measurements were somewhat higher (between 5 % and 20 %) compared with previous reliable results in the high energy tail of our present measurements around 130 eV. The source of this error was located as a long-time energy independent shift of the relative detector efficiencies due to frequent floating of the vacuum chamber and short pumping times. This resulted in a constant factor by which the transmittance was measured too low, i.e. an additive constant error for μ . The absolute value X·10⁵ cm⁻¹ of this correction could be determined from former absorption values considered to be reliable in the overlapping energy range between 120 eV and 150 eV. If a correction of this type was applied it is designated in the description of the absorption curves as " μ (T)-X".

Magnesium (Figs. 2-6, Table 1)

a) Construction of µ-spectrum

E(eV) Origin of the data, reference no.

 $10^{-3} - 0.2$ μ(DrP) 15 -12R 39, 40, 15; we applied Kramers-Kronig-analysis with extrapolation obtained from transmittance data -45 μ(T) 14 -154 $\mu(T) - 1.0$ present work, absolute value fitted at 45 eV -530 no experimental data, interpolated segment >530 μ/ρ(T) 41, 42, 43

- 13 -

b) Remarks

The dip in the reflectivity at 7.1 eV is assigned to a nonradiative surface plasmon¹⁵, which can be excited by electromagnetic radiation only at a rough surface. Referring to the method of sample preparation¹⁴ it has to be admitted that the shape and the absolute value of μ between 12 eV and the onset of the L_{2,3}-absorption at 49.5 eV could be influenced by MgO-impurities. If the situation is similar to that with Al in the respective energy range μ could be considerably increased by oxigen impurities. A UHV measurement would be necessary to clarify this point. The absolute value of μ between 50 eV and 160 eV given by Townsend¹³ is low by at least a factor of 3 compared to our results. The expected value of the number of electrons n_{eff} = 12 however is obtained only with the high μ -values measured by us. The few experimental values above 160 eV do not allow statements on possible structure of the spectra in this range.

Aluminum (Figs. 7-10, Table 2)

	a)	Construction	of	µ-spectrum
--	----	--------------	----	------------

E(eV) Origin of the data, reference no.

10 - 3-0.155	μ (DrP)	44
-0.8	-	interpolated according to 44
-2.0	ê (E11)	20 (UHV)
-13.5	∿µ (DrP)	estimated according to 44
-36	$k(R(\alpha_i),T)$	19
-74	u(T)	present work (UHV, see b and section 2.1), absolute values fitted at 74 eV
-150	μ(Τ)	45, experimental procedure similar to
		present work
-300	J (T)	shape from 29 and 30, absolute values
		fitted to 28 (see also Ref. 1)
300	(cp)	

b) Remarks

The reflectivity as calculated by Kramers-Kronig-analysis is in good agreement with the measured normal-incidence reflectivity³¹. The maximum position of $-Im\frac{1}{6}$ at 15.0 eV coincides within 1 % with the measured position of the plasmon energy loss at 14.9 eV as determined from the characteristic energy loss of fast electrons³². In the region of low absorption between the plasma frequency at 15 eV and the onset of the $L_{2,3}$ -absorption at 72.6 eV the transmittance of the Al samples varied with preparation conditions like basepressure and evaporation rate. This was recognized earlier, compare e.g. Ref. 54. We have attributed this variation to Aluminumoxid implanted in the foils during evaporation and therefore remeasured the absorption coefficient in this energy range with Al-films prepared in situ under UHV conditions. The extremely low μ -values obtained this way are consistent with those from Hunter⁴⁶ in the region of overlap. The experimental results of different authors^{1,28-30} are deviating between 73 eV and 150 eV by 8 % at most. The μ -spectrum chosen here⁴⁵ shows the largest differences between peaks and minima. From 200 eV to 500 eV the values may be less accurate which could be responsible for the overestimation of n_{eff} by 0.5 electrons as compared to the theoretical limit of 13.

Copper (Figs. 11-14, Table 3)

a) Construction of the µ-spectrum

E(eV) Origin of the data, reference no.

10 ⁻³ -0.5	$\mu(DrP)$	5
-6.5	k(R,T)	5
-13	k(R,Kr)	12)
	$k(R(\alpha_i))$) interpolated curve, absolute values 11) fitted to Ref. 11
-150	μ(T)-0.8	present work
-450	μ (T)	47, compare also Ref. 9
>450	σ (cp)	

b) Remarks

A reasonable interpolation between existing results (e.g. Ref. 11, 12) from 6.5 eV to 13 eV could be found without running into discrepancies, which in a quite natural way joins the results from reflectance measurements at long wavelengths to those of our absorption measurements at shorter wavelengths. The o.c. for Cu calculated here are no longer in contradiction to electron-loss spectra^{6,55}. The remaining deviations might be due to the difficulties with separating multiple losses in electron energy-loss experiments. There are large deviations from the results of Haensel <u>et al.</u>⁹ in the vicinity of the onset of the M_{2,3}-absorption (73.6 eV) which could be attributed to errors in those measurements induced by the use of Al-filters.

Silver (Figs. 15-18, Table 4)

a) Construction of the µ-spectrum

E(eV)	Origin of the data,	reference no,
10 ⁻³ -0.5	μ(D rP)	5
-3.5	k(R,T)	5
-11	k(R,Kr)	18 (UHV)
-16	-	interpolated segment, interpolation facilitated by results from Ref. 11, 12 and from present work
-110	μ(Τ)-0.7	present work (calculated from Eq. 4,5, compare b).
-300	μ(T)	9
>300	σ(cp)	•

b) Remarks

Up to an energy of 3.5 eV the k-values from Ref. 5 have been taken for the construction of the absorption spectrum. On the basis of the total absorption curve chosen the n-data given in Ref. 5 are not Kramers-Kronig-consistent (see Fig. 17). The peaks of the calculated $-Im_{\hat{\epsilon}}^{1}$ at 19 eV, 27.5 eV, and 35 eV come to lie at higher energies than the corresponding peaks in the energy-loss-spectra as determined in Ref. 6 and 38, whereas the structures in $-Im_{\hat{\epsilon}}^{1}$ from optical data above 40 eV have not been found in energy loss experiments⁶. Because of the high reflectance in the soft x-ray range (16.5 % at 23.5 eV) it is not permissible to determine μ from the simplified Eq. 2, instead the Kramers-Kronig-relation Eq. 4 and the procedures described in the section following Eq. 3 have been applied in this energy range.

Gold (Figs. 19-22, Tables 5, 6)

a) Construction of the µ-spectrum

Е	(\mathbf{eV})	Origin	of	the	data.	reference	ກດ
	<u>v</u> . j		-			reterence	$-\mathbf{u}\mathbf{v}$

10 ⁻³ -0.6	μ (DrP)	5
-2.4	k(R,T)	5
-10.5	k(R,Kr)	18 (UHV)
-20	-	fitted segment, shape from Ref. 10 (reflecti measurements)
-117	μ(T) -1.4	present work (calculated from Eq. 4,5, compare Ag (b))
-300	μ (T)	48
> 300	μ(Τ)	shape up to 500 eV interpolated from Ref. 9,
	σ (cp)	absolute values fitted in such a way that a
		smooth connection at 300 eV and 500 eV is
		achieved

b) Remarks

The remarks on n of silver as given in Ref. 5 apply here as well. For Au the joining of the results from reflection measurements¹⁰ to the transmission resul (present work) was not possible without appreciable arbitrariness between 12 eV

and 40 eV. Au is the element exhibiting the highest reflectance in this energy range in comparison to all other materials investigated here. At 22.5 eV it is 16 % from the direct reflection measurements and 26 % on the basis of a Kramers-Kronig-analysis of the transmission spectrum. Such discrepancies have been found by several experimentalists for a number of substances: Lukirskii et al.¹⁷ obtained the absorption coefficient of Al, Ag and Au from reflection and penetration between 113 Å and 23 Å, the reflectivity results give only 50 - 60 % of the penetration results. Similar deviations have been measured by Parratt⁵⁶ for copper with radiation with a few Angström wavelength, and by Römer⁵⁷ for rhenium and plantinum between 30 eV und 130 eV photon energy. The authors assume that this is caused in part by the lower surface density of evaporated films compared to the density of bulk material. Furthermore due to surface roughness part of the light may not be specularly reflected from the sample. Another possibility is the reduction of the measured reflectance in the vacuum-ultraviolet by impurity atoms adherent to the surface, an effect that was observed by Platzöder and Steinmann³ for gold.

Therefore we give two alternative versions of the o.c. of gold: the first one (Table 5) follows from fitting the adjacent values to our transmission results, the second one (Table 6) from extrapolating the measured reflectance data. The first alternative is leading to the correct value of 79 effectiv electrons, the second one reproduces the energy-loss-spectra^{6,38} more closely.

.

Corresponding discrepancies did not show up so severely with other substances. Also in several cases measured reflectances extending up to 40 eV - 50 eV were not available.

- 18 -

Bismuth (Figs. 23-26, Table 7)

a) Construction of the µ-spectrum

E(eV)	Origin of the data,	reference no.
0.2-0.6	$\hat{\epsilon}(\mathbf{R}(\alpha_{i}))$)	22, 75
-15	$\mu(\mathbf{T}(\alpha_{i},\mathbf{P})))$	49, 22, present work:
	ê(EL,Kr)	interpolated between the
	μ(Τ)	different results
-150	μ(Τ)	present work
-500	μ(Τ)	synthesized curve from Refs. 9, 25
-1000	-	interpolated segment
>1000	σ(cp)	

b) Remarks

The reflectivity as measured by Cardona and Greenaway²⁷ exhibits additional structure when compared to the result of the Kramers-Kronig-analysis, probably because the measurements were made with Bi-single-crystals (Bi is a non-cubic crystal). The absolute value and the slope of the absorption curve as determined from our work joins in a natural way with the low energy data by Hunter <u>et al.²⁴</u> in the vicinity of the onset of the $0_{IV,V}$ -absorption at 24 eV and with the data by Haensel <u>et al.⁹</u> near the 57 eV-peak. The splitting of the dominant peak between 50 eV and 80 eV in our measurements is not as pronounced as in Ref. 29, no splitting was observed, however, in Ref. 26. We feel that our measurements are more accurate than the others in this respect since the two-beam technique is especially accurate in the measurement of relative intensities.

Glassy carbon (Figs. 27-30, Table 8)

a) Construction of the μ -spectrum

E(eV) Origin of the data, reference no.

$10^{-2} - 0.5$	R

21, 50; we applied Kramers-Kronig-analysis with extrapolation obtained from transmittance data

-80 $k(R(\alpha_i))$ 51

-700 μ(T) 52, the absolute values have been reduced by a factor of 0.75 (density correction) to obtain the correct value of 2 effective K-electrons

>700 σ(cp)

b) Remarks

In this case our values have not been used for constructing the universal curve. The results by Carter <u>et al.³⁷</u> for n and k have been obtained from multiangle reflectance measurements with graphite. When comparing values by Klucker⁵³ (not shown here) on graphite (to be averaged over the crystal orientations for this purpose), the results on glassy carbon⁵¹ and our results from amorphous evaporated carbon we come to the conclusion that oscillator strength from the 5 eV ($\pi \rightarrow \pi$ transitions) to the 15 eV ($\sigma \rightarrow \sigma$ transitions) peak in ϵ_2 must be transferred along with the changes of structure. Great care has to be applied in assessing absolute μ -values since the density of carbon samples depends crucially on the conditions of preparation. The values reported here are given on the basis of $\rho = 1.5$ g cm⁻³.

Al_2O_3 (Figs. 31-34, Table 9)

a) Construction of the µ-spectrum

E(eV)	Origin of the data,	reference no.
5.5-10	k(R(a _i))	36, interpolated between 2 experimental points
-20	$k(R(\alpha_i))$	46; shape interpolated by means of our transmission measurements
-150	μ(Τ)-0.6	present work
-500	μ(Ι)	33 (12 measured points)
500	σ (cp)	calculated by superposition of Aluminum- and oxygen-data

b) Remarks

Here the o.c. of evaporated amorphous Al_2O_3 are reported, which are important in estimating errors due to oxydation of Al and Al-alloys. The only results obtained with a continuum light source are those between 15 eV and 180 eV (our measurements and Ref. 1) and <u>more structure of the spectra may be hidden between the few measured points</u>. The overall absolute values however seem to be reasonable since no serious discrepancies between different experimental result have been detected and n_{eff} is exceeding the number of 50 electrons theoretically expected only little. The absorption coefficient in the vicinity of the oxygen k-edge obtained by superposition of Hubbell's data⁴ is probably overestimating the oscillator strength (tested by sum-rules) in this region. This is not the case with the values measured by Fomichev and Parobets³³, but with these values the continuation of μ to higher photon energies is problematic.

5. Sum rules

The optical constants of materials in the region of linear response fulfil various sum rules². Alterelli <u>et al.⁶⁵</u> have given a systematic derivation of these sum rules. We have applied several of them to check on the accuracy and consistency of the o.c. given here:

-

$$B \int_{0}^{\omega_{0}} \omega \varepsilon_{2}(\omega) d\omega = n_{eff}(\omega_{0})$$
(6)

$$\mathbf{c} \cdot \mathbf{B} \int_{0}^{\omega_{0}} \mu(\omega) d\omega = n_{\text{eff}}(\omega_{0})$$
(7)

$$-B \int_{0}^{\omega_{0}} \omega \operatorname{Im}(\hat{\varepsilon}^{-1}(\omega)) d\omega = n_{eff}(\omega_{0})$$
(8)

$$\lim_{\substack{\omega_{0} \to \infty \\ 0}} cB \int_{0}^{\omega_{0}} \mu(\omega) (n(\omega)-1) d\omega = 0$$
(9)

$$\lim_{\omega_{0}\to\infty}\int_{0}^{\omega_{0}} \left(n(\omega)-1\right)d\omega = 0$$
(10)

$$B = \frac{m}{2\pi^2 e^2} \frac{A}{\rho \cdot L}$$

с

vacuum speed of light

 $n_{eff}(\omega_{o})$

effective number of electrons per atom (molecule) contributing to the optical transitions in the frequency range up to ω_0

- m electron rest mass
- e electron charge
- L Avogadro's number

A atomic weight of the substance

ρ density of the substance

The results for n eff as a function of E = $\hbar \omega_0$ as given in Tables 1-9 have been calculated from Eq. 6. Figures 35-42 are showing the values of the integrals as a function of E according to Eqs. 6-8. An evaluation of the results of the numerical integrations (Eqs. 6-8) and a comparison with the theoretically expected number of electrons for the substances investigated is listed in Table 10. Quite generally, the agreement is very good. An example of the behaviour of the integrals Eqs. 9 and 10 is given in Fig. 43 for Ag. The integration of $\mu(n-1)$ (Eq. 9) is approaching zero within the limits of accuracy of the computation proving the correct distribution of n around 1 in the energy region below 10^3 eV. A quantitative test of Eq. 10 could not be achieved because the integration routine used on the computer was not suitable for integrating values very close to zero over a large energy range. This results in the rapid oscillations at the high energy end of Fig. 43. However, the general trend is clearly recognized in Fig. 43. The large deviations from zero of the value of the integral between 10³ and 10⁵ eV are clearly associated with the oscillators in the K-shell. In testing the o.c. of the other materials with Eqs. 9 and 10 we obtained similar results which are not shown.

It can be extracted from Figs. 35-42 that for most of the substances an analysis of partial sum rules with the aim of obtaining the number of the effective electrons from a single atomic inner shell (or subshell) does not make much sense. For most inner electrons, oscillator strength is shifted away from the onset of a particular transition to higher energies, and frequently the contribution of a shell is by far not exhausted at the onset of transitions from the next shell. The x-ray absorption coefficient from the onset of K-transitions should contribute 2 electrons per atom corresponding to the number of electrons, the contribution to the sum rules in this region, however, appears to be low by 30 % on the average (cf. Table 10, for C compare Section 4, "glassy carbon", a). Such a deficiency was noted previously for a number of materials⁷³. This transfer of oscillator strength from more tightly bound to less tightly bound shells can be understood on a qualitative basis.⁷⁴

Acknowledgments

The cooperation of U. Nielsen in extending the on-line computer software to the Kramers-Kronig transformation of absorption and transmission data is gratefully acknowledged. We also wish to thank H. Zeiger for his help in the preparation of the samples. Thanks are due to V. Budde and W. Knaut for skilful drafting the many figures and to K. Koehler, J. Schmidt and D. Stanusch for the excellent photographic work. We thank E. Thumann for her careful typing of the manuscript.

References

- + now at Philips Forschungslaboratorium Aachen, 5100 Aachen, W.-Germany
- 1. V.A. Fomichev, Sov. Phys. Solid State 8, 2312 (1967)
- 2. see e.g. P. Nozières and D. Pines, Phys. Rev. 113, 1254 (1959)
- 3. K. Platzöder and W. Steinmann, J.Opt.Soc.Am. 58, 588 (1968)
- 4. J.H. Hubbell, Atomic Data 3, 241-297 (1971)
- 5. P.B. Johnson and R.W. Christy, Phys. Rev. B 6, 4370 (1972)
- J. Daniels, C. v. Festenberg, H. Raether, and K. Zeppenfeld, in <u>Springer Tracts in Modern Physics, Vol. 54</u>, p. 77 (G. Höhler Ed., Springer Verlag, Berlin, 1970)
- 7. H.P. Myers, L. Wallden, and A. Karlsson, Phil.Mag. 18, 725 (1968)
- W.E. Engeler, M. Garfinkel, J.J. Tiemann, and H. Fritzsche, in <u>Optical Properties and Electronic Structure of Metals and Alloys</u>, p. 189 (F. Abelès Ed., North Holland Publishing Co., Amsterdam, 1966)
- 9. R. Haensel, C. Kunz, T. Sasaki, and B. Sonntag, Appl.Opt. 7, 301 (1968)
- 10. L.R. Canfield, A. Hass, and W.R. Hunter, J. de Physique 25, 124 (1964)
- 11. L.R. Canfield and G.Hass, J.Opt.Soc.Am. 55, 61 (1965)
- 12. H. Ehrenreich and H.R. Philipp, Phys. Rev. 128, 1622 (1962)
- 13. J.R. Townsend, Phys.Rev. 92, 556 (1953)
- 14. H. Kröger and D.H. Tomboulian, Phys. Rev. 130, 152 (1963)
- 15. T.F. Gesell, E.T. Arakawa, M.W. Williams, and N.R. Hamm, Phys.Rev. B 7, 5141 (1973)
- 16. P. Jaeglé and G. Missoni, Compt.Rend. 262, 71 (1966)
- A.P. Lukirskii, E.P. Savinov, O.A. Ershov, and Yu.F. Shepelev, Opt. Spectrosc. <u>16</u>, 168 (1964)
- 18. G.B. Irani, T. Huen, and T. Wooten, J.Opt.Soc.Am. 61, 128 (1971)
- 19. R.W. Ditchburn and G.H.C. Freeman, Proc.Roy.Soc. (London) A 294, 20 (1966)
- 20. A.G. Mathewson and H.P. Myers, Physica Scripta 4, 291 (1971)
- 21. E.A. Taft and H.R. Philipp, Phys.Rev. 121, 1100 (1961)

- 22. P. Zacharias, Opt. Comm. 8, 142 (1973)
- 23. J. Toots and L. Marton, J.Opt.Soc.Am. 59, 1305 (1969)
- 24. W.R. Hunter, D.W. Angel, and R. Tousey, Appl.Opt. 4, 891 (1965)
- 25. P. Jaeglé, G. Missoni, and P. Dhez, Phys.Rev.Lett. 18, 887 (1967)
- 26. P. Dhez and P. Jaeglé, in Proc. Colloque C.N.R.S. Processus électroniques
- et multiples du domain X et X-UV, J. de Physique <u>32-C4</u>, 26 (1971)
- 27. M. Cardona and D.L. Greenaway, Phys.Rev. 133, A 1685 (1964)
- 28. V.A. Fomichev and A.P. Lukirskii, Opt.Spectrosc. 22, 432 (1967)
- 29. C. Gähwiller and F.C. Brown, Phys.Rev. B 2, 1918 (1970)
- 30. R. Haensel, B. Sonntag, C. Kunz, and T. Sasaki, J.Appl.Phys. 40, 3046 (1969)
- 31. H. Ehrenreich, H.R. Philipp, and B. Segall, Phys.Rev. 132, 1918 (1961)
- 32. C. v. Festenberg, Z. Physik 207, 47 (1967)
- 33. V.A. Fomichev and A.S. Parobets, Opt.Spectrosc. 21, 419 (1966)
- 34. G.H.C. Freeman, Brit.J.Appl.Phys. 16, 927 (1965)
- 35. R.P. Madden, L.R. Canfield, and G. Hass, J.Opt.Soc.Am. 53, 620 (1963)
- 36. G. Hass, W.R. Hunter, and R. Tousey, J.Opt.Soc.Am. <u>47</u>, 1070 (1957)
- 37. J.G. Carter, R.H. Huebner, R.N. Hamm, and R.D. Birkhoff, Phys.Rev. <u>137</u>, A 639 (1965)
- 38. M. Schlüter, Z. Physik 250, 87 (1972)
- 39. A. Daudé, M. Priol, and S. Robin, Compt. Rend. 264, Ser. B, 1489 (1967)
- 40. D. Hacman and W. Heitmann, Appl.Opt. 12, 895 (1973)
- 41. E. Bauermann and K. Ulmer, Z. Naturforsch. 12a, 670 (1957)
- 42. R.B. Root jr., Phys.Rev. 113, 826 (1959)
- 43. J.H. McCrary, E.H. Plassmann, J.M. Puckett, A.L. Conner, and G.W. Zimmermann, Phys.Rev. <u>153</u>, 307 (1967)
- 44. H.E. Bennett and J.M. Bennett, in <u>Optical Properties and Electronic Structure</u> of <u>Metals and Alloys</u>, p. 175 (F. Abéles Ed., North Holland Publishing Co., Amsterdam, 1966)

45. H.-J. Hagemann, Diplomarbeit, Universität Hamburg (1974),

H.-J. Hagemann, W. Gudat, and C. Kunz, to be published

- 46. W.R. Hunter, J.Opt.Soc.Am. 54, 15 (1964)
- 47. B. Sonntag, Interner Bericht, DESY-F41/1, Hamburg (1969)
- 48. R. Haensel, K. Radler, B. Sonntag, and C. Kunz, Sol.State Comm. 7, 1495 (1969)
- 49. T. Sasaki and A. Ejiri, in <u>Optical Properties and Electronic Structure</u> of <u>Metals and Alloys</u>, p. 417 (F. Abelès Ed., North-Holland Publishing Co., Amsterdam, 1966)
- 50. Y. Sato, J. Phys. Soc. Japan 24, 489 (1968)
- 51. M.W. Williams and E.T. Arakawa, J.Appl.Phys. 43, 3460 (1972)
- 52. V.A. Fomichev and I.I. Zhukova, Opt. Spectrosc. 24, 147 (1968)
- 53. R. Klucker, Interner Bericht, DESY F41-72/1, Hamburg (1972)
- 54. R.P. Madden, in <u>Physics of Thin Films, Vol. 1</u> p. 123 (G. Hass Ed., Academic Press, New York, 1963)
- 55. M. Creuzburg, Thesis, Universität Hamburg (1966)
- 56. L.G. Parratt, Phys.Rev. 95, 359 (1954)
- 57. J. Römer, Diplomarbeit, Universität Hamburg (1970)
- 58. see e.g. R.P. Godwin, in <u>Springer Tracts in Modern Physics</u>, Vol. 51 (G. Höhler Ed., Springer Verlag, Berlin, 1969)
- 59. W. Gudat, J. Karlau, and C. Kunz, Appl.Opt. <u>13</u> No. 8 (1974)
- 60. H. Dietrich and C. Kunz, Rev.Sci.Instr. 43, 434 (1972)
- 61. U. Nielsen, Interner Bericht, DESY F41-73/4, Hamburg (1973)
- 62. R. Klucker and U. Nielsen, Computer Phys. Comm. 6, 187 (1973)
- 63. H.-J. Hagemann, R. Klucker, and U. Nielsen, Interner Bericht, DESY F41-73/10, Hamburg (1973)
- 64. H.R. Philipp and H. Ehrenreich, J.Appl.Phys. 35, 1416 (1964)

- 65. M. Altarelli, D.L. Dexter, and H.M. Nussenzveig, Phys.Rev. B 6, 4502 (1972)
- 66. see e.g. J.S. Toll, Phys.Rev. 104, 1760 (1956)
- 67. see e.g. M. Born and E. Wolf, <u>Principles of Optics</u> p. 36 (Pergamon Press, London, 1959)
- 68. D.L. Greenaway and G. Harbeke, <u>Optical Properties and Bandstructure of</u> Semiconductors p. 4 (Pergamon Press, London, 1968)
- 69. P.-O. Nilsson, Appl.Opt. 7, 435 (1968)
- 70. F. Abelès and M.L. Thèye, Surface Sci. 5, 325 (1966)
- 71. O.S. Heavens, in <u>Physics of Thin Films, Vol. 2</u> p. 193 (G. Hass and R.E. Thun Eds., Academic Press, New York, 1964)
- 72. Note that the simple minded idea that the transmittance of a film in a region where small reflection and large absorption occurs is always less than the transmittance calculated from $T = exp(-\mu d)$ is not right! This is to be seen e.g. from working out Eq. (2.21) in Ref. 68.
- 73. see e.g. A.H. Compton and S.K. Allison, <u>X-Rays in Theory and Experiment p. 545</u> (D. van Nostrand Co., New York, 1935)
- 74. J.W. Cooper, Phys.Rev. 128, 681 (1962)
- 75. J.N. Hodgson, Proc. Phys. Soc. (London) B 67, 269 (1954)

Figure Captions

- Fig. 1: Grazing incidence beam splitter. A puls (duration 10 msec) of monochromatized radiation is reflected either by the rotating mirror M1 and continues on the path marked "1", or it passes the open segment of the mirror holder, is reflected by the static mirror M2, and continues as beam "2". The beams hit the KCl-coated cathodes of the open photomultiplier D1 and D2 at a grazing angle of 15°. Path "2" serves as the reference channel. The signals of the 2 detectors are electronically divided.
- Fig. 2: a) Transmissivity of Ag: example of inserting different filters into the primary beam (see Fig. 1). The agreement of the curves at low photon energies with and without Sb-filter indicates low stray-light and low higher-order contributions in this region. The Al-filter reduces second order radiation between 36 eV and 72 eV, which simultates higher Ag-transmissivity when measured without filter. Possessing a transmittance window between 60 eV and 120 eV, Pr is an efficient filter material in this region. Above 120 eV, however, it is totally inadaquate as a filter due to a giant absorption peak around 130 eV which reduces the primary intensity by several orders of magnitude. The different segments of the curves can be joined smoothly to give the correct Ag-transmissivity.

b) Bottom part: unprocessed spectrum ("apparative characteristics") without samples in positions 1 and 2 (cf. Fig. 1), central part: raw data of a VA1₃ alloy film (position 2) when compared with a V-film (position 1) of equivalent V optical density. Upper part: This spectrum after correction for the apparative characteristics, plotted with a calibrated linear energy scale. Figs. 3 - 34: Symbols of the optical functions:

Scaling factors:

e.g. "x3": values taken from the graphs for this section have to be multiplied by a factor of three.

If there is a break in the curves without a factor the left respective right scale applies to the adjacent individual sections.

Drafting of the curves:

Full lines: final absorption spectra as they were composed from the different measurements and results from the Kramers-Kroniganalysis. For measurements which have been used for the full line curves see text. For Mg there is an important spectral range where no measurements were available, the solid line is interrupted here, (Fig. 3). Representative additional experimental results are drawn into those graphs which show the optical functions that were measured.

The materials are given in the following order: Mg, Al, Cu, Ag, Au, Bi, C, Al_2O_3 .
Test of the sum rules according to the integrals given in the figures (see also Eqs. 6-10). The lower boundary is 0 while the upper boundary of the integrals corresponds to the photon energy given. N_{eff} is the effective number of electrons/atom or molecule contributing to the respective optical function between these boundaries. The left scale in Fig. 43 is given in units of 10^5 cm⁻¹ while the right scale is given in units of eV.

scaling factors:

e.g. "10 x": This curve section has been enhanced in the graph by a factor of ten.

Table Captions

....

Tables 1 - 9: Numerical values of the optical functions from the Kramers-Kronig-analysis of absorption data, N-EFF according to Eq. 6. Table 6 gives in addition the results of the Kramers-Kronig-analysis of the <u>measured reflectivity</u> of Au which has been extrapolated to higher energies.

Tables 10: Summary of the numerical evaluation of the sum rules according to Eqs. 6 - 8.

OPTICAL CONSTANTS CF MG

,

.

5

-EFF	212	619 619 619 654 654 654 654 719	767 944 944 273 273 267 267 267 2655	588 5115 5511 5512 552 5532 5532 5532 5532	675 683 683 700 700 714 714 714 723 723	739 767 767 767 967 973 973 917 956
ENF DG YLOSS	1.8326-04 2.7256-04 4.5556-04 5.995-04 7.575-04	9.196-04 1.125-03 1.865-03 2.376-03 2.376-03 3.766-03 3.766-03	6. 34 6. 34 6. 34 6. 87 7. 66 6. 87 7. 66 6. 87 7. 66 6. 87 7. 66 7. 63 7. 65 7. 63 7. 63	1. 456-02 2. 796-02 5. 396-02 5. 396-02 7. 329-02 7. 329-02 9. 896-02 1. 416-01 1. 416-01 1. 546-01 1. 646-01	1. 716-01 1. 776-01 1. 776-01 1. 876-01 2. 136-01 2. 136-01 2. 136-01 1. 16 00 1. 16 00 1. 576 00	3. 626 00 2. 246 00 1. 216 00 7. 826 01 5. 356 01 3. 815 01 3. 815 01 1. 426 0100000000000000000000000000000000000
3 EFLECTE	97.354 96.803 95.822 95.415 95.143	94.877 94.877 94.875 93.663 92.583 90.358 82.346	80.103 82,320 92,320 92,332 92,332 95,530 95,634 95,023	93.556 91.556 91.556 80.477 84.947 84.942 78.446 76.563 75.658 75.412	75.658 77.411 80.635 83.149 83.149 83.304 79.320 65.651 31.133	19.073 13.370 7.816 5.134 3.604 3.604 2.417 0.419 0.421 0.421 0.404
ABSCDEFF	4.195 05 4.915 05 5.705 05 5.545 05 7.105 05	7.636 95 7.826 05 7.856 05 7.666 05 7.456 05 7.456 05 6.776 05 5.676 05	5-925 05 7-255 05 1-265 05 1-325 06 1-305 06 1-155 06 1-116 76	1.076 06 1.016 06 9.706 05 9.556 05 9.316 05 9.196 05 9.176 05 9.176 05 9.186 05 9.186 05	9.156 05 9.176 05 9.026 05 8.616 05 7.976 05 7.196 05 5.036 05 3.156 05 3.156 05 1.956 05	1.84E 05 1.77E 05 1.68E 05 1.57E 05 1.39E 05 1.33E 05 1.33E 05 1.28E 05 1.28E 05 1.28E 05 1.201E 05 8.03E 04
×	6.02501 4.88601 3.76501 3.26501 2.88501	2.526 01 2.226 01 1.456 01 1.685 01 1.475 01 1.475 01 1.226 01 9.335 00	8-986 00 1-026 01 1-556 01 1-456 01 7-966 00 5-746 00 3-666 00	2.636 00 2.006 00 1.746 00 1.566 00 1.566 00 1.566 00 1.396 00 1.396 00 1.316 00	1.275 00 1.235 00 1.105 00 1.066 00 9.265-01 6.475-01 4.995-01 2.965-01 1.765-01	1.58E-01 1.455-01 1.27E-01 1.115-01 9.16E-02 7.92E-02 5.92E-02 5.92E-02 3.30E-02
z	3.036 01 2.386 01 1.895 01 1.526 01 1.235 01	0.516 7.519 6.069 5.069 5.056 4.194 4.194	8.800 1.12F 01 8.269 4.776 2.977 7.791 7.332 7.91	C.132 C.111 C.1112 C.112 C.121 C.121 C.126 C.197 C.199 C.199 C.199	0.1184 C.1171 C.1155 C.1155 0.115 8.58E-C2 7.17E-O2 6.91E-O2 7.23E-O2 0.11C 0.11C	0.4474 0.4474 0.4477 0.45477 0.4544 0.441 0.441 0.881 0.885
EPSILON2	3. 69E 03 2. 34E 03 1. 42E 03 9. 98E 03 7. 34E 02	4. BCF 02 3. 36F 02 2. 38F 02 2. 38E 02 1. 775 02 1. 775 02 1. 125 02	1. 58F 02 2. 55E 02 2. 56E 02 2. 56E 02 1. 41E 02 1. 76F 01 1. 28F 01 1. 34E 00 1. 34E 00	6. 546-01 3. 566-01 3. 566-01 4. 366-01 4. 366-01 5. 366-01 5. 366-01 5. 366-01 5. 266-01 5. 266-01	4. 68E-01 4. 215-01 3. 68E-01 2. 44E-01 1. 59E-01 3. 94E-02 7. 21E-02 6. 50E-02 1. C3E-01	1. 276-01 1. 396-01 1. 476-01 1. 476-01 1. 476-01 1. 276-01 1. 276-01 1. 176-01 1. 176-01 1. 176-02 7. 816-02 5. 846-02
EPSILINI	- 2, 73E 03 -1, 83E 03 -1, 06E 03 -9, 33E 02 -6, 86F 02	-5,42E 32 -4,36E 52 -3,44E 32 -3,44E 22 -1,96E 02 -1,30E 02 -5,02E 01	-2.703 2.136 01 -1.71E 02 -1.87E 02 -1.56E 02 -6.32E 01 -3.30E 01 -1.136 01	- 6, 854 - 3, 976 - 3, 976 - 3, 689 - 2, 465 - 2, 465 - 2, 465 - 1, 893 - 1, 789 - 1, 686	-1.585 -1.485 -1.485 -1.384 -1.384 -1.385 -1.855 -0.415 -0.2415 -1.555-02 5.535-02	0, 138 0, 207 0, 207 0, 402 0, 472 0, 472 0, 543 0, 543 0, 782 0, 782
ENSP 3Y	7. 70E- 32 1. 50E- 32 1. 50E- 31 2. 50E- 31	4. 505-01 1. 505-01 1. 505-01 1. 505-01 5. 505-01 5. 505-01 5. 505-01	3. 576-01 7. 506-01 7. 776-01 1. 576-01 1. 576-01 1. 576-00 1. 576-00 3. 576-00	5. 73E 30 5. 73E 30 5. 73E 30 5. 73E 30 5. 70E	7.105 00 7.505 00 8.505 00 8.505 00 8.505 00 0.505 00 1.005 01 1.105 01	1. 156 01 1. 736 01 1. 736 01 1. 436 01 1. 506 01 1. 606 01 1. 606 01 2. 406 01 2. 406 01

Table 1, page 1

OPTICAL CONSTANTS OF MG

Ef: ER GY	EPSILONI	EPSILON2	N	к	ABSCOEFF	₹EFLECT%	ENERGYLDSS	N-EFF	
2 (25 01	0 923	4. 5 AF - A2	0-906	2.525-02	6.63E 04	0.261	6.765-02	2.015	
2+0JC //1	0.027	3 635-02	0 000	1 045-02	5.575 04	0.167	4.98F+02	2.038	
2.875	0.853	3. C3E=02	0,020	1.905-02	5 100 04	0.104	4-075-02	2.059	
3.COE 01	C.88Z	3.176-02	0.939	1.690-02	5.125 04	0.100	3 505 63	2 070	
3.20E 01	0.903	2. 92E-02	C+95C	1.545-02	4.98E 04	< C.071	3. 752	2019	
3.498 01	9.919	2.7CE-02	C.959	1.41E-02	4.85E 04	0.049	3 <u>∎ 196</u> -02	Z. 99.9	
3.608.01	0.935	2.225-02	2.967	1.148-02	4.18E 04	0.031	2.535-02	2.117	
3. 63E 01	0,951	1.585-02	0.975	1.026-02	3.91E 04	0.018	2.195-02	2.134	
4.015.01	0.956	1.746-02	0.982	8-84E-03	3.58E 04	0.010	1.875-02	2.149	
4 235 31	0 079	1.455-02	0.985	7.365-03	3.13E 04	0.005	1.525-02	2.163	
4.200 01	0 204	1 375-07	0 007	6 945-03	3 045 04	0.001	1.385-02	2.175	
4 4 12 11	Ge 994	te 3 mm 02	Q4 991		34006 04	U IC /I			
4.60F 11	1.609	1.2CE-02	1.004	5.975-03	2.78E 04	0.001	1.185-02	2.190	
4. 80F 01	1.076	1. G2E-02	1.018	5.025-03	2.445 04	0.008	9.53E-23	2.199	
4.656 01	1.046	1 • 02E=02	1.023	4-965-03	2.44E 04	0.013	9.285-03	2.201	
4 COE 01	1 647	1 025-02	1.032	4.925-03	2.45E 04	0.027	8. 54E-03	2.204	
4.90E /1	1.001	1.025.02	1 0 4 0	4.035-03	2.445 04	1.039	8.765-03	2.205	
4.42E 01	1. 1.81	1.026-02	1+040	4.425700	20402 04	0.004	6. 101 00	. .	
4.54E 01	1.109	2.238-02	1.053	1.06E-02	5.29E 04	0.072	1.80E-02	2.207	
4.56F 01	1.101	7.095-02	1.050	3.385-02	1.70E 05	2,087	5.845-02	2.214	
4 535 01	1.079	8-68F-02	1.040	4.18E-02	2.11E 05	0+080	7.415-02	2.223	
5. COE 01	1.065	9- 6CE-02	1.010	4.17E-02	2.11E 05	0.065	7.605-02	2.232	
5.05E 01	1.045	7.755-02	1.023	3.795-02	1.94E 05	0.049	7+065=02	2.254	
			1 001	3 595-03	1 955 05	0 042	6. 70E-02	2,274	
5.105 01	1+042	7•31E=92	1.021	3.330-02	14075 05	0.046	7 005-02	2.295	
5.15E 🛄	1.039	r.60E-02	1.020	3.725-02	1.94E UD	0.044	7.000-02	7 214	(m. 1. 1.)
5+20E 01	1.037	7.675-02	1.019	3.76E-02	1.985 05	2.044	7.105-02	20210	lable I, page 2
5.25E 01	1.035	7.915-02	1.018	3.89E-02	2.07E 05	0.045	. 335-12	2.334	
5.30E 01	1.033	8. 005-02	1.017	3.935-02	2.11E 05	0.045	7.465-02	2.361	
5.35E 01	1.023	8.268~02	1.015	4.075-02	2.21E 05	0.046	7. 156-02	2.384	
5 436 31	1027	9.14E=02	1.014	4-015-02	2.21E 05	0,045	7.68E=02	2,408	
	1 034	00175 52	1 012	3.00E+02	2.23E 05	0.044	7-635-02	2.431	
0440E 01	1.020	0.00E-02	1.017	10701 C1 A 365-03	2 345 05	0.045	7 775-02	2.455	
5.57E UI	1.027	8+225-02	1.010	1.00 - 72	2.200 00	0.047	7 016-02	2 400	
5.55E 01	1,023	9+34E-CZ	1.012	4.125-12	2.025 00	0.046	1. 715-UZ	2∎ 7 010	
5.60E 01	1.021	8.46F=02	1.011	4-185-02	2.37E 05	0.046	8.06F-02	2.505	
5 705 01	1 018	9.26E-02	1.010	4.09E-02	2.365 05	0.044	7.925-02	2.555	
5 905 31	1 (17	2 245-07	1 709	4.085-02	2.405.15	0.043	7-925-02	7 606	
5407 <u>6</u> 31		3 2 4 5 - 0 2	1.00-	4 105-02	2 455 05	0 043	7-975-02	2.659	
N 992 01	1.015	3.219-02	1.000	4.005.07	2 405 05	0.042	7 845-02	2.711	
5 . ℓ7 <u>5</u> °1	1.015	8.25E-D2	1.008	4+ U95-02	2.498 10	12 + 04-3	1. 302-02	2011	
5.278 01	1.015	8.355-02	1.008	4.145-02	2.60E 05	0.044	8.05E-02	2.821	
5.40E 01	1.014	8.71E-02	1.008	4.32E-C2	2.80E 05	0.049	8.405-02	2.936	
6.63E /1	1-014	9.235-02	1.008	4.585-02	3.06E 05	0.054	8.995-02	3.062	
5.80F 01	1.009	1.015-01	1-005	5.035-02	3.47E 05	0.064	9.865-02	3.204	
T.COE OI	0,996	1.076-01	1.000	5.335-02	3.78E 05	0.071	1.065-01	3,350	
1 232 43	0 001	1 6 15 01	c	5 34 F 64	3 0/F OF	0.071	1 075-01	3, 572	
74 KJE 01	C. 981	L.L4t=01	6.992	2.205-02	3+841 93 3 675 AC	0 0/2	10000000	3 4 7 5	
7•43E 01	G• 970	9• 37E−02	0.986	4.755-02	3.57E 95	0.062	9.885-02	2 0 2	
7.61E 11	0.567	8.155-02	0.984	4.145-02	3.195 05	0.050	8.655-02	5 . 51.4	
7.80E 01	C.971	7.38E-02	C.986	3.74E-02	2.965 05	0.040	7.79E-02	7.940	
4.005 01	A. 973	7.1CE-02	0.987	3.605-02	2.925 05	0.037	7.465-02	4.062	
8-21E 01	<u>6.974</u>	6- 55E- 02	0,988	1-52F-02	2.938 05	0+035	7.295-02	4.184	
A. 4 7F	1. 274	6. H25-02	089	3.45E-02	2.946 D5	0.034	7.165-02	4.377	
8.435 01	A 074	6 645-02		3,345-02	2.975 05	1, 123	6-99F-97	4.410	
9 70F 61	20 71 7		0.007	3.345-07	2 055 AF	0.000	6.035-02	4 401	
na (95 - 81	0.973	0.0112	0.987	5.54E-0Z	2.775 07	2.052		7. 5.52	
8.805 01	0.974	6.59E-02	0.987	3.345-02	2.93E 05	0.032	6 • 92E= 92	4.5.24	
	' •	•						۲	
1 - 1	· · ·								•
	,						•	•	

OPTICAL CONSTANTS OF MG

.

EN ER GY	1EP SL1	EPSILON2	1N	к	ABSCOEFF	₹EFLECT\$	ENEPGYLOSS	N= FF F		
8.SOE 01	2.76E-02	6.656-02	1.336-02	3.375-02	3.045 05	0.033	7.025-12	4.617		
9.00E 01	2.89E-02	6.51E-02	1.40E-02	3.306-02	3.015 05	0.033	6.87F-02	4.673		
9.508 01	3.31E-02	6.CSE-02	1.628-02	3.105-02	2.93E 05	9.031	5.495-02	4.991		
1.00E 02	3.75E-02	5.25E-02	1.85E-02	2.685-02	2.715 05	0.027	5.65F-02	5.297		
1.C5E 02	3.72E-02	4.415-02	1.855-02	2.255-02	2,395 05	0.022	4.755-02	5.547		
1 105 02	2 425-02	3 365, 93	1 715 03	1 010 01	1 165 or	0 017	() ()))	r 330		
	3.105-02		1. FOR 02	1.930-02	20120 02	0.017	4.10F=02	2. 170		
1+100 02	3+190-02	2040CTU2	1.595-02	1.778-02	2+05E 05	0.014	3.715-02	5.995		
1.200 22	3.00E-02	0+200-02	1.046-02	1.005-02	2.015 05	0.013	3 476-72	20.5		
1.205 02	3+ UDE-02	3. CCE-02	1.535-02	1.522-02	1+93E 05	0.012	3.195-02	6.413		
1.39E 02	3.088-02	2. 000-02	L. 54E-02	1.356-02	1+78E 25	0.011	2•83F-02	6.605		
1,35E 02	3.00E+02	2.250-02	1.51E-02	1.16E-02	1.59E 05	0+039	2.43F-02	6.777		
1.40E 02	2 80E-02	1.585-02	1.40E-02	1.005-02	1.425 05	C. 008	2.09F=07	6.932		
1.45E 02	2.58E-02	1.758-02	1.29E-02	8.856-03	1.30E 05	0.006	1 84E-02	7.072		
1.50E 02	2•37E-02	1.615-02	1.196-02	8.16E-03	1.24E 05	0,005	1.695-02	7.274		
1.60E 02	2.17E-02	1.415-02	1.095-02	7 .11 5-03	1.155 05	0.024	1.475-02	7.451		
1.80F 02	1.78E-02	1.056-02	8.52E-03	5.305-03	9.66E 04	0.003	1.095-02	7, 881		
2.COE 02	1.54E-02	9. C8F-03	7.73E-03	4.075-03	8.25F 04	0.002	8.345-03	B. 245		
2.50E 02	1.C4E-02	4.27E-03	5.21E-03	2.15E-03	5.435 04	0.001	4.36F-03	B. 915		
3.00E 02	7.34E-03	2.485-03	3.67E-03	1.255-03	3.78E 34	0.000	2,52E-C3	9.365		
3.50E 02	5.198-03	1.62E±03	2.605-03	8.115-04	2.865 04	0.000	1.635-03	9.619	Table 1, page 3	
4.01E 02	4-58F-03	1.085-03	2.295-03	5.425-04	7,20F 04	0.000	1. COE-03	0.019		
4.50F 02	3.24F-03	7.49F-04	1.62E-03	3.755-04	1.71E 04	0.000	7.535-04	10,131		
5-00E-02	2.61F-03	5 325-04	1.31E-03	2.665-04	1.356.04	0-000	5 356-04	10 282		
5. COF 02	2-03E-03	2.78F-04	1.02E-03	1-395-04	8.45E 03	0.030	2. 79E-04	10.495		
9.00E 02	8. 37E-04	3.83E-05	4.04E-04	4.41E+05	3.56E 13	0.0	8.845-05	10.701		
1.00E 03	2.25F=04	3. 726-05	1.136-04	1-865-05	1 865 03	0.0	7 725-06	10 707		
1.205.03	7 065+05	1.79E+05	3.535+05	8.94E-06	1 045 03	0.0	1 705-05	10 940		
1 256 03	1 105-04	1.425-05	5.50E=05	7.095-06	10055 00	0.0	1 (25-05	10 950		
1 745 73	P 935_06	1.425-05	4 42E+C5	9.155-06	1 075 02	0.0	1 675-05	10.041		
1 335 63	-6 166-06	7 010-05	-7 575-05	1 505-05	2 1/5 01	0.0	2.005-05	10 000		
10000 00	-3-136-03	30012-03	-20000-00	10 00 1-000	2 .14 0 73		2 UD5 - 00	10.973		
1.50E 03	- 7. C2E- 04	9.52F+05	-3.51E-04	4.76E-05	7.22E 03	0.0	9 . 51 E- 05	11.227		
2.COE 03	2.715-04	3.495-25	1.36E-04	1.755-05	3.46E 03	0.0	3.505-05	11+532		
4.COE 03	4.11E-04	2.375-C6	2.065-04	1.195-26	4.70E 02	0.0	2.375-06	12.051		
6.00E 03	2.08E=04	5.50E+07	L.04E-94	2 .75 E-07	1.54E 0?	0.0	5+50E-07	12.118		
8.CQE 03	4,57E-05	1.655-07	2.28E-05	8.27E-08	6+365 01	0.0	1.66E-07	12.146		
1.COE 04	-1.70E-04	6+ 67E-08	+8.49E-05	3.336-08	3.22E 01	0.0	6+67E+08	12.159		
2.COE 04	-1.09E-03	4.C8E-C9	-5.47E-04	2-045-09	4.01E 00	0.0	4.07F-09	12.175		
3.00E 04	-7.18F-04	9.61E+10	-3.59E-04	4.80E-10	1.34E 00	9.0	9.595-10	12.179		
4.00E 04	-3.24E-05	2.7CE-10	-1.625-05	1.358-10	5.26E-01	0.0	2+70E-10	12.180		
5.00E 04	-1.26E-04	1.C8E-10	-6.29E-05	5.385-11	2.67E-01	0.0	1.C3E-10	12.191		

• •

OPTICAL CONSTANTS OF AL

ENERGY	EP ST LONI	EPSILCN2	N	к	ABSCOEFF	REFLECTE	ENERGYLOSS	N-EFF	
1.006-03	-7.27E 04	2.6CE 06	1,126,03	1 165 03	1.175.05	00 977	3 855.47		
5. COE- 03	-4.49E 04	5-116 05	4 B4E 02	5 295 02	2 495 05	770027	2.025=Ur 1.0/€.0/	0.077	
1 • COF- 02	-3.61F 04	2.556 06	3 325 02	2.205 02	2.000 00	99.024	L 94E 96	0.077	
5- COE= 02	-2.516 04	3 545 04	0.575.02	3.825.02	3.88E US	99.484	3+85E-06	9+175	
1.005-01		3 305 00	9.51E 01	1.858 02	9+37E 05	99.121	1.886-05	0.821	
1.005-01	-1.512 04	7+78E 03	3.24E 01	1.19E 02	1.20E 06	99.155	3.34E-05	1.251	
2.COE-01	-3.78E 03	1.CSE 03	8.732	6.20E 01	1.25E 06	99-115	7.065-05	1.527	
3.00E+01	-1.73E 03	3.63E 02	4.311	4.18E 01	1.27E 06	00.020	1 165-04	1 4 3 1	
4.00E-01	-9.74E 02	1.68E 02	2.684	3,136,01	1.275 06	00 071	1 775-04	1:071	
5.00E-01	-6.25E 02	9.76E 01	1.946	2 515 01	1.275 06	00 770	14 122- 14	1.07	
7 . COE- 01	-3.17E 02	4.55E 01	1.274	1.78E 01	1.26E 06	90.110	2.445-04 4.455-04	1.797	
a 605 at							1 1 1	1.0.1.02.0	
A* COE- OT	-1.87E OZ	2.78E 01	1.015	1.37E 01	1.25E 06	97.884	7.01E-04	1.928	
1+COE CO	-1+48E 02	2.32E 01	0.949	1.22 0 1	1.24E 06	97.517	1,03E-03	1.847	
1.10E 00	-1.18E 02	2.C2E 01	0.926	1.09E 01	1.22E 06	96, 987	1.41F-03	1.864	
1.20E 00	-9.37E 01	1.93E 01	0.994	9 73E 00	1.18F 06	95,968	2-125-03	1.981	
1.30E CO	-7.38E 01	2.17E 01	1.250	9.68F 00	1.14F.06	93.779	3_67E-03	1 001	
						234112	JEC 2-0.	1 · · · ·	
1.40E 00	-5.64E OI	2.97E 01	1.916	7.758 00	1.10E 06	88.822	7.31E-03	1.927	
1.50E CO	-5.20E 01	4.38E 01	2.829	7.75E 00	1.18E 06	84.856	9.47E-02	1,970	
1.60E 00	-6.64E 01	4.43E 01	2.588	8 55E OD	1.39E 06	87.959	6-95E-03	2.026	
1.70E 00	-6.53E 01	3.47E 01	2.082	8.34E 00	1.44E 06	89.470	6- 36E-03	2.073	
1.80E CO	-6+03E 01	2.76E 01	1.731	7.96E 00	1.45E 06	90- 261	6.235-07	2.108	
								24 2 9	
2.COE CO	-5.13E 01	1.88E 01	1,292	7.28E 00	1.48E 06	91 .1 35	6.29F-02	2.169	
2.50E 00	-3,45E 01	9+21E CO	0.771	5.91E 00	1.49E 06	91.972	7.175-03	2.201	
3.C9E 60	-2.51E 01	5.68E 00	0.548	5.008 00	1.49E J6	92.165	8.56F-03	2.313	
4.COE CO	-1.38E 01	2.27E 00	0.298	3.70E 00	1.48E 06	92.349	1.16E-02	2.393	Table ', page 1
5.00E CO	-8,328	1.C7E 00	0.183	2.88E 00	1.45E 0o	92.524	1.51E-02	2,425	
7.COE 00	- 3- 709	3. 766-01	0.000	1 225 20	1 7/5 7/				
9.006 00	-1 930	1 (05-01	0.098	1.93E UU	1.305 06	92+047	2.756-02	2.475	
1.105 01	-0.994	10705-1	0+072	1.355.00	1.238.06	90,209	5+91E=02	2.506	
1 205 01	-0.604	1.136-01	0.061	9.46L-C1	1+05E 06	37.960	1.455-91	7,527	
1 20E 01	-0.580	9.298-02	0.061	7.67E-01	9.32E 05	85.832	2+72E-01	2.536	
1,305 UT	-0.347	7. T1E-02	0.065	5.935-01	7.81E 05	82.476	6+136+01	7.544	
1.40E 01	-0.157	6.75E-02	C.C84	4-04F-01	5.73E 05	74,912	2.43E 00	2.551	
1.45E 01	-0.079	6.4CE-02	0.107	3-016-01	4-42E 05	67.549	6.27E C	2 666	
1.50E 01	-0.012	5+66E=02	0.152	1.87E-01	2.84E 05	55.376	1.645 01	2 550	
1.55E 01	0.054	5.015-02	6.252	9.975-02	1.575.05	36.105	0 300 00	7.541	
1.60E 01	0.117	4.43E-02	0.346	4 496-02	1 055 05	24 054		7 • 1 1 L	
			0.040	0,400 02		244.000	2014 (10)	<+ 75#	
1.80E 01	0.317	4.01E-02	0.564	3.555-02	6.48E 04	7.810	3.92F-01	2.575	
2.00E 01	0.453	3.59E-02	0.673	2.675-02	5.41E 04	3.834	1 . 74E - 01	2,586	
3+CDE 01	0.778	2.2CE-02	0.882	1.256-02	3.80E 04	0.398	3. £4E= C2	2. 538	
4.00E 01	0.891	1.636-02	0.944	8.645-03	3.50E 04	0.086	2.05E-02	2 488	
5.CUE 01	0.948	1.14E-02	0.974	5+84E-03	2.96E 04	0.019	1.276-02	2.736	
6. COE - 01	0.004	0 666 00	0 000					_	
6.50E 01	V 0 7 0 %	5. 772-U3	0.49Z	4.51E-03	2+74E 04	0.012	9.25E-C3	2.778	
6.71E 01	1.001	0. JJE-03	1.001	4+27E-03	Z.81E 04	0.000	6.536-03	2.799	
2 COE A1	1.007	8. /UE-03	1.005	4.335-03	2.94E 04	0.001	P.54E-C3	2.807	
0 3 JE UL 2 0 JE 01	1.017	B. 88E-03	1.009	4.405-03	3.08E 04	0.002	8,58E-03	2.817	
THUJE OI	1.023	9.0CE-03	1.012	4•45E=03	3.16E 04	0.004	8.59E-03	2.821	
7.10E 01	1.029	9.14E-03	1.015	4.505-03	3. 245 04	0.034	8. 635-63	2.074	
7.20E 01	1.042	9.41E=03	1.021	44 201-03	3 31C A7	0.011	0 6 C 1 C T 1 3	20025	
7.25E 01	1.053	9, 99F=03	1 021	A 705 03	3 63C 04	0.017	0 9 17 - 11 3 0 9 7 - 1 - 1	2.0 4.47	
7.27E 01	1.063	1.255-00	1 020	7 # F7LTV3 6 045-03	3034C U4 4 470 44	0.0017	0.0155U	2.54	
7.29E 01	1.073	3 615.00	1 031	0.U05-03	4.4/E U4	0.024	1+116=02	2.835	
····	LEVIJ	24016-05	1.030	1.145-02	1.40E 05	n•n39	3.50E-02	2,838	

· · · ·

OPTICAL CONSTANTS OF AL

Table 2.923 2.952 2.981 3.010 3.040 3.501 3.515 3.515 3.517 3.577 3.577 N-EFF 2.843 2.948 2.953 2.957 2.957 3.071 3.104 3.161 3.161 3.180 3.263 3.305 3.350 3.350 3.449 3. 874 3. 870 3. 870 3. 935 3. 935 4. 754 4.106 4.153 4.199 4.243 4.243 4. 334 4. 437 4. 437 4. 537 4. 594 4. 637 4. 690 4. 743 4. 795 4. 849 4. 967 4. 957 5. 011 5. 064 ENERGYLOSS 6. 02F-02 6. 13c-02 6. 41F-02 6. 725-02 7. 02F-02 42 F-02 69E-02 99E-02 31 E-02 8. 785-02 8. 875-02 8. 685-02 8. 135-02 7. 495-72 6. 695-02 6. 126-02 5. 846-02 5. 705-02 5. 695-02 4.72E-02 5.09E-02 5.49E-02 5.83E-02 5.93E-02 5. 77F-02 5. 89E-02 6. 04E-02 6. 14E-02 6. 14E-02 6. 26E-02 6. 26E-02 6. 24E-02 6. 22E-02 6. 18E-02 6. 14E-02 6. 18E-02 6. 13E-02 6. 07E-02 6. 07E-02 6. 03F-02 3.57E-02 4.40E-02 4.46E-02 4.25E-02 4.44E-02 4.39E-02 4.34E-02 4.31E-02 4.30E-02 4.42E-02 · · · · · · · EFLEC T 2 0.031 0.033 0.029 0.029 0.020 0.019 0.019 0.019 0.027 0.025 0.027 0.027 0.040 0.042 0.044 0.046 0.048 0.049 0.049 0.047 0.047 0.042 0.036 0.029 0.033 0.033 0.033 0.030 0.024 0.022 0.021 0.021 0.021 0.023 0.023 0.024 0.024 0.025 0.025 0.025 0.025 0.024 0.024 0.024 0.024 0.024 ABSCOEFF 00000 50000 50000 50000 00000 00000 00000 00200 05 05 05 05 05 05 05 1.77E 1.77E 1.78E 1.80E 1.88E 2.06E 2.23E 2.43E 2.60E 2.60E 2.74E 2.83E 2.995 3.16E 3.345 3.56E 3.72E 3.88E 4.06E 4.22E 1.44E 1.78E 1.80E 1.76E 1.78E 4.30E 4.355 4.245 3.98E 3.68E 3.32E 3.09E 2.98E 2.96E 2.99E 3.07E 3.18E 3.28E 3.28E 3.42E 3.48E 3.51E 3.52E 3.52E 3.54E 3.54E 3.54E 3.59E 3.59E 3.58E 1.965-02 2.385-02 2.405-02 2.405-02 2.405-02 2.495-02 2.40E-02 2.45E-02 2.38E-02 2.38E-02 2.43E-02 2.43E-02 2.505-02 2.695-02 2.895-02 3.065-02 3.125-02 3.156-02 3.215-02 3.355-02 3.515-02 3.515-02 3.666-02 3.86E-02 3.98E-02 4.11E-02 4.26E-02 4.39E-02 4...42E-02 4...42E-02 4...27E-02 3..96E-02 3..63E-02 3.24E-02 2.99E-02 2.86E-02 2.81E-02 2.81E-02 2.81E-02 2.86E-02 2.93E-02 2.99E-02 3.05E-02 3.07E-02 3.09E-02 3.09E-02 3.07E-02 3.06E-02 3.06E-02 3.01E-02 3.03E-02 3.00E-02 2.97E-02 2.94E-02 × 1.030 1.028 1.028 1.025 .015 .015 .014 410.14 410.14 410.14 .012 .011 .007 1.001 0.998 0.994 0.9991 0.989 0.989 0.992 0.992 0.996 0.9995 0.9995 0.9994 0.9944 0.994 0.997 0.997 0.997 0.996 0.993 C.993 0.992 0.992 0.992 z 4. C3E-02 4. 89E-02 4. \$2E-02 4. 81E-02 4. 88E-02 4. 88E-02 4. 97E-02 4. 83E-02 4. 83E-02 4. 94E-02 5. CGE-02 5. 47E-02 5. 88E-02 6. 21E-02 6. 34E-02 6.38E-02 6.51E-02 6.75E-02 7.11E-02 7.43E-02 7.81E-02 8. C5E-02 8. 3CE-02 9.58E-02 9.81E-02 8. 865-02 8. 825-02 8. 495-02 7. 855-02 7. 1855-02 6.41E-02 5.93E-02 5.58E-02 5.58E-02 5.60E-02 5. 69E-02 5. 84E-02 5. 97E-02 6. 07E-02 6. 07E-02 6.16E-02 6.14E-02 6.12E-02 6.08E-02 6.08E-02 6.04E-02 986-02 526-02 556-02 886-02 846-02 EPSILON2 EP SILONI 1.023 1.020 1.016 1.015 0.992 0.993 0.993 0.993 1.032 1.033 1.033 1.033 1.033 1.027 1.027 1.028 1.028 1.027 1.027 1.000 0.985 0.985 0.980 0.980 0.984 0.984 0.988 0.988 0.9997 0.989 0.988 0.9887 0.986 0.985 0.985 0.983 0.983 0.983 1.056 10010 10016 10000 22000 10000 10010 222220 02202 22222 22222 GY 7.31E 7.33E 7.35E 7.43E 7.43E 1.01E 1.02E 1.02E 1.03E 1.04E 7. 67E 7. 77E 7. 87E 7. 97E 8. 07E 8.17E 8.23E 8.33E 8.43E 3.59E 60E 80E 90E 90E 00E 9.13E 9.33E 9.40E 9.50E 1. C5E 1. C7E 1. C7E 1. C9E 1. C9E 9. 67E 9. 70E 9. 87F 3. 57E 1. 00E ENER 16E 17E 18E 19E 20E -----

page 2

2.

DPTICAL CONSTANTS OF AL

ENERGY	1EPSL1	EPSILON2	1N	к	ABSCOEFF	REFLECTS	ENERGYLOSS	NHEFF	
1.22E 02	0.019	5.79E-02	0.009	2.92E-02	3.62E 05	0-024	6.00E-02	5.171	
1.24E 02	0.023	5. 7CE-02	0.011	2.88F-02	3-62E 05	0.024	5.055-02	5 201	
1.26F 02	0.025	5.47E-02	0-012	2.775-02	3 536 05	0.027	5 775 62	2.201	
1.28E 02	0.027	5 155+02	0 012	2 415-02	2 205 05	0.023	5. 13E-02	5.388	
1 305 02	0.027	A 93E-02	0.014		2025 05	2.4922	5.435-02	5+491	
1.305 02	0.020	4.820-02	0.014	2.442-02	3.22E 05	0.020	5. C9E-02	5.589	
1.32E 02	0.028	4.46E-02	0.014	2,265-02	3.03E 05	0.019	4.71F-02	5.681	
1.34E 02	0.027	4•20E-02	C.013	2.13E-02	2.89E 05	0.016	4.43F-02	5.769	
1.36E 32	0.026	4.035-02	0.013	2.045-02	2.82E 05	2.015	4-255-02	5.854	
1.38E 02	0.025	3.895-02	0.012	1-97E-02	2.76F 05	0.014	4. C9E-02	5.034	
1.40E 02	0.024	3.78F-02	0.012	1.91E-02	2.726 05	0.013	3. 96E- 02	6.018	
1.45E 02	0.023	3.575-02	0.012	1 915-02	3 465 A5	0.010	2 2/5 42		
1 506 02	0 023	2 425.01	0.012		2.030 03	0.012	3. 745-02	6.2.7	
1 405 00	0.023	5 455 02	0.011	1.732-02	2.64E US	0.011	3.598-02	5.415	
1.005 02	0.023	3.105-02	0+912	1.605-02	2.60E 05	0.010	3.315-02	5. 306	
1. FOE 02	0+025	2.71E-02	C+012	1.375-02	2.37E 05	0.009	2.85E-02	7.190	
1.8JE 02	0.023	2.2CE-02	0+011	1.115-02	2.03E 05	0.006	2+31E-02	7.409	
1.90E 02	0+022	1.955-02	0.011	9.876-03	1.90E 05	0+005	2.045-02	7.790	
2.008 02	0.018	1.74E-02	0.009	8.765-03	1.786 05	0-004	1-805-02	8-042	
2.20E 02	0.014	1.38E-02	0.007	6.965-03	1.55E 05	0.003	1.425-02	8 554	
2.40E 02	0.013	1.C8F-02	0.007	5-465-03	1.33E 05	0.002	1.115-02	9 077	
2.60E 02	0.015	8.465-03	0.008	A 265-03	1 126 06	0.002	1+110-02	0 777	
		00.000.000	0.000	4.002-03	10120 00	0.002	0. (2579)	A# 345	
2.806 02	0.009	6.585-03	0.004	3.315-03	9.38E 04	0.001	6.70F-03	9-634	
3.COE 02	0.008	5.128-03	0.004	2.57E-03	7.81E 04	0.001	5.205-03	G 879	Table 2 three 2
3.50E 02	C.CO7	3.C7E-03	0.004	1-546-03	5.46E 04	0-000	3-116-03	10 343	Table 2, page 3
4.005 02	0.004	2.025-03	0.002	1-016-03	4.105 04	0 000	2 045-02	10 4 5 4 5	
5.COE 02	0-002	9. 325-04	0.001	A 445-04	7 74 5 04	0.000	2.1.40-00	19.014	
		/ JE 04	0.001	4.000-04	20306 04	0.000	4. 202-04	11.135	
6.00E 02	0+002	4.546-04	0.001	2.27E-04	1.38E 04	0.000	4.56E-C4	11-382	
8.COE 02	0.000	1.508-04	0.000	7.52E-05	6.08E 03	0.0	1.50F+C4	11.636	
1.COE 03	-0.001	6.21E-05	-0.000	3.105-05	3.15E 03	0.0	6-205-05	11 755	
1.50E 03	-0.001	1.435-05	-0.000	7-146-06	1.08E 03	0.0	1 435-05	11 004	
1.55E C3	-0.001	1.29E-05	-0.000	6.435-06	1 015 03	0.0	1 205 05	11+000	
				00170 70	1.010 05	0.0	104405700	7.000 B	
1.60E 03	-0.001	4.64E-05	-0.000	2.325-05	3.91E 03	0.0	4.636-05	11,956	
1.65E 03	-0.000	9.236-05	-0.000	4.62E-05	7.87E 03	0.0	9.235-05	12.037	
1.705 03	-0.000	1.236-04	-0.000	6.13E-05	1.06E 04	0.0	1.235-04	12.116	
2.00E 03	0.000	6,475-05	0.000	3.245-05	6.55E 03	0.0	6-47F-05	12.457	
3.COE 03	-0,002	1.5CE~05	-0.001	7.516-06	2.27E 03	0.000	1.505-05	2.935	
5.008 03	-0.003	2.1CF=06	-0.002	1-056-04	5 305 03	0.000	3 695 67	12 00-	
7.00E 03	-0.005	5.665-07	-0.002	1.075-07	2,500 02	0.000	2.045-06	1.2.48	
9.005.03	-0.000	2 265-07	-0.003	2.975-07	2.116 02	0.010	5.90E-07	13,391	
	-0-000	2.200-07	-0.000	1.126-07	1.02E 02	0+000	2.246-07	13.432	
1 505 04	-0.004	I. USE-UI	-0+00Z	5.141-08	5.72E 01	0.000	1.025-07	13.452	
1400E 14	+0+003	2.935-08	-0-000	1.465-08	2.20E 01	C. 0	2.925-08	13.471	
2.00E 04	-0.001	9.38E-09	-0.001	4.68E-09	9.465.00	0.0	9.35E-C9	13.481	
3.0JE 04	-0.003	2.135-09	-0.002	1.065-09	3.21E 00	0.000	2.11F-00	13 400	
4.COE 04	-0.003	7.545~10	-0.002	3.77-10	1.52E 00	0.000	7.50-10	13 407	
5.00E 04	-0.001	2.99E-1C	-0.001	1.50F-10	7-516-01	0.000	2.005-10	12.775	
6.CJE 34	-0.003	1.62E-10	-0.001	8-095-11	4-855-01	0.000	1 416-10	13 604	
		LUCEL XV		178070-11	48022-01	0000	1.010-(1)	13.444	
8.00E 04	0.001	4.95E-11	0.000	2.47E-11	2.095-01	0.000	4.56E-11	13.494	
1.COE 75	-0.003	1.98E-11	-0.001	9.885-12	1.005-01	0.000	1.975-11	13.495	
1.20E 05	0.002	1.65E-11	0.001	8.245-12	1,005-01	0.000	1.655-11	13.495	

OPTICAL CONSTANTS OF CL

ENERGY	EP SILON1	EPSILON2	N	ĸ	ABSCDEFF	REFLECTS	ENERGYLOSS	N-FFF	
7-00E-03		6.125.05		5 116 02	9 995 04	00 592	2 605-06	0.004	
5-005-03	-1-37E 04	1.5CE 05	2.706.02	2.045.02	1 495 05	770002	2 4 4 9 % - C 0 4 3 5 5 - C (0 01 7	
1. COE= 02	-1.065 04	7.926 04	1 845 07	2 1 1 5 0 2	2 146 46	77+JZJ 00 073	0+200-00	0.030	
6 COE=02	-6.74E 03	1 205 04	4 295 01	1 035 02	2010C 92	99.07	1.245-07		
1 00E-01	-6 365 03	1. DUC 04	0.200 01	1.035 02	2.245 95	98+298	6+175+95	0+141	
1.006-01	-4.246 03	4.25E Q3	2.916 01	7:115 01	7.025 05	98+067	1.215-04	0.310	
5.COE-01	-3.08E 02	6.C4E 01	1.692	1.76E 01	8.83E 05	97.878	6.115-04	0.506	
1.COE 00	-7.18E 01	7.355 00	0.433	8.46E CO	8.555 05	97.650	1.435-03	6.579	
1.50E 00	-2.76E 01	2.73E 00	0.260	5.265 00	7.99F 05	96.439	3. 58F-03	0.557	
1.70E 00	-1.96E 01	1.58E DO	0.223	4.43E 00	7-64E 05	95.778	5.116-03	0.556	
1.75E 00	-1-805-01	1.825 00	0.214	4-24E 00	7-536 05	95,601	5-586-03	0.554	
						,,,,,,,,,			
1.8CE 00	~1,63E_01	1.72F CO	0.213	4.05E 00	7.38E 05	95,212	6.43F-07	0.557	
1.85E 00	-1.48E 01	1.66F 00	0,215	3.865 00	7.235 05	94.720	7.485-03	0.558	
1.90E 00	-1.34E 01	1.575 00	0.214	3.575 00	7.065 05	94.251	8.665-03	0.559	
2.CCE 00	-1.C4E 01	1.76E 00	0.272	3.245.00	6.56E 05	91,016	1.585-02	0.561	
2.10E 00	-7-673	2.635 00	0.468	2.815 00	5.98E 05	R1.350	4.016-02	0 543	
				20011-00	201010	914999	HUCKE VG	N. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9.	
2.20E 00	-6.085	4.3CE 00	0.826	2.60E 00	5.80E 05	67.307	7.74F-02	0.567	
2.30E 00	-5.643	5.38E 00	1.037	2.59E 00	6.04E 05	61.838	8.855-02	0.574	
2.4JE 00	-5.519	5.83E CO	1.121	2,50E 00	6.33E 05	50.232	9.05F-02	0.581	
2.60E 00	-4.938	5.77 <u>5</u> 00	1.152	2.505.00	6.60F 05	57.703	1.005-01	0.597	
2.8CE 00	- 4. 216	5.52E 00	1.169	2.36E 00	6.70E 05	54.535	1.14E-01	P-614	
								·• • • • •	
3,CGE 00	-3.475	5.23E 00	1.184	2.21E 00	6.71E 05	50,910	1.33F-01	C.631	
3.20E 00	-2.757	5.C9E 00	1.232	2.07E 00	6.71E 05	46.759	1.52E-C1	C. 648	
3.40E 00	-2,204	4.56E 00	1.270	1.95E DC	6.73E 05	43.365	1.695-01	0.666	Table 3, page 1
3.60E 00	-1.789	4.5CE 00	1.310	1.875 00	6.83E 05	40.730	1. RCE-01	0.685	
3.80F 00	-1.475	4.82E 00	1.336	1.818 00	6.95E 05	38.700	1.90E-01	0.705	
4. COF 00	-1.146	4.62F 00	1.344	1.72E-00	6.97E 05	36.359	7. C4E= 01	0.725	
4.20E 00	-0.679	4.66E.00	1.419	1.645 00	6.985 05	32.543	2 105-01	0 746	
4.40F 00	-0.467	4 676 00	1 497	1.64E 00	7 305 05	33 807	20101201	0 740	
4. 60E 00	-0.474	5.075.00	1.570	1 675 00	7 705 05	33 661	1 055-01	c 701	
A 805 00	-0 504	5 245 00	1 5 2 3	3 715 00	P 245 05	224771	1.772=91	0.020	
	- 20 200	J 200 90	14933	10/12 00	0.245 02	24+431	1.885-01	1.121	
5.COE 00 1	-1.010	5.23E 00	1.470	1.78E 00	9.02F 05	36.533	1.846-01	0.949	
5.20E 00	-1.334	4.95E 00	1.378	1.80E 00	9.48F 05	37.991	1 - B8F-01	0.876	
5.40E CO	- 1. 550	4.55E CO	1.276	1.78E 00	9.76E 05	38.951	1.975-01	0.903	
5.605 00	-1.611	4,115 00	1.183	1.74E 00	9.85E 05	39-156	2-116-01	n. 979	
5.80E 00	+1.581	3.65E 00	1.102	1.67E 00	9,975 05	38.937	7.795-01	n 052	
					ו••••	50.000		··· • • • • • •	
6.COE 00	-1.464	3.3CE (Q	1.036	1.59E 00	9.69E 05	37.984	2.53E=01	C.974	
6.50E 00	-0.958	2.62E 00	0.958	1.37E 00	9.02E 05	32.883	3, 365-01	1.023	
7.COF 00	-0.497	2.34E NO	C.972	1.20E 0C	8.52E 05	27.063	4.105-01	1.068	
7.50E 00	-0.188	2.2CE 00	1.005	1.095 00	8.32E 05	22.955	4.51E-01	1.113	
8.COE 00	-0.007	2.12E 00	1.029	1.03E 00	8.37E 05	20.576	4.715-01	1.159	
8.50F CO	0.100	2.02F 00	1.029	9.795-01	8.445 05	18.905	4. 95E-01	1,205	
9.00E 00	0.205	1 895 00	1.027	9.215-01	8 415 AS	17 1/2	5 226-01	1 2007	
9 535 00	A 20.5	1 785 60	1.029	9.676-01	0 - 70 C U D 8 36C 05	15 770	20 CC 17 91 5 CC 17 91	1 300	
1 00E 01	0 407	1 7/2 00	1 020	0 10 - 01	0.39E U3	12+409	20 7727 VI 5 577-01	1.248	
1.100 01	0 697	1 430 00	1 076	94101TV1 7 646-01	0.405 05	11 770	9 77 ET VL	1.544	
I.IJE UI	U. 501	1.020 (0	T#014	(•)94E=U1	8.4VE 35	11+112	D. 40E-01	2.458	
1.20E 01	0.656	1.6CE 00	1.091	7.316-01	8.90E 05	11.068	5.36E-01	1.539	
1.30€ 01	0.651	1.578 00	1.084	7.24E-01	9.54E 05	10.907	5.446-01	1.648	
1.40E 01	0.589	1.53E 00	1.055	7.245-01	1.03E 06	11.095	5.70E+01	1.763	
1.45E 01	0.555	1.48E 00	1.034	7.17E-01	1.05E 06	11.084	5.91E-01	1.821	
1.50E 01	0.518	1.435 00	1.009	7.076-01	1.075 06	11.016	6. 29F-01	1.979	

•

ENERGY	EPSILON1	EPSILCN2	N	к	ABSCOEFF	REFLECTS	ENERGYLOSS	N-EFF	
1.55E 01	0.479	1.34E 00	0.981	6.955-01	1-09E-06	10.971	A. 535-01	1 017	
1.60E 01	0.458	1.2 ME 00	0.954	6-735-01	1.095 06	10.451	6. JJC=01	1 957	
1.70E 01	0.449	1.13F 00	0.913	4.205-01	1.07E 06	0 400	7 435 01	1+995	
1.80E 01	0.477	0.000-01	0 990	6 41 5-01		7.099	1+03E+01	2.1 0	
1.006 01	0 623	74 70E-UL	0.000	5-01E-VI	1.026 06	8.409	8-1601	Z.200	
10 306 01	V. 923	3+ 265-01	0.883	5.076-01	9.765 05	7.121	8.32E-01	2.294	
2.COE 01	0.571	8. C2E-01	0.882	4.55E-01	9.22E 05	5.894	8-28E-01	2.383	
2.108 01	0.635	7.36E-01	C+ 897	4-11E-01	8.74E 05	4.764	7. 79E-01	7 448	
2.20E 01	0.695	6.98E-01	0.917	3-81F-01	8.49F 05	3.978	7-196-01	2 5 5 2	
2.30E 01	0.756	6. SCE-01	0.943	3-665-01	8.52E 05	3.502	6 595-01	24 772	
2.40E 01	0.785	7.16E-01	0-961	3-736-01	9.06E 05	3.521	6 34E+01	2.070	
				34136 VI	,	24 221	0.546-01	2+121	
2.50E 01	0.765	7.61E-01	0.960	3•96E-01	1.00E 06	3.963	6.54E-C1	2. 975	
2.60E 01	0.685	7.42E-01	0.921	4.036-01	1.065 06	4.379	T. 27E-01	2.930	
Z.70E 01	0.634	6.76E-01	0.684	3.825-01	1.05E 06	4.329	7.876-01	3.032	
2.80E 01	0.624	5.97E+01	0.862	3.46E+01	9.82E 05	3.864	8.005-01	3.125	
2.90E 01	0.630	5.126-01	0.849	3.025-01	8.88E 05	3.247	7.775-01	3,211	
3.COE 01	0.664	4.48E-01	0.856	2-625-01	7.95E 05	2.540	A. CRE_01	3 207	
3.10F 01	0.711	4.19E-01	0.076	2 305 01	7 516 05	2007	0+ 16L = 01	7.237	
3 20E 01	0.743	3 5 85-01	0 0010	2 370-01	7 345 05	20020	0.10C-01	36 37 8	
3.305 01	1 767	3 65C 01	0.001	2=235701	7.240 01	1.707	D• 695-01	3,479	
3.405.01	0 70/	2+020-01	0.901	2.146-01	7+150 05	1+513	5.235-01	3.497	
3840E 31	00 I 00	24 135-CI	0.910	2.055-01	1-062 05	1.359	4.935-01	3.556	
3.50E 01	0.801	3.64E-01	0.917	1.98E-01	7.048 05	1 . 247	4. 70E-01	3,435	
3.60E 01	0.812	3.555-01	0.922	1.935-01	7.03E 05	1.162	4- 525+ 01	3 705	
3.70E 01	C.820	3-46F-01	0.925	1.875-01	7-02E 05	1.088	4. 375-01	3 774	Table 3 page 3
3.80E 01	0.827	3.34E=01	0-927	1.805-01	6.935 05	1 006	4 105-01	3 0 4	Table 5, page 2
3.90E 01	0.835	3,235-01	0.930	1 745-01	4 945 05	0.000	4 COC 01	3+ 34 4	
		J. 2.32 91		10740-01	9+80E UJ	10 7 32	4.635-11	4.917	
4.CJE 01	0.845	3.12E-01	0.934	1.676-01	6.76E 05	0.854	3.84E-01	3.980	
4 1JE 71	9.854	3+ 028-01	0.938	1.615-01	6.705 05	n.791	3, 695-01	4.048	
4.20E 01	0.862	2. 96E-01	0,942	1.575-01	6.695 05	0.740	3.56F-01	4-115	
4.30E 01	0.869	2+915-01	0.945	1.548-01	6.71E 05	0.701	3.46F-01	4.143	
4.40E 01	9.876	2. E7E-01	0.948	1.515-01	6.74E 05	0.670	3.385-01	4.2-2	
4-50E 01	0-879	2. 825-01	0.845	1 495-01	4 775 05	A 444	2 216 01		
4-60E-01	0.882	2 775-01	04747	1#400-01	0+17E 00	0+044	0.012-91	4.321	
4.70E 01	1 895	2 775-01	0.051	1.405-01	0.00C 00	0+020	5.245-01	4.540	
4.80E 01	0 0 0 0	2 676-01	0.050	1.405.01	0.010 00	0.590	3 # 185~01	4 459	
4000C 01	0.000	24072-01	0.952	1.405-01	6.81E 05	0+575	4.11F-01	4 525	
4. 70E 01	0.088	2.018-01	0.952	I.37E-01	6.80E 05	0.549	3.05F-01	4.599	
5.00E 01	0.890	2.55E-01	0.953	1.345-01	6.775 05	0.524	2.976-01	4.658	
5.10E 01	0.892	2.48E-01	0.953	1.30E-01	6.72E 05	0.438	2.895-01	4.734	
5.20E 01	0.895	2.41E-01	0.954	1.26E-01	6.65E 05	0.469	2.805-01	4.9.4	
5.30E 01	0.898	2.35E-01	0.956	1.235-01	6.61E 05	0.446	2. 73E-01	4.872	
5•40E 01	0.901	2.29E-01	C.957	1.205-01	5.55E 05	0.421	2.655-01	4,939	
5.50E 01	C. 9C 5	2.23F-01	C. 958	1,175-01	6.50E 35	0.309	2 575-01	5 05/	
5.60= 01	0.909	2.185-01	0 940	1 145-01	4 445 05	78397		2.00	
5.70F 01	0.913	2.155-01	0.040	1 105 01	2 X 50 00	11541	2.505mの1	2.073	
5.80E 01	01712	2+132-01	0.902	1.125-01	0.47E U)	0+359	2.445-01	5.139	
5. 6AE A1	0.021	2.12E-U1	0.984	1.105-01	0.415 05	0.347	2.395-01	5,206	
76 7VC 'VI	0.921	2.1CE-01	0.966	1.095-01	6.50E 05	0+335	2.355-01	5.273	
6.COE 01	0.922	2.1CE-01	0.966	1.095-01	6.62E 05	0.335	2.358-01	5.342	
6.10E 01	0.922	2.C8E-01	0.966	1.08E-01	6.67E 05	0+329	2+335+01	5 411	
6.20E 01	0,920	2.C6E-01	0.965	1.075-01	6.71E 05	0.325	2.325-01	5.480	
6.30E 01	0.920	2.015-01	C.965	1.04E-01	6.66E 05	0.313	2.275-01	5 549	
6.40E 01	0.921	1.965-01	C.965	1-025-01	6.60F 05	0.299	2.225-01	5.619	
		· · · -							

• • • • •

				Table 3, page 3		
N-EFF	ນ ໂ ໂ ໂ ໂ ໂ ຈີ່ເຈັ່ງ ອີດີສີ່ຊີ ຍີ່ອີ່ອີ່ຍີ່ ຍີ່ອີ່ອີ່ຍີ່ ເບິ່ງ ເອີ້ຍີ່	1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	5.51 5.51 5.51 5.55 5.55 5.85 5.85 5.55 7.55 5.55 5.55	7,219 7,374 7,574 7,574 7,574 7,574 7,870 8,570 8,515 8,515 8,515 8,515	9,605 11,305 13,375 15,625 16,625 16,625 16,623 17,776 18,429 18,547 18,449 18,449	19,840 20,662 23,084 24,473 24,9473 24,9473 24,948 25,359 25,359 27,4078 27,4078 27,505
ENERGYLOSS	2. 155-01 2. 096-01 2. 055-01 2. 005-01 1. 965-01	1.916-01 1.916-01 1.916-01 1.916-01 1.916-01 1.916-01 1.916-01 1.916-01	1.975-01 1.975-01 1.975-01 2.906-01 1.995-01 1.985-01), 916-91 1, 846-01 1, 746-01 1, 656-01 1, 656-01 1, 536-01 1, 376-01 1, 376-01 1, 316-01	1. 205-01 6. 805-02 3. 416-02 1. 065-02 5. 005-03 5. 065-03 2. 245-03 1. 315-03 1. 315-03 3. 495-04 3. 495-04	1. 71E-C3 1. 65E-03 5. 46E-04 1. 65E-04 1. 89E-04 1. 33E-04 1. 33E-04 1. 33E-04 1. 33E-04 1. 28E-04 8. 12E-07 8. 12E-07 8. 12E-07 8. 89F-09
A EFLECTS	0,283 0,268 0,257 0,257 0,247	0.225 0.225 0.229 0.229 0.229 0.229 0.220 0.220 0.220 0.220 0.220	0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,	0.229 0.197 0.1179 0.1179 0.1179 0.1156 0.1138 0.1138	0,000 0,000000	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
ABSCJEFF	6.525 05 6.645 05 6.425 05 5.395 05 6.355 05	6.34605 6.34605 6.34605 6.347605 6.347605 6.347605 7.05070	7.440E 05 7.53E 05 7.67E 05 7.77E 05 7.77E 05 7.77E 05	イ ・ ・ ・ ・ ・ ・ ・ ・ ・ ・ ・ ・ ・	6.575 05 4.716 05 9.536 05 9.556 05 9.656 05 9.656 05 9.616 04 9.616 04 1.556 05 1.556 05 1.556 05 1.556 05 1.556 05 1.556 05 04 04 04 04 04	8.605 04 9.176 04 7.556 04 7.556 04 7.556 04 7.9586 04 7.9586 03 7.686 03 7.686 03 7.8686 03 7.8686 03 7.8686 03 7.876 02 2.236 01
¥	9.906+02 9.636+02 9.456+02 9.276+02 9.276+02	8,936-02 8,816-02 9,6816-02 8,556-02 8,556-02 8,556-02 8,76-02 8,776-02 9,176-02	9.36E-02 9.46E-02 9.46E-02 9.46E-02 9.34E-02 9.34E-02 9.11E-02	8.775-02 8.345-02 7.885-02 7.445-02 6.935-02 6.535-02 5.955-02 5.955-02 5.995-02	5-406-02 3-106-02 5-136-02 5-136-03 5-516-03 5-516-03 5-516-03 2-63 2-64 2-64 1-746-04	8.515-04 8.235-04 6.245-04 9.496-04 9.496-05 5.626-05 5.386-07 3.656-07 4.0567-07 4.456-07 4.456-07
12	00000 4 11 0 0 0 4 11 0 0 0 4 11 0 0 0 5 11 0 0 5 1	0000 0000 0000 0000 0000 0000 0000 0000 0000	0,021 0,021 0,022 0,022 0,022 0,027 0,027	0,033 0,037 0,037 0,035 0,035 0,033 0,033 0,033 0,032	0.035 0.022 0.022 0.003 0.003 0.003 0.003 0.003 0.000 0.000 0.000	0000 0000 0000 0000 0000 0000 0000 0000 0000
EPSILON2	1,916-01 1,865-01 1,825-01 1,825-01 1,865-01 1,765-01	1. 746-01 1. 716-01 1. 656-01 1. 656-01 1. 677-01 1. 677-01 1. 677-01 1. 716-01 1. 817-01	1, 845-01 1, 845-01 1, 855-01 1, 855-01 1, 855-01 1, 855-01 1, 775-01	1,655-01 1,655-01 1,525-01 1,345-01 1,345-01 1,345-01 1,265-01 1,165-01	1. 345-01 5. 016-02 3. 126-52 4. 676-03 4. 676-03 2. 215-53 1. 305-53 1. 305-53 1. 305-53 5. 266-54 5. 266-54	I. 456-03 I. 656-03 S. 456-03 J. 566-04 I. 686-04 I. 686-05 I. 686-05 B. 126-07 B. 126
1EPSL1	0,077 0,077 0,075 0,077 0,077 0,077 0,077 0,077	00000 0000 0000 0000 000 0000 0000 0000 0000	2,00 2,00 2,00 2,00 2,00 2,00 2,00 2,00	00000000000000000000000000000000000000	0,002 0,007 0,006 0,007 0,006 0,007 0,00000000	0,001 0,001 0,001 0,000 0,000 0,000 0,001 0,001 0,001 0,000 0,001
ENEFOY	8, 53E 01 6, 63E 01 5, 73E 01 6, 83E 01 5, 93E 01	7, COF 01 7, LOE 01 7, 206 01 7, 316 01 7, 406 01 7, 506 01 7, 506 01 7, 706 01	7, 80F 01 7, 90E 01 9, 00F 01 9, 10F 01 1, 10F 01 3, 40F 01 3, 40F 01	R,60E 01 88,87E 01 9,505 01 9,505 01 9,505 01 1,605 02 1,105 02 1,105 02		1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.

•

.

•

5

•

•

÷

OPTICAL CONSTANTS OF AG

EN ER GY	EPSILGNI	EPSILCN2	N	к	ABSCOEFF	REFLECT\$	ENERGYLOSS	N-EFF	
C 005 03	-1 635 66	7 315 05	5 315 02	6-89F 02	3.49E 05	99.720	1.28F-06	G.116	
5.002-03	-1.93E C.			E 045 02	5 135 06	00 660	2 535-04	0.245	
1.005-32	~1.60E 05	3-138 05	3.69E 02	3.00E V2	3013E 0 3	97.077	4 336-06	J 440	
2.5)E-C2	-8.C3E C4	7.54E G4	1.10E Q2	3.065 02	7.54E 05	99.570	6.335-06	24472	
5.CGE-02	-2,84E C4	1.27E 04	3.67E 01	1.73E 02	8.74E 05	99.529	1.315-05	9.617	
1.COE-01	-8.05E 03	1.79E 03	5.536	9.02E 01	9.15E 05	99.519	2.646-05	0.715	
2.CCE-01	-2.086 03	2.6CE 02	2.842	4.57E 01	9.24E 05	99.459	5.92E-05	Q. 756	
3. CCE+ 01	-9,29E 02	8.615 01	1.411	3.05E 01	9.28E 05	99,397	9.895-05	0.775	
4. COE+ 01	-5.23E 02	4 166 01	0.909	2,295,01	9.28E 05	99.311	1.51=-04	0.789	
4 COE 01	-2 255 02	2 455 01	5.665	1,835 01	9.28F 05	99.208	2.17E-04	C. 799	
5+CAE-01			0 3 70	0.035.00	9 126 05	99.654	7. 646-04	0_825	
INCRE CO	-8.15E UI	5.C45 90	Vezfo	9.022 00	7812L VJ	70.007		0.017	
1.50E CC	-3.35E C1	3.14E OC	C.271	5.80E 00	8.81E 05	96.915	2.78E-03	0.844	
2.016.00	-1.74E C1	2.241 00	0.269	4.185 00	8.47E 05	94.352	7.336-03	0.862	
3 616 00	-6 514	1.476 00	0.237	3.09E 00	7.845 05	91.443	1.59E+C2	0.977	
24536 00	- 5 1 24	1 025 00	0 224	2 285 00	4.92E 05	86.455	3. 77E-02	0,891	
Setup Cu	-5.123	1.036 00	0.225	2.202 00	6 1 AE AE	91 437	6 945-07	6 906	
3+25E 00	-3.423	8.53E-C1	0.229	1.895 00	0.145 00		0.000-02	V E 0 *C	
3.53E 60	-1.969	5.996-01	0.211	1.428 00	5.038 05	75,740	1.41E-C1	0.901	
3.6CE 00	-1,219	5.17E-01	0.230	1.13E 00	4.116 05	66.882	3.025-C1	0+902	
3.306.00	-0.497	4.585-01	0.300	7.65F-01	2.875 05	47.199	1.035 00	2.904	
3 375 66	5 110	A 205-01	0 5 2 7	3.005-01	1.526 05	15.374	2.205 00	0.904	
3 110 CU	0.1.10	44202-01	0 7 2 7	2 045-01	1 176 05	5.957	1.176.00	0.905	
3 . 808.00	0+442	4.385-01	6+721	3.045-01	7+1+0 03	160.0	INCREASE AND	UB 70 J	
3.50E CO	1.549	9.35E-C1	1,295	3.60E-01	1,42E 05	4.042	2.E7E-01	0.907	
4.00F (0	7.240	1.54E 00	1.615	5.995-01	2.43E 05	10.261	2.186-01	0.912	
4.1CF 00	2.263	2.525 00	1.729	8-456-01	3.528 05	15.333	2.105-01	0.922	Table 4, page 1
4 214 61	1.947	3 724 00	1.752	1-06E 00	4.52E 05	19.437	2.115-01	0.934	doite 4, page :
4 2 3 E CC	1.700		1 770	1 135 00	4.956.05	20.826	2.156-01	0.948	
4039E (V	10703	5.522 00	1.123	10132 00	44772 33	2	20192 0		
4.5CE (C	1.234	4.33E CC	1.654	1.28E 00	5.83E 05	23,809	2.135-01	0.977	
4.15E CC	C.3C4	4.328 00	1.612	1.34E 00	6.458 05	25.177	2,245-01	1.017	
5.00E 00	C. 564	4.205.00	1,549	1.35E 00	6.87E 05	25.648	2.345-01	1.059	
5 575 67	r. 291	3.666 00	1.444	1.34E.00	7.48E 05	25.695	2.56F-C1	1.142	
	0 1 (6		1 370	1 295 00	7 745 05	24 544	2 925-01	1.224	
0.0.0	301CH	JeHZC VU	1.537	10201 00	1010E 33	140,000			
6.5CE CC	0.183	2.96E CO	1.254	1.18E 00	7.76E 05	22.468	3.375-01	1.302	
7.00E 0.0	0.269	2.4SE 00	1.178	1.065 00	7,50E 05	19.624	3.976-01	1.373	
7. FIF CO	0-475	2. CRE 00	1.142	9-115-01	6.92E 05	15.680	4.575-01	1.437	
3 1 CE CO	C 777	1 365 60	1.160	7.635-01	6.11E 05	11.341	4.77E-01	1.494	
	20111 1 2 4 4	1 455 05	1 224	5 495-41	5 1 7 5 4 5	7.321	3.46E=C1	1.600	
9.000 C.	1.4.4.4.4	1.430 00	1.520	J.U20-01	J.122 JJ	1.391	J. 100 01	1.0.7	
1.COE 01	1.32a	1.63E 00	1.462	5.578-01	5.64E 05	8.214	2.72E-01	1.719	
1.1JE 01	2.080	1.71E 00	1.545	5.535-01	6.168 05	8.879	2,365-01	1.858	
1.23E C1	2.243	1.85E CO	1.608	5 87E-01	7.14E 05	9,994	2,205-01	2,025	
1,205,01	2.329	2.125 00	1.655	6-40E-01	8 435 05	11.240	2.145-01	2.227	
1 416 01	2 346	2 455 60	1 720	7 835-01	1,116,06	14,124	2.116-01	2.494	
1.4400 71	20.742	24636 (0	1.120	leose or					
1.45E C1	1.936	2.68E CC	1.644	8.75E-01	1.29E 06	15.211	2.395-01	2.644	
1.568 01	1.592	2.868 00	1.560	9.18E-01	1.40E 06	15.631	2.67E-01	2.812	
1.63E 01	1.190	2.595.00	1.421	9+10E-01	1.48E 06	15.037	3.19E-C1	3.143	
1.7JE 01	1.022	2.3CE 00	1.330	9.645-01	1.49E 06	13.844	3.635-01	3.457	
1.80E 01	0.993	2.CEE CO	1.281	8.055-01	1.47E C6	12.435	3.936-01	3.753	
	1 4 2 2		1 2 4 4	2 636 63	1 455 04	11 167	4 055-01	6 620	
1.708 01	1.039	1.905 00	1.266	1.52E=01	14455 06	11.10/	70 UJCT V1	4.094	
2.CJE 01	1.154	1.84E CC	1.290	7.14E-01	1.458 06	10.315	5.90E=01	4.325	
2.108 01	1.254	2.C1E 0C	1.346	7.45E-01	1.59E C6	11.146	3.58E-C1	4.639	
2,168 01	1.231	2.19E CO	1.368	8.015-01	1.75E 06	12.443	3.475-C1	4.815	
2.205 01	1.025	2.34E CC	1.338	9.745-01	1,958 06	14.107	3.585-01	5.011	

ч к С •

OPTICAL CUNSTANTS OF AG

EN ER G Y	EPSILGN1	EPSILCN2	N	К	ABSCOSEF	REFLECTS	FNERGYLCSS	N-EFF	
		N 946 AA	1 345	0.265-01	2.136.06	15-727	3,096-01	5.219	
2.25E 01	Geral	Z.Ste St	1+202		2 205 04	16 3 65	4.306-01	5.423	
2.3JE 01	0.491	2.21E 00	1.175	9+43EmUL	2.275 00	14 530	4 735-01	5.616	
2.35E 01	C.355	2.C5E DC	1+104	9.305-01	2.212 96	10.335	- 101-01 - 001-01	5 707	
2.40E 01	0.263	1.EEE CC	1.039	9.045-01	2.205 06	16.444	5.22++01	20191	
2.45E 01	C+223	1.72E 00	C.989	8.685-01	2.15E 06	15.995	5.73E-C1	5.965	
2,50F 01	0+212	1.57E CC	0.547	8.286-01	2.10E C6	15.363	6.275-01	6.123	
3 556 01	0.229	1-42E 00	0.913	7.78E-31	2.01E 06	14,357	6.86 <u>5-01</u>	6.270	
	0 244	1 325 00	6.857	7.346-01	1.94E 06	13.232	7.295-01	6.407	
2.000 UI	0.210	1 335 00	C 89C	6.915-01	1.86E 06	12.110	7.655-01	6.537	
2.65E 01	0.312	1.230 00	0 007	6 505-01	1.786 06	10.948	7,906-01	6.662	
2.73E 01	0.362	1.15E UL	1.00C	0.000-01	18702 30	100710			
2.35E 01	0-416	1.1CE CC	0.851	6.16E-01	1.72E 06	9.877	7 575-01	6.781	
	0.466	1.768 65	0,902	5.90É-01	1.678 06	9.015	7.885-01	6.895	
2.6JE 01	0.50	1 040 00	0.011	5.776-01	1.655.06	9.410	7 785-01	7.016	
2.83E U1	0.000	1.042.00	0.010	5 575-01	1 64E 06	7,971	7.67E-01	7.133	
2.506 01	5.535	L.LZE DU	0.919		1 (60 0/	7 107	7 495-01	7.349	
3.COE 01	0.575	1.C1E C0	0,931	5+415-01	14032 00	7 . 37 1	18478-01		
	0 563	C \$45+01	C. 622	5-348-01	1.69E C6	7,224	7+48F-C1	7.611	
3.1JE CI	0,500	0 715-01	0 021	5-285-01	1.716.06	7.176	7.665-01	7.855	
3.20E 01	0.009	9.115-01	0.000	5 14E-01	1 775 06	7,091	8. C3E-01	8.098	
3.30E 01	0+544	9•25E=31	0.000	34146-01	10125 00	4 992	9 405-01	8. 337	
3.40E 01	0.533	a.6CE≁01	5.875	4.895-01	1.042.00	0.135		a 552	
3.5JE 01	0.541	7.856-01	0.865	4.54E-01	1.015 06	6.C71	6 ¢ ¢ 5 k = 01	70 222	
	0.503	1 256-01	C 876	4.18E-01	1.53E 06	5.149	8.25E-01	8.763	
3.6GE GI	U + 2 9 4	J+32E-JI	0.005	× 035-01	1,505,06	4.067	7.955-01	5,959	
3.70E 01	0.623	7.082-01	0.000	1.000-01	1,000 00	4. 346	7.735-01	9-176	
3.805 01	C+645	6.526-01	C-852	3.85E-UI	14495 00	4 117	7 695-01	C. 384	Table 4, puge 2
3_90E C1	0.659	5.778-01	0.895	3.185-01	1.49E UO	94117 0.00F		0 507	
4.CJE 01	0.467	6.6(5-01	0.856	3.635-01	1,49 <u>5</u> 06	3. 92 3	re prode dia	7. 2 - 2	
		6 075-01	0.967	3.49E-01	1.49E 06	3.567	7.30E-C1	10.007	
4.23E C1	0.582	0.272-01		3 245-01	1 495 04	3, 275	7.106-01	10.421	
4.4JE 01	0.695	6.C(E-01	0.899	34345-01	1 610 06	2 114	7.035-01	10.840	
4.608 01	0.699	5.8CE-01	6.826	3.235-01	1.510 00	20117	7 035-01	11 050	
4.7CE C1	C.697	5.675-01	C.893	3.176-01	1.516 99	3.044	7 025 01	11 360	
4.83E C1	0.693	5.458-01	0.886	3.C9E-01	1.575 06	2 . 95 5	7. UZE-UI	A 1 - 2 0 0	
	A (C)	6 3 6 5 - 01	0.886	3-006-01	1.49F 06	2.824	6.55E-01	11.463	
4.50E CI	0.094	5.3CE-01	0 6 6 6 6	2.90E-01	1.475 06	2.675	6.835-01	11.665	
5.CGE 01	0.545	5.122-01	0.004	1 915-01	1 455 06	2.532	6.67F-01	11.8ć5	
5.10E 01	0.705	4.552-01	356.0	2 365-01	1.445.06	2.61	6.545-01	12.067	
5.20E C1	C.714	4 . 916-01	0.885	2-752-01	1.4CE UD	26431	6 615-01	12.265	
5.30E 01	C.716	4.9CE-C1	0.890	2.756-01	1.48E US	2.405	C. 012-01	124207	
	6 J C A	4 65E-01	0.685	2.745-01	1.5CE 06	2.432	6.58E-C1	12.475	
5.4JE 61	0.718		C 071	2.59E+01	1.47E 06	2.352	6.62E-C1	12.979	
5.60E 01	0.691	4.525-01		2 375-01	1 305 06	2.070	£.27E=C1	13.242	
5.80E 01	0.698	4.115-01	C.868	2.3/5-01	1.350 00	1 013	5 945-01	13.629	
6.COE C1	0.713	3.856-01	0.873	2.215-01	1.345 00	1 (20	5.630-01	12 001	
6.20E 01	0.731	3.71E-01	C.881	2 .11 t=01	I.32E 05	1.035	3 . 325-01	124 771	
6 (AF A1	r. 723	3,716-01	C.885	2.10E-01	1.36E 06	1.596	5.44E-C1	14.362	
G. 40E UL	Uersu e 720	2 225-01	0 983	2.116-01	1.41E 06	1.625	5.49E-C1	14.745	
6.EJE 01	0.753	3./3ETV1	0.000	2.085-01	1.448 04	1.695	5.64E-C1	15.134	
5.60E C1	9.715	3.03L-VI	0.05C	1 076-01	3 405 04	1-681	5-615-01	15.513	
7.CQE C1	0.658	3.3EE-01	6.829	1.915-01		1 501	5 395-01	15.872	
7.20E 01	0.691	3.C8E-01	Q.851	1+815-01	1.320 00	10371	70 396-01	1 10 01 2	
7.4.)E 01	0.700	2.£3E-01	0.853	1.665-01	1.25E C6	1.424	4.57E-01	16.209	
7. 606 01	0.763	2.656-01	C.853	1.586-01	1.21E 06	1.343	4.758-01	16.53	
7.006.01	C_7C)	2.540-01	C.851	1.495-01	1.18E 06	1.297	4.556-01	16.947	
7 + 6UE UI	0 700	2,346-01	C. RAR	1.395-01	1.12E 06	1.229	4.315-01	17.146	
8.CGE 01		20JJC-J1	0.944	1,116-03	9,55E 05	1.056	3.54E-C1	17.816	
8.5JE C1	0.703	1.000-01	V.04C	I O I I C-UI					

OPTICAL CONSTANTS OF AG

EN ER G Y	1EPSL1	EPSILCN2	11	κ	ABSCUEFF	REFLECTS	ENERGYLOSS	N-EFF	
9.CCE C1	C.287	1.4CE-01	0.151	8.24E-02	7.528 05	0.857	2.655-01	18.365	
9.50E 01	0.262	9.72E-02	0.135	5-65-02	5.43E 05	0.650	1,75E-01	18.769	
1.CJE 02	C.234	6.1(E-02	0.124	3-826-02	3.87E 05	0.478	1-136-01	14.564	
1.05E 02	0.209	4.646-12	0.110	2.616-02	2.78F 05	0.359	7.406-02	16.277	
1,115 12	0.166	3 115 02	0.058	1 725-02	1 626 05	0 271	4 405-02	10 470	
		54110-02	04030	10126-02	1076E JJ	Cezil	H. 191792	194454	
1.20E C2	0.143	1.156-02	0.074	6-225-03	7.55E 04	0.150	1.575-02	15.586	
1.30E 02	0.110	6.915-03	3.057	3-666-03	4.83F 04	0.035	9.736-03	19.662	
1.406 02	0.089	6.776-03	0.045	3.545-03	5.03E C4	0.054	6.15E-03	10 775	
1.50E 32	0.073	7. 8 F - C 3	C. C 37	4.076-03	6.19E 04	1.116	9-135-03	10 913	
1.6CF 02	6.062	8.455-03	0.032	A 33E-03	7.105 04	0.026	G. (5E+03	10 377	
		0		40300 02			70 307, 10	± 7∎ 7, 1	
1.73E 32	5.054	5.55E-C3	0.027	4.425-03	7.61E 04	0.020	9.EOE-03	26.041	
1.80E 02	0.044	8.435-03	0.022	4.315-03	7.865 04	0.913	9.22F-03	27.160	
2.CGE C2	G.J.3.a	7.4CE-03	0.018	3.778-03	7.63E 04	0.009	7.55=-03	20.397	
2.208 32	0.020	6.clE-03	0.013	3.455-03	7.70E 04	0.005	7.195-03	25.532	
2.4JE 02	0.021	6.525-03	C.C11	3.50E-03	8.495 04	0.013	7.225-03	20, 374	
-									
2.60E 02	3.015	o.172-03	6.00.8	3.115-03	8.198 04	n , 302	6.36F-C3	21.131	
2.80E 02	0.011	5.37E-03	0.006	2.705-03	7.615 04	n.001	5,50 <u>1</u> -03	21.355	
3.005 02	600 . C	4.635-03	0.004	2.325-03	7.058 04	0.001	4.71F-03	? \ ,Ģ73	
3.50E 02	-0.002	3.565-03	-0.001	1.685-03	5.94E 04	n.uph	3.345-03	12.056	
3.70E 02	-0.014	1.6t6-02	-0.007	3.23E-03	3.095 05	0.003	1.615-02	22 373	
4.CCE 02	0.463	1.76E-02	C + C C 2	8.825-0.	3,565 05	0.002	1.778-02	24 015	
5.CDL 02	0.003	9 .1 08-03	0.102	4.575-03	2.31E 05	0.001	9 <u>,275-0</u> 2	2 R] 4	Table 4, page 3
6.005 02	0.007	5.375-03	0.4000	2.695-03	1.638 35	0.000	5.446-03	10,914	
7.43E 32	5.CC3	2.835-03	0.002	1.425-05	1.065 05	0.000	2.656-03	a a - a - 5	
8.005 02	0.005	2.165-03	0,003	1•03E-03	8.78E 04	0.200	2.185-03	74,170	
1-605 03	0.003	1 545-13	0.025	1 176- 7 .	5 376 24	C 0.30	1 (65-03	34 0.04	
1 616 13	5.002	1 (N 1-00) 7 (A 1-1-1)		3 • 2 30 - 34 1 - 31 5 - 34	1 375 01		1.COF-CS	17.004	
	-0.001	스웨덴포토르토색 - 스토트 - 스토		1.2184-14	よきづつた 一時	1.000	. 425-1,4		
3 605 03		16 9 3 (T V 3 7 - 3 6 T - 6 5		++ (25-00	7•00± vo	0.0.0	90 925 - 7		
2000 13	-0.001	4.750-55	-1.001	2.405-05	5.556 03		4. (34 - 5. 5	· · · · · ·	
3•1.7E 53	- (. 0(2	2.862-00	-0.001	1.435-05	4.312 23	5 C O O	2.4 858-05		
3.50E 03	-0.007	3-442-05	-0.003	1.728-05	6.145-03	0.000	3,400-05	10.4	
3.6)E 03	-0.005		-0.000	3_ 745-05	1.1dE 04	1,100	6-435-75	40-679	
4.CJE 03	-0.007	7.176-05	-0.003	3.576-05	144F 04	0,000	7 . 075 - 05	1.5.3	
9.50E 13	-0.002	4.476-15	-5.001	2 215-05	1.015 04	0.000	4.476-15	1 7 7 4 4	
5 CDE D3	-0.003	3.655-05	-1.001	1.525-05	7.689.03	5 010	4,735-05	47.57-	
						· • · · ·			
6.CCE 03	-C.C.+	1.684-05	-0.002	d.365-06	5.075 03	0.000	1.655-05	47.463	
8.CDE 03	0.050	5.E50-06	0.000	2.925-06	2.365 03	0.0	5.85H-CA	44, 147	
1.CGE 04	0.002	2.570-06	0.001	1.295-06	1.306 03	0.000	2.585-08	45.315	
2.CJE 04	0.302	1.519→07	0.001	9.575-08	1.94E 02	∂ ∎0	1.576-07	40.01	
2.505 04	-0:003	7.265-08	-0,001	3.63E-38	9.216 01	0.000	7.24=-08	46.121	
1 405 54			. ·		<u> </u>				
2.032 04	-6.62	4.220-07	-C.1C1	2.115-07	5.545 02	010	4.205-07	+6•3 1	
3.€UE 94	-0,001	2.645-07	-0 . 000	1.325-07	3.998 02	ט•ר	2.635-07	44.54r	
4.CDE 04	-C.(S5	9.31E+08	-0.003	4.646-08	1.875 02	0)+000	9 . 235-0H	46.907	
5 GJE 54	-3.005	3.865-08	-0,003	1,928-39	9.73E 01	0.000	9.82 <u>2</u> +06	47.l^?	
7.50E 04	-0.003	8.675-09	-0.000	4.33E+09	3.298 01	9 . 0	ε.67 ξ−26	47.3.77	
1.COF 35	0.001	2.576-00	0.171	1 605-30	1 516 01	1.000	3 696-06	67 367	
2.000.05	0.003	2.2610	0 000	1.155-10	1 2 2 2 D //	0.000	2 3 2 5 1 7	- 1+ 30 / 1 / 7 / 7 /	
5,0)8 15		7 626-10	-0.000	7 4 10 5 T 10	2005-01	0 0 20	2 6 75 7 1 % 7 - 65 6 - 1 2	979913 7786A2	
	- 044 03	(***±*±Z	サリーンジュ	2.90071Z	2.096401	2. C ()	★● 평가트폰 높은	1 2 2 5	

.

a i Al get i

OPTICAL CONSTANTS OF AL

•

-

• •

. .

ENERGY	EPSILON1	EPSILÓN2	N	ĸ	ABSCOEFF	REFLECTS	ENERGYLOSS	N-EFF
1-006-03		1.17E 06		7.68E 02	7.78E 04	99.740	8.57E-C7	0 <u>=</u> 0
5 000-03	- 2 805 04	2.776.05	3.458 02	3.79E 02	1.755 05	99.449	4.325-06	0.035
3.000-00	-1 430 04	1 146 05	7 775 02	2 565 02	2.605.05	99.230	8-615-06	0-080
	-1.02E 04	1.146 00	2022L 02	1 345 03	4 14E 05	00 405	4 305-05	0 366
5. COE-02	-1.10E 04	1.000 09	C. JCC U1	1.246 02	0.146 VD	70 00 J		0 530
1.005-01	-5.90E 03	4.47E 03	5.646 OT	BOLE OI	1.80E 05	98. 242	Be rot-Up	0.030
5.COE-01	-3.29E 02	4.74E C1	1.273	1.81E 01	9.08E 05	98.499	4.205-04	0.742
1.COE 00	-7.COE 01	6.278 00	0.375	8.36E 00	8.45E 05	97.894	1.305-03	0.774
1.50E 00	-2.62E 01	4.3CE CO	C.418	5.13E 00	7.80E 05	94.086	6.146-03	C. 800
2.005 00	-1.C7E 01	3.22F CC	0.487	3.31E 00	6.70E 05	85.122	2. 60E-02	0.925
2 2000 00	-6 4 5 1	3.225 00	0.613	2.64E 00	5.88E 05	74.097	6.27F-02	0.835
2.202 00	-0.011	J. 222 00	0.013		J.COL (J)			
2.405 00	-3.265	3.52E 00	C.872	2.01E 00	4.89E 05	53.565	1.53E+C1	C. 848
2.60E CO	-0.548	5.27E CC	1.541	1.71E 00	4,518 05	34.294	1.886-01	0. 366
2.80£ 00	0.041	6.63E 00	1.826	1.81E 00	5.15E 05	35,244	1.516-01	0.693
3. CCE 00	0.127	7.27F 00	1.550	1.865.00	5.678 05	35.943	1.375-01	C. 925
3.15E OC	0.271	7.41E CO	1.960	1.89E 00	6.03E 05	36+428	1.35E-01	C. 952
								0.001
3.3CE 00	C.3C9	7.366 00	1.560	1.88E 00	6.29E 05	36+222	1.368-01	6.581
3.45E CO	0.500	7.22E 00	1.967	1.84E 00	6.42E 05	35.357	1.385-01	1.010
3.60E OC	D . 823	7.32E 00	2.024	1.81E 00	6.60E 05	34.797	1.356-01	1.940
3.80E 00	0.703	7.58E (C	2.039	1 . 868 00	7.16E 05	35.720	1.315-01	1+084
4.CGE CC	0.434	7.52E CO	1.995	1.895 00	7.64E 05	36.251	1.335-01	1+131
A 215 00	C 154	7.28F CC	1.927	1-89E 00	8-03E 05	36,453	1.37F-01	1.179
4,236 03	-0.07-	6 CCE 00	1 949	1.875 00	9 336 05	36.289	1.45E=01	1. 226
4.4UE (U	=0+010		1 707	1.070.00	0.530 05	36 756	1 445-01	1 306
4.755 CO	-0.200	0.USE UU	1 (10	1 (55 00	0.305 05	27.120	1 955-01	1 240 Table 5, page 1
5.COE 00	-0.055	5.425 00	1.038	1.636.00	5.385 02	32+420	1.004-01	1+300
5.5GE CC	0.456	4.66E QQ	1+603	1.455 00	8.10E 05	27.859	2.135+91	1.402
6.CCE 00	0.932	4.2CE 00	1.618	1.30E 00	7.89E 05	24+211	2.275-01	1.560
5.50E 00	1.355	3.97E CC	1.665	1.195 00	7.84E 05	21.837	2.265-01	1.560
7-006-00	1.701	3-52F 00	1.728	1.13E 00	8.04E 05	20.800	2.156-01	1.765
7 625 00	1.864	4.12E 00	1.786	1.15E 00	8.76E 05	21.397	2.025-01	1.991
2.00E 00	1 500	4 71E 00	1.727	1.225 00	9.88E 05	22.560	2-116-01	2.010
8.00E 00	1. 500	4021L CV		1.220 00	J. COL ()	22.000	20112 02	G ♥ - k · /
8.50E CC	1.413	3.85E CC	1.666	1.178 00	1.01E 06	21.309	2.27E-01	2.140
9.00E 00	1.311	3.67E CC	1.614	1.14E 00	1.04E 06	20.572	2.416-01	2.269
9.508.00	1.370	3.39E CO	1.585	1.075 00	1.03E 06	18.976	2.54E-01	2.395
1-015-01	1.343	3,315,00	1.572	1-05E 00	1.07F 06	18.576	2 • 58F- C1	2.524
1.055 01	1.416	3.C6E 00	1.548	9.905-01	1.05E 06	17+126	2.695-01	2.651
				A 155 A)			a (ar ar	
1.10E 01	1+527	2.54E 00	1.326	9.45E-U1	1.050 00	10+188	2.082-01	2.111
1.15E 01	1.617	2.85E 00	1.565	9.205-01	1.07E 06	15+712	2. 64 E-01	2.906
1.20E 01	1.682	2.E7E CC	1.583	9 . C8E⊷01	1.1CE 06	15+523	2.59E-C1	3∎039
1.308 01	1.725	2.86E CC	1.592	8.996-01	1.19E 06	15.401	2.56E-C1	3.322
1.40E 01	1.682	2.93E 00	1.591	9.225-01	1.31E 06	15.850	2.575-01	3.631
1.505 01	1.500	2.88E 00	1.540	9.346-01	1-42F 06	15.899	2.735-01	3.965
1 405 01	1.440	2.7CE 00	1.505	8-985-01	1.46E 06	14.939	2. 86E= C1	4-302
1 205 01	1.547	2.626.00	1.513	8-655-01	1.495 06	14.314	2.845-01	4-646
1 000 01	1 200	2.71E 00	1.545	8-655-01	1.595 04	14-577	2.656-01	5.011
1.80E 01	1 / 0 5	2 CAE 00	1 412	0 60E_01	1000 A4	15 637	2 505-01	5 X33
1.90E 01	1+090	SALCE VU	1.017	4*305=01	1.03E VO	10+251	2. 70C- 01	7 8 4 7 7
2.COE 01	1.374	3.38E CC	1,584	1.07E 00	2.16E 06	18.911	2.545-01	5.933
2.10E 01	0.775	3.64E 00	1.499	1.21E 00	2.58E 06	22.309	2.635-01	6.504
2.15E 01	0.365	3.57E 00	1.406	1.27E 00	2.77E 06	24.009	2.775-01	6.805
2.20E 01	-0.002	3.34E (C	1.292	1.295 00	2.88E 06	25.375	2.99E-01	7.097
2.25E 01	-0.240	3.63E 00	1.183	1.28E 00	2.92E 06	26.142	3,286-01	7.359

and the second sec

•

OPTICAL CONSTANTS OF AL

ENERGY	EPSILON1	EPSILCN2	N	ĸ	ABSCOEFF	REFLECT:	ENERGYLOSS	N-EFF	
2-30E 01	-0.384	2.65F 00	1 - C BC	1.24F 00	2.90F 06	26-485	3+ 65E+ 01	7.621	
2.35E 01	-0.386	2.396 00	1.005	1.185.00	2.816.06	25.775	4.105-01	7.849	
2.406 01	-0.345	2.136.00	0.953	1.12E 00	2.72E 06	24.769	4.578-01	8.054	
2 806 01	-0.191	1 925 70	0.905	1.005.00	2.555 04	21 043	5 445-01	0 6 7 4	
24,000 01	-0.054	1 620 00	0.905	0.175-01	2.625.04	210 426	20445-01 4 746-01	0 743	
2.005 01	-0.050	1.032 CG	0.000	90172-01	2042C VD	14.423	0.140-01	0+100	
2.70E 01	0.052	1.51E CC	0.885	8.55E-01	2.34E 06	17.363	6.61E-01	9.085	
2.80E 01	0.133	1.45E CO	0.892	8.14E-01	2.31E 06	15.888	6.83E-01	9.403	
2.90E 01	0.159	1.44E CO	0.896	8.02E-01	2.36E 06	15.439	6.885-01	9,725	
2.55E 01	0.142	1.43E CC	0.867	8.03E-01	2.40E 06	15.639	6.94E-C1	9.889	
3.00E 01	0.168	1.4CE 00	C.868	8.04E-01	2.44E 06	16.041	7.126-01	$10_{*}053$	
3.C5E 01	0.075	1.35E CC	C.844	7.99E-01	2.47E 06	16.391	7.395-01	10.215	
3.10E 01	0.047	1.25E 00	0.818	7.88E-01	2.48E 06	16.682	7.75E-01	10.372	
3.20E 01	0.015	1.13E 00	0.757	7.47E-01	2.42E 06	16.939	8.84E-C1	10.668	
3.30E 01	0.080	9.81E-01	0.730	6.72E-01	2.25E 06	15.249	1.01F 00	10.933	
3.4JE 01	0.153	9. C1E-01	0.730	6.175-01	2.12E 06	13.420	1.C8E CO	11.177	
3.50E 01	0-214	8.455-01	0.737	5.735-01	7.03E 06	11.907	1.116.00	11.409	
3.605 01	0.258	8. CIE+01	0.741	5.40E=01	1.97E 06	10.705	1.135 00	11.616	
3,70E 01	0.294	7.616-01	0 745	5.116-01	1.025 06	9.870	1.145 00	11.857	
3 605 01	0.324	7 265-01	0 740	/ 9AE=01	1 876 64	0.044	1 155 00	12 073	
3 0.05 01	0 363	6 635-01	0 751	4046-01	1 075 04	74040		13 305	
30,905 01	0.352	0.935-01	0.121	4.015-01	1+82C U0	0.001	T#T26 00	12.200	
4.CCE 01	0.377	6.6CE-01	0.754	4.38E-01	1.77E 06	7.715	1.14E CO	12.492	
4.10E 01	0.404	6.31E-01	0.760	4.15E-01	1.73E 06	7.052	1.12E 00	12.695	
4.20E G1	0.428	6.C9E-01	0.766	3.98E-01	1.69E 06	6.503	1.10E CO	12.895	
4.30E CI	0.446	5.51E-C1	0.770	3-84E-01	1.67E 06	6-104	1.085 00	13,094	m -11 - E mara)
4.40E 01	0=455	5.72E-01	C.770	3.71E-01	1.66E 06	5+836	1.07E 00	13.291	ladie 5, page 2
4.50E 01	0.463	5.468-01	C. 767	3,556-01	1.62E 06	5.553	1.67F 0C	13.485	
4.60E 01	0.476	5-13F-01	0.767	3.355-01	1.56E 06	5,151	1.05E 00	13.671	
4.70E 01	0.495	4-86E+01	0.771	3-15E-01	1.50E 06	4.689	1.01E 00	13,851	
4-80E C1	0.515	4-646-01	C.778	2.985-01	1.45E 06	4.251	S. 63E-01	14.026	
4.90E 01	0.538	4.468-01	0.787	2.84E-01	1.41E 06	3.851	9.13E-01	14.198	
5 COF 01	0 557	4 225-01	0 705	2 775-01	1 285 04	3 531	0 (05-0)	14 247	
5 205 01	0.001	44.355-01	0 900	2.555-01	1.300.00	34337	0.04E-01	14.001	
5 406 01	0 414	2 555-01	0.000	2.0000001	1 335 04	3+0+3	7.570	14.107	
2040E 01	0.014	3+52E-01	0.820	2.415-01	1.32E UG	2.085	7.415-01	15.036	
5 00C 01	0.033	3+815-91	6.836	2.305-01	1.306 00	2+408	0.45E+01	15-370	
2006 JI	0.049	3-135-01	0.816	2.235-01	1.316 06	2.245	0+005-01	124 100	
6.COE 01	6.654	3.668-01	C.838	2.19E-01	1.33E 06	2.165	6.528-01	16.C48	
6.20E 01	0.649	3.52E-01	0.833	2.11E-01	1.33E 06	2.128	6.458-01	16.391	
6.43E 01	0.643	3.3CE-01	0.830	1.99E-01	1.29E 06	2.027	6.23E-01	16.725	
6.60E 01	0.651	3.026-01	0.828	1 .86E →01	1.245 06	1.898	5.936-01	17.046	
6.80E 01	0.654	2+625-01	0.827	1.71E-01	1.18E 06	1.760	5.56E-C1	17.353	
7.COE 01	C.662	2.575-01	0.828	1.555-01	1.10F 06	1-592	5-10F-C1	17.642	
7.20F 01	0.677	2.345-01	0.835	1.405-01	1.025.06	1 398	4 545-01	17 011	
7-40E 01	0.692	2.215-01	0.842	1.316-01	9,846 05	1.235	4.195-01	19.140	
7.6CE 01	0.707	2.106-01	0.847	1 246-01	9 546 05	1 120		10 4103	
7.805 01	0.700	241VE-01	0 050	1 175-01	7857C VJ 0 246 46	1 167	3 445-01	10.447	
I DOG OF	08769	10335-01	0.000	1.1/0-01	7029C VJ	1.001	3.00C-91	100000	
8.CJE 01	C.715	1.86E-01	0.853	1.09E-01	8.86E 05	0.971	3. 40E-C1	18.900	
8.ZJE C1	0.724	1.73E-01	C.857	1.01E-01	8.37E 05	0.834	3.11E-01	19,126	
8.30E 01	0.730	1.66E-01	C.86C	9.636-02	8.10E 05	0.836	2.96E-01	19.234	
8.35E 01	0.723	1.628-01	C.861	9.43E-02	7.98E 05	0.808	2.88E-01	19.287	
8.40E 01	0.737	1.626-01	0.865	9.38E-02	7.99E 05	0.775	2.83E-C1	19.340	

· · ·

~

• •

ENERGY	1EPSL1	EPSILCN2	1N	к	ABSCOEFF	REFLECT	ENERGYLOSS	N-EFF
8.45E 01	0-260	1.66E-01	0.135	9-62F-02	8.248 05	0.784	2.005-01	10 304
8.50E 01	0-262	1.655-01	0-136	9.56E=02	8.27E A5	0.707	2 905-01	
8.60F 01	0.265	1.545-01	0 1 3 9	0 195-02	9 005 05	0 720	2.095-01	
8.70E 01	0 242	1 5(5-01	01130	94102-92	0.00E 00	0.755	2.80E-01	19.557
8 75E A1	0 240	1 445-01	0 1 3 6	0.10E-02	1.0fm UD	0.755	2.655-01	19+659
0.13E VI	Ve 260	1.44CE**VI	0.135	8.445-02	7.49E 05	0.731	2.56E-01	19.709
3.80E C1	0.257	1.456-01	0.134	8.38E-02	7.48E 05	0.717	2.54E-01	19,759
3.50E 01	0.258	1.4CE-01	0.135	8.07E-02	7.28E 05	0.708	2.45E-01	19.858
9.10E 01	0.252	1.25E-01	0.132	7.18E-02	6.62E 05	0.649	2.176-01	20.040
9.30E 01	0.243	1.11E-01	0.128	6.368-02	5.998 05	0.581	1,905-01	20. 204
9.50E 01	0.234	9.55E-02	0.123	5.705-02	5.49E 05	0.520	1.676-01	20.356
1.COE 02	0.211	8.C7E-02	0.111	4.546-02	4.60E 05	0.402	1,29E-01	26-696
1.05E 02	0.151	6.365-02	0.100	3-53E-02	3.76E 05	0.312	9.475-07	20.040
1.10E 02	0.171	5 155-02	0.089	2.835-02	3 156 05	0 2 2 0	7.675-02	210 70 7
1.15F 02	0.155	4-125-02	0.080	2.746-02	2.416.05	J 1 00	F 366-00	21+292
1.20E 02	0.137	3.316-02	0.071	1 795-02	2 175 05	V. 144	D. 700-02	21.490
14200 02	00131	JOJICOL	0.011	10100-02	2+11E UD	0.144	4+455-02	ZI. 564
1.25E 02	0.123	2•86E-02	0.063	1.528-02	1.93E 05	0.113	3.716-02	21.706
1.3JE C2	0.110	2.516-02	0.056	1.335-02	1.75E 05	0.089	3.176-02	21.033
1.35E 02	0.059	2.25E-02	0.051	1.186-02	1.62E 05	0.071	2.775-02	21.952
1.43E 02	0.083	2.C8E-02	0.045	1.095-02	1.55E 05	0.056	Z. 50E-02	22-067
1.50E 02	9.C72	1.95E-02	0.037	1.01E-02	1.54E 05	0.037	2.265-02	22.293
1.60E 02	0.059	1.55E-C2	0.030	1.01E-02	1.638 05	0.026	2.205-02	22.533
1.70E 02	0.050	2.015-02	0.025	1.035-02	1.78E 05	0.019	2.225-02	22 703
1.80E 02	0.043	2.1CE-02	0.021	1.076-02	1.96E 05	0.015	2.295-02	22 CB1 Table 5 Dage 3
1.50E 02	0.037	2.1EE-02	0.015	1.11F-02	2.145 05	0.012	2 355-03	23 JOI TABLE J, Page J
2.CCE 02	0.034	2.26E-02	0.017	1.15E-02	2.33E 05	0.011	2.425-02	23.743
2.20E 02	0.029	2-32E-02	0.014	1-18F-02	2.635 05	0.000	2 445-07	34 513
2.40E 02	0.026	2.23E-02	0.013	1.135-02	2 355 45	0.007	2.965 02	
2.60E 02	0.024	2.(SE-02	0.012	1.045-02	2 702 05	0.004	2.05 02	47+343
2.80E 02	0-021	1.53E=02	0.011	G. 745-07	2 775 05		2.195-02	20.193
A.COE 02	0.010	1 775-02	0.000	9 05C-03	2.775 05	0.005	2+02E=02	27.040
30000 02		10171 52	0.007	0.792-03	2.128 03	0.004	1.84E-02	27.875
3.50E 02	C+015	1+45E-02	0.008	7.31E-03	2.59E 05	0.003	1.505-02	29.895
5.00£ 02	0.009	9.38E-03	0.005	4.715-03	2.38E 05	0.001	9+56E=03	35.581
6.COE 02	0.007	6 . 78E-03	C.OC4	3.40E-03	2.06E 05	0.001	6.E7E-03	38.744
8.00E 02	0.005	3.25E-03	0.003	1+635-03	1.308 05	0.000	3.285-03	43, 359
1.CQE 03	0.003	1.528-03	0.002	9+605-04	9.72E 04	0.000	1.93E-03	46.528
2.COE 03	0.001	2.4CE-04	0.000	1.205-04	2.43E 04	0.0	2.415-04	53, 226
2.50E 03	0.000	4.22E-04	0.000	2.11E-04	5.35E 04	0.0	4.225-04	55.575
2.85E 03	0.001	2.9CE-04	0.001	1.45E-04	4.18F 04	0.0	2.505-04	59 113
2.90E 03	0.001	3.285-04	0.001	1-64F-04	4.83E 04	0.0	2 205-04	50 401
5.00E 03	-0.002	5.14E+05	-0.001	2.87E-05	1.44E 04	0.000	5.725-05	66.716
1.00F 04	-0-001	5.(7E-C6	-0.000	2.525-04	3 545 43			
1-33E 04	-0-002	5.126-04	-0.001	200500	2+70C UJ	0.0	5.U8E-06	/1.107
1.405 64	-0.602	3.885-04	-0.001	2000	3.372 03	0.000	5.11E-06	72.200
1.505 04	-0.001	4.546-r4	-0.0001	1.945-00	2./5E U3	0.000	3.875-06	72.615
	-0.001	1,775-44		2.205-30	3.40E 03	0.0	4.556-06	73.133
2000C U4	-0.001	1+110-08	-0.00L	8.835-07	1.78E 03	0.0	1.765-06	74. 961
3.COE 04	0.000	3.65E-67	0.000	1.85E-07	5.60E 02	0.0	3.69E-C7	76.446
5.COE 04	-0.001	0.14E-08	-0.000	3.05E-08	1.54E 02	0.0	6.C9E-08	77.297
0+00E 04	-0+000	1.04E-C8	-0.000	5.226-09	4.22E 01	0.0	1.04E-08	77.637
0.30E 04	-0.005	3.52E-C8	-0.002	1.955-08	1.64E 02	0.000	3.885-08	77.682
1.50E 05	-0+000	5.126-09	-0.000	2.565-09	3.88E G1	0.0	5.125-09	78.465

OPTICAL CONSTANTS OF AU FRCP REFLECTIVITY-CATA FITTED TO CANFIELD ET AL (10)

4 I 4

ENERGY	EPSILON1	EFSILCN2	N	к	ABSCOEFF	REFLECT	ENERGYLCSS	N EFF	
				5 085 AO	9 AAE A5	97.101	2.915-03	0.006	
1.50E CO	-2.80E C1	2.25E CC	C+212	5.286 00	A DEE OF	710 2 2 1	1 225-02	0.018	
2.COE CO	-1.10E 01	1.63E 00	0.245	3.33E 00	6.756 05	92 241	1.920-02	0 024	
2.20E 00	-6.803	1.9CE 00	C.361	2.63E 00	5.86E Q5	83.423	3.092-02	0 0 2 3	
2 405 00	- 7.177	2. EEE 00	C.700	1.90E 00	4.63E C5	57.C87	1.576-01	0.000	
24445 00	-1.073	4.75E CC	1.378	1.728 00	4.55E 05	36.166	2.00E-01	0.049	
2.000 00	- 10 0 / 5	44732 00							
	0 ()7	4 545 66	1.449	1.83E 00	5.20E 05	36.419	1.646-01	0.072	
2.80E CU	-0.037	8.42 00	1 730	1 995 00	5.756 05	37.259	1.526-01	0.102	
3.COE CC	-0,585	6.546 00	1.729	1 505 00	6 06E 05	37.289	1.50E-01	0.126	
3.15E 00	-0.535	6.64E 00	1.750	1.902 00	4 20E 05	34, 931	1.516-61	C.152	
3.30E CC	- 0. 450	6.5EE OC	1.753	1.88E 00	D+20E UU	30.031	1 646-01	0.178	
3.45E 00	-0+217	6.48E OG	1.770	1.83E 00	6.40E 05	22+ FTV	1.145-01	2.1	
						26 221	1 605-01	0.205	
3.60E 0C	0.046	6.67E CC	1.832	1.82E 00	6.64E 05	55. 321	1.700-01	0.2/5	
3.805.00	-0.092	6.ESE CC	1.838	1.868 00	7.18E 05	36.206	1.468-01	6.247	
	-0.309	6-775 00	1.798	1.89E 00	7.63E 05	36.760	1.475-01	0.297	
	-0.547	6 676 00	1.739	1.89E 00	8.04E 05	37.167	1.516-01	C+331	
4.200 00			1.660	1.885 00	8.38E 05	37.384	1.585-01	C.373	
4.402 00	-0.111	OFTHE AA							
		5 375 60	1 464	1.77E 00	8.51E 05	36.044	1.646-01	0.445	
4.155 66	-0+689	3.236 00	1 460	\$ 455 00	8.37E 05	33.557	2.055-01	0.492	
5.COE CC	-0.622	4.245 66	14952	1 495 00	8.24E 05	29.295	2.37E-01	0.584	
5.505 00	-0.147	4.22E CC	1.427	1.485 00	0.175 05	25 493	2.645-01	0.673	
6.COE 00	0.211	3.77E CC	1.412	1.33E 00	B 412E 00	23.066	2.826-01	0.740	
6,50E CO	0.618	3.43E OC	1.433	1.20E 00	(+89E 05	22.030	20020-01	VU 1 U V	
						20 350	2.685-01	0.852	
7.CGE CC	1.014	3.43E CC	1.516	1.13E 00	8.04E 05	20, 034	2 495-01	0.953	
7.50E CC	1.176	3.64E CC	1.582	1.15E 00	8.16E UD	20.000		1 046	Table 6, page 1
A.CCE CC	C.783	3.77E CC	1.522	1.24E 00	1.00E 06	22+884	2.545-01	1.104	
8-505 00	0.693	3.44E CC	1.449	1.19E 00	1.02E 06	21.720	2.80E-CI	1.104	
	0.569	3.26F CC	1.392	1.17E 00	1.07E 06	21.476	2.585-01	1.244	
Secto VV	V. JU /								
0 405 00	0 660	2.57E 00	1.346	1.10E 00	1.06E 06	19.841	3.246-01	1.411	
9.500 00	0.540	2 955 00	1.316	1.095 00	1.11E 06	19.690	3.35E-¢1	1.523	
I.COE GI	0.597	2.666.00	1 247	1.045.00	1.11E 06	18.636	3.645-01	1.632	
1.C5E C1	0.515	2.646 00	1.201	10-21-01	1.106.06	17.166	3.96E-01	1.738	
1.1CE 01	0.536	2-41E UU	1.225		1 045 04	16 841	4-19F-01	1.838	
1.15E 01	0.675	2.17E 00	1.215	9*436-01	1.040 00	THEORY			
				0 605-01	1 045 04	13.813	4-C8F-01	1.939	
1.20E C1	C.813	2.14E CO	1.295	8.395-01	1 005 00	12 077	4.015-01	2.147	
1.30E C1	0.924	2.C8E 00	1.265	8-236-01	1.685 00	12.0071	4 105-01	2-366	
1.40E C1	0.929	2.C1E 00	1.254	8.C2E-01	1.142 00	12.373	4.102-51	2 500	
1.50F C1	0.927	1.52E 00	1.236	7.756-01	1.18E 06	11.11/	4.238-01	20799	
1.605 01	0.963	1.82E CO	1.229	7.39 [-01	1.20E 06	10.866	4.296-01	2.017	
	•••				1			3 6/3	
1.705 01	1-014	1.74E 00	1.231	7.07E-01	1.22E C6	10.100	4.29E-01	5.047	
1 005 01	1 1 1 5	1-71E CC	1.257	6.82E-01	1.24E 06	9.552	4.10E-C1	3+295	
LACUE OF	10117	1 975 00	1.792	7-035-01	1.355.06	10.091	3.88E-C1	3, 547	
1.905 01	10110		1 210	7.635-01	1.55E 06	11.450	3.78E-C1	3.946	
2.00E 01	1-1-54		1 374	9 455-01	1 84E C6	13.918	3.925-01	4,191	
2.1GE 01	0.874	2.20E 00	1+2/4	0.0000-01					
		3 365 66	1 314	0 045-01	1.97E 06	15,159	4.18E-01	4.375	
2.15E C1	C+653	2.26E LG	1.214	9#000-01 0 105-01	2 055 06	15.972	4-57F-C1	4.557	
2.206 01	0.443	2.CSE 00	1.131	9.192-01		16 005	5.02E-01	4.728	
2.25E Cl	0.340	1.93E 00	1.073	A*016-01	24000 00	15 041	5.44F=C1	4.897	
2.30E C1	0.275	1.75E CC	1.021	8.171-01	2.040 00	170041	5 C2E_01	5 047	
2.35E 01	0.244	1.65E 00	0.978	8.445-01	Z*018 06	15.417	D . 300 € 0 (74.041	
							/ /05 01	6 103	
2.40F C1	0.238	1.53E CC	C.944	8+C8E-01	1.97E 06	14.814	C. 40E-C1	5+143	
2,505 01	0.286	1.34E CO	0.910	7.365-01	1.87E 06	13.136	7.146-01	2.403	
2.405 01	0,343	1.22E CG	0.856	6.79E-01	1.79E 06	11.619	7.626-01	5.716	
2.4CUE U1	C. 267	1.146 00	0 895	6.35E-01	1.74E 06	10.385	7.845-01	5.958	
2 # FUE U1	0 443	1.145 00	0.901	6.07E-01	1.72E 06	9,502	7.86E-Cl	6.197	
2005 VI	0.443	T1/3- AA							

ч (ө

OPTICAL CONSTANTS OF AL FRCM REFLECTIVITY-CATA FITTED TO CANFIELD ET AL (10)

_

ENERGY	1EPSL1	EPSILON2	1N	ĸ	ABSCOEFF	REFLECTS	ENERGYLCSS	N-EFF	
9.10E 01	0.208	8.1CE-02	0+109	4.55E-02	4.19E 05	0.388	1.285-01	14.344	
9.308 01	0.200	7+06E-02	0.104	3.94E-02	3.716 05	0.347	1.09E-01	14.449	
9.50E C1	0.192	6.15E-02	C.100	3.426-02	3.29E 05	0.311	9.36E-C2	14.543	
1.CCE 02	0.173	4.65E-02	0.090	2.56E-02	2.59E 05	0.240	6.785-02	14.741	
1.C5E 02	0.156	3.33E→C2	0.081	1.816-02	1.93E 05	0.187	4+ 67E-02	14.893	
1.10E 02	0.139	2.47E-02	0.072	1.336-02	1.48E 05	0.143	3.326-02	15.007	
1.15E 02	0.125	1.7CE-02	0.064	9.C8E-03	1.06E 05	0.113	2+225-02	15.094	
1.20E 02	0.110	1.156-02	0.057	6.C8E-03	7.39E 04	0.086	1.458-02	15.154	
1.25E 02	0.058	8.74E-03	0.050	4.60E-03	5.82E 04	0.067	1.075-02	15,198	
1.30E 02	0.088	7.236-03	0.045	3.79E-03	4.98E 04	0.053	8.70E-03	15.235	
1+35E 02	0.079	5.53E-03	0.040	3.098-03	4.22E 04	0.043	6.59E-C3	15.266	
1.40E 02	0.070	5.23E→03	0.036	2.71E-03	3.85E 04	0.033	6.05E=03	15,295	
1.50E 02	0.058	5.95E-03	C.029	3-06E-03	4.66E 04	0.022	6.70E-03	15.360	
1.60E 02	0.048	6.12E-C3	0.024	3.14E-03	5.C9E 04	0.015	6.76-03	15.436	
1.70E 02	0.041	7.15E-03	0.021	3+65E-03	6.29E 04	0.011	7.785-03	15.527	
1.80E 02	0.035	9.458-03	0.017	4.81E-03	8.79E 04	0.008	1.C1E-02	15-647	
1.90E 02	0.031	1.086-02	0.016	5.485-03	1.05E 05	0.007	1.155-02	15.803	m) k = 3
2.COE 02	0.029	1.136-02	0.015	5.725-03	1.16E 05	0.006	1.205-02	15.078	Table 5, page 3
2.20E C2	0.025	1.15E-02	0.013	5.818-03	1.305 05	0.005	1.21E-02	16.371	
2.40E 02	0.023	1.C4E-02	0.011	5.286-03	1.28E 05	0.004	1.095-02	15.781	
2.60E 02	0.022	1.C9E-02	0.011	5.535-03	1.46E 05	0.004	1.145-02	17-226	
2.80E 02	0.020	7.536-03	0.010	4-015-03	1.14E 05	0.003	8-265-03	17 596	
3.COE C2	0.020	6.41E-03	0.010	3.246-03	9.84E 04	0.013	6.69E-03	17.029	
3.50E 02	0.017	3.325-03	C.CCS	1.67E-03	5.89E 04	0.002	3.445-03	18.584	

OPTICAL CONSTANTS OF AU FROM REFLECTIVITY-CATA FITTED TO CANFIELD ET AL (10)

ENERGY	EPSILGNI	EPSILCNZ	N	к	ABSCOEFF	REFLECTS	ENFRGYLCSS	V-E-t	
2.5CE 01	0.463	1.(8E CC	0.905	5.595-01	1.76E 06	9.234	7.818-C1	6.441	
2 S5E C1	0.447	1.C8E 00	0.900	5-01E-01	1-80E-06	9,153	7.88F-01	6.564	
3.CCE C1	0-423	1.C7E 0C	C-887	6-035-01	1.8°E 06	9,594	F.CPE-C1	5 585	
3.05E 01	0.395	1.C5E 00	0.870	6-018-01	1.86E 06	9,803	8.366-01	6.815	
3.105 01	0-370	1.01E 00	6-851	5.965-01	1.675 06	9.977	9.7CE-C1	6.918	
54102 01	0.510	INGIC 65	0.01	303-01	100/2 00	2 0 2 1 :	34 (SE CI		
3.20E C1	0.323	5.17E-01	C.805	5.70E-01	1.85E 06	10.132	9.705-01	7.175	
3.3CE 01	0.345	8.(56-01	0.781	5.15F-01	1.72F 06	9.127	1.055 00	7.392	
3.40E 01	0.384	7.37E-01	0.779	4.73E-01	1.63E 06	8.027	1.07E CC	7.591	
3.50E 01	0.420	6.E8E-01	C.783	4.39E-01	1.568 06	7.122	1.C6F CC	7.701	
3.60E 01	0.447	6.518-01	0.786	4.145-01	1.51E 06	6.457	1.C4E CC	7.965	
3.70E C1	0.449	6-17E-01	ŕ. 7 88	3-C1F=01	1-475-06	5.003	1.03E CC	8,145	
1. BOE C1	0.489	5 845-01	0 791	3 715-01	1 435 06	5 410	1 015 00	8 370	
3 COE CI	0 505	5 600-01	0 703	3 5 3 5 - 01	1 305 06	5.005	0.055-01	6 4 91	
4 006 01	0 520	5 315-01	0 765	3 245-01	1 345 04		0 415-01	0 458	
4 10E CI	0 5 2 0	5+51C-01	0.700	3.340701	T 905 00	4.310	30C1CTUL	0 0 0	
4.IUE UI	Ve 230	3.165-01	0.199	3.172-01	1.325 06	4.213	5•275701	8.820	
4.20E C1	0.555	4.E7E-01	C.8C4	3.C3E-01	1.29E 06	3.890	E.54E-C1	8.93C	
4.30E 01	0.567	4.72E-01	0.807	2.92E-01	1.27E 06	3.651	8.685-01	9.139	
4.40E C1	0.572	4.56E-01	0.807	2.82E-01	1.268 06	3.491	8.52E-01	5.296	
4.50E 01	0.576	4.35E-01	0.805	2.70E-01	1.235 06	3.321	E. 35E-01	9.450	
4. ECE C1	C. 584	4-C8E-01	0.805	2-54E-01	1.185 06	3-081	8.05F-01	5.599	
					10101 00	5.001		-	
4.7CE C1	G.597	3.856-01	0.809	2.385-01	1.13E 06	2.805	7. 6 3E-C1	5.741	
4 .80E Cl	0.612	3.66E-01	0+814	2.25E-01	1.09E 06	2.543	7.19E-01	5.580	
4.90E 01	0+629	3.5CE-01	0.821	2.135-01	1.C6E 06	2,303	6.765-01	16.014	Table 6, page
5.00E 01	0.643	3.38E-01	0.828	2.64E-01	1.045 06	2.112	6.40E-Cl	10.147	
5.20E C1	0.667	3.195-01	0.835	1.905-01	1.005 06	1 • 821	5.83E-C1	10.407	
5.40E C1	0.667	3.C5E-01	C.848	1.80E-01	9.83E 05	1.608	5.40E-C1	10.665	
5.60E C1	0.703	2.535-01	0.856	1.71E-01	9.71E 05	1.449	5.C5E-C1	10.921	
5.80E C1	0.714	2.66E-01	C.861	1.665-01	9.77E 05	1.343	4.84E-C1	11.190	
6.COE C1	0.718	2.8CE-01	0.863	1.625-01	9.88E 05	1.294	4.72E-C1	11.441	
6.20E 01	0.714	2.69E-01	0.859	1.565-01	9.836 05	1.273	4.62F-01	11.703	
6-40E 01	0.712	2.515-01	C.857	1-475-01	0.525.05	1.213	4.41E-C1	11.558	
6. AOE 01	0.714	2.335-01	0 856	1 365-01	9 115 05	1 1 1 5	4. 13E=01	12,202	
6.80E 01	0.716	2.126+01	0 855	1.24E=01	9 545 05	1 053	1.01E-C1	12.434	
7 (05 01	0.722	1 015-01	0 057	1 125-01		0 050	3 435-01	12 450	
7 305 01	0 724	1 335-01	1 1 1 1 1 1	0.075-01	7 995 95	0 0 0 1	3 035-01	12 849	
	V. / 34	19120-01	0.062	7.710-02	1.20E UD	34331	5.052-01	120049	
7.40E 01	C.746	1.61E-01	0.869	9.27E-02	6.95E 05	0.738	2.77E-01	13.037	
7.60E 01	0.754	1.52E-01	0.873	8.71E-02	6.71E 05	0.675	2.57E-C1	13.219	
7.80E C1	C. 760	1.42E-01	C.875	8.135-02	6.43E 05	0.628	2.386-01	13.395	
8.COE C1	0.765	1.325-01	0.878	7.525-02	6.1CE 05	0.581	2.19E-C1	13,563	
8.20E C1	0.772	1.2CE-01	0-881	6.82E-02	5.66E 05	0.528	1.575-01	13.721	
8.30E C1	0.777	1.15E-01	0.884	6.53F=02	5.49E 05	0.500	1.876-01	13,796	
8.35E 01	0.780	1.13F-01	0.885	6.37E-02	5.405 05	0.483	1.82E-C1	13.833	
8.40F 01	0.784	1,125-01	0.888	6.375-02	5,395 05	0.444	1.796-01	13.870	
8.45E 01	0.785	1.145-01	0.999	6.545-02	5.615.05	0.449	1-855-01	13.509	
8.50E C1	0.783	1 155-01	0.000	6 A95-02	5 595 05	0.474	1 036-01	13.944	
GRIGE RE	VERCO	1.150-01	0001	0.000-02	30195 03	78414	70036-01	1 26 240	
8.60E C1	0.781	1.CSE-01	0.88ć	6.13E-02	5.34E 05	0.472	1.75E-C1	14.020	
8.70E 01	0.783	1.026-01	0.887	5.766-02	5.08E 05	0.452	1.64E-01	14.090	
8.75E 01	0.786	9.916-02	C.888	5.585-02	4.95E 05	0.438	1.585-01	14.124	
8.8JE 01	0.788	S. 84E-02	0.885	5.548-02	4.94E 05	0.429	1.565-01	14.157	
8.SOE 01	0.787	9.34E-C2	0.869	5.26€-02	4.74E 05	0.423	1.495-01	14.224	
	6	16							

a 4

OPTICAL CONSTANTS OF BI

, ,

EN ER GY	EPSILON1	FPSILCN2	N	κ	ABSCOEFF	REFLECTS	ENERGYLOSS	N-EFF	
2.008-01	4.565 01	3.036 01	6.908	1.478 00	2,985.04	57.296	8-175-03	C. 003	
4. 005-01	5.86E C1	3-79E 01	9-572	2-21E 00	8.955 04	64 467	6 145-03	0 027	
- C 1E= 11	6 C9E 01	5 775 01	7 444	3 975 00	3 355 05	46 533			
3 COE 31	1 0/5 01	54776 01	1.700	24010 20	2.350 05	070742	1.168-92	··• 11 /	
9.C0⊨=01	1.805 01	D. 646 U.I	0.247	4.52E 00	3.665 05	65+737	1.605-02	0.254	
1.03E (00)	1.949	4.87E C1	5.03£	4.84E 00	4.91E 05	66.361	2. 056-02	0.412	
1.50E 00	-6.977	2.23E 01	2.861	3.89E 00	5.91E 05	61.925	4.10E-02	0.736	
2,025,02	-4.584	1.395 (1	2.244	3 175 00	6.29E 05	55.438	5.48F-02	0.976	
2.50F 10	- 3,629	9.95E 00	1.865	2.675 00	6 76F 05	51.320	8. 87F- 02	1 180	
3.00E 10	- 2.722	7. 665 00	1.556	2,275 00	6.89E 05	46 673	1 245-01	1 37/	
1.675.00	-1.053	5.71E 00	1.541	1 855 00	4 575 05	37 441	1+2+0-01	14 3 (4	
دي چور ور	1.000	J# 112 CO	10 243	1002.00	5.97E US	⊇/ • 0₩1	1.040-01	1.010	
4.00E 00	-0.585	5.155 00	1.517	1.70E 00	6.88E 05	34.185	1.92E-01	1.704	
5,00E 00	-3.101	4,495.00	1.482	1.525.00	7.68E 05	29.903	2.235-01	2.059	
5 . C)£ nh	- 0. 5C 4	4.155 00	1.364	1.54E 00	9.35E 05	31.406	2.355-01	2.450	
9.005.00	- 0.872	2 358 00	0.904	1.305 00	1.05E 06	31.954	3.745-01	3,103	
1.038.03	-0.432	1.3EE 00	0.710	9.685-01	9,815 05	26.428	6.625-01	3.71.2	
1 225 61	- 0 077	9 545-51	0 4 2 7	(
1.218 11	-0.072	5+242701	9.027	6.61E-UL	8.29E 05	19.411	1.16E 00	4.097	
1.49E 21	Q• 49 4	5.836~01	+04	4+565-01	6.415.05	11.653	1.535 00	4.394	
1.636 71	0.393	4.055-01	0.692	2.935-01	4.755 05	5.135	1.27E 00	4.630	
1.80E 01	3.555	2.575-01	0.763	1.685-01	3.07E 05	2.683	6.87E-01	4, 310	
3.008 01	0.722	1.766+01	0.856	1.035-01	2.99 <u>5</u> 15	0.903	3 . 195-01	4. 938	
2.235 01	0.872	1.34E-01	0.936	7.176-02	1.60E 05	1.248	1 726-01	5 64 3	
2 335 11	0.959	1.22E-01	0.981	6.27E-07	1 455 05	0 1 10	1 215 01	201244	
7 255 11	1 027	3 236+01	1 012	6 005-02	1.450 05	0.004	1.315-01	2.55	
3 435 31	1 1 70	1 630 01	1.045	3 305 03	1+405 00	9+036	1+16+-01	5.11?	
*+41E 11	1.128	2 0 70 - 11	1.000	1.395-02	1.80E 05	2.227	1+21F-01	5.139	Table 7, page 1
2.455 01	1-112	3. 525-01	1.070	1.83E-01	4.55E 05	0.893	2.825-01	5.195	, , , , , , , , , , , , , , , , , , , ,
2.50E 01	0.979	3.386-01	1.004	1.68E-01	4.26E 05	0.700	3.156-01	5.270	
2,558 11	C.978	3+ 05E= 01	1.001	1.525-01	3.94E 05	0.576	2.915-01	5. 335	
2.605 01	0.976	2.926-01	0.999	1.465-01	3.86E 05	0-534	2. 825-01	5.309	
2.655 01	0.978	2.75F-01	0.998	1-385-01	3.70F 05	0.473	2 675-01	5 460	
2.70F 01	1.006	2.59E-01	1.011	1,285-01	3,518 05	0.407	2.405-01	⊃•4⊃8 5-516	
2.155 01	1.048	3 .105 ~01	1.035	1.508-01	4 . 17E 05	0.567	2+595-01	5.579	
2,808,01	0.966	3.43E-C1	0.998	1 726-01	4,88 <u>5</u> 05	0.735	3.27E-01	5.658	
2.85E 01	0.953	2.94E-01	0.987	1.49E-01	4.31E 05	0.563	2. 56E-01	5. 730	
2.90E 01	0.961	2.83E-C1	0.991	1.43E-01	4.19E 05	0.514	2 825 01	5.798	
2.55E 01	0.957	2.726-01	C.988	1.38E-01	4.12E 05	9.482	2.755-01	5.964	
3. COF 01	9,959	2.50E+01	0.987	1.275-01	3.865 05	0.410	2 665 61	¢	
3,105,01	0 001	2.205-01	A 907	1 155-01	3400E 03	04410	2.556-01	5.927	
1 225 21		2 1 55 - 01	1 000	1.005.01	3.01C UJ	U. 33L	2.205-01	6.046	
2 + Z J E 11	1.007	2+100-01	14009	1.000-01	3,50E 05	0.290	2.056-01	6.160	
100JE 01	1.029	Z•19E=01	1.020	1.U8E-01	3.60E 05	0.293	1.585-01	6.278	
3.408.01	1.044	2.245-01	1.027	1.09E-01	3.76E 05	0.307	1.976-01	6.402	
3.60E 01	1.065	2.36E-01	1.038	1.146-01	4.14E 05	0.344	1.58F-01	6. 671	
3.805 01	1.080	2.528-01	1.046	1.20E-01	4.64F 05	0.396	2.055-01	6 072	
4.00E 01	1.087	2.755-01	1.051	1.31F-01	5.30E 05	0.466	2 195+01	7 31 1	
4.20E 01	1-079	2, 58E-01	1.048	1.425-01	6 04E 05	0.700	C # 1977 VI	10 21 1	
4. 40E 01	1.043	3_ 015=01	1.041	1.445-01	4 AAE DE	0 534	2.005401	7. 700	
	1000	36 012- GI	10091	1.4445-01	0+94E ())	0.539	2.46E-01	8.127	
4.60E 01	1.052	3.CSE-01	1.036	1.498-01	6.95E 05	0.565	2. 57E-01	8.581	
4+80E 01	1.044	3.14E-01	1.033	1.528-01	7.40E 05	0.583	2.64E-01	9.066	
5.00E 01	1.029	3.29E-01	1.027	1.60E-01	8.13E 05	0.649	2.82E-01	9.590	
5 .10E 01	1.016	3.41E-01	1.022	1.67E-01	8.63E 05	0.688	2.97F-01	9,94.0	
5.20E 01	0.999	3.398-01	1.014	1.676-01	8.83F 05	0.691	3, 055-01	10.167	
	-			· · · · •		00071	De UDICH UD	101121	

•

OPTICAL CONSTANTS OF BI

· · · ·

ENERGY	EP SILON1	EPSILON2	N	ĸ	ABSCOEFF	REFLECTE	ENERGYLOSS	N-EFF	
5.30E 01	0.985	3.38E-01	1.007	1-685-01	9.025 05	0-696	3.125-01	10-451	
5.40E 01	C.973	3.35E-01	1.000	1.675-01	9,166,05	0 405	2 145-01	10 7/0	
5.50E 01	0.959	3-32E-01	0 993	1 475-01	0 315 05	0,070	3.100-01	194745	
5-60E 01	0.947	3. 256-01	0 097	1 455 01	2431C 02	9.090	3.22E-01	11=047	
5.705 01	0.076	3 105-01	0.701	1.635-01	4.30C US	0.088	3+256-01	11. 347	
20172 V.	7 8 9 1 Q	5#19E-V1	0*481	1.626-01	9.38E 05	0+677	3.26E-01	11.645	
5.83E 01	0.925	3.11E-01	0.975	1.59E-01	9.37E 05	0.663	3.26E-01	11.942	
5.90E 01	0.916	3.C1E-01	0.970	1.55E-01	9.27E 05	0.639	3-235-01	12.234	
6.00E 01	C.909	2.51E-01	C.966	1.51F-01	9,176 05	0.616	3-105-01	17 677	
6.50E 01	0.894	2.51F-01	0.955	1.325-01	8.665.05	0.504		120022	
7.005 01	0.874	2 255-01	0.942	1-205-01	9.495 AF	0.504	24 712-01	17.847	
			UU / /L	10206 01	0000000	0. 404	2. //=01	10.215	
7.53E 01	0.860	1.845-01	0.933	9.85E-02	7.48E 05	0.379	2.37E-01	16,420	
8.008 01	0.862	1.5CE-C1	0.932	8.07E-02	6.545 05	0.297	1.965-01	17-466	
8.50E 01	0.866	1.256-01	0.933	6.71E-02	5.78E 05	2.241	1.64F-01	19.399	
9.COE 31	0.872	1.0CE-01	0.935	5.36E-02	4 895 05	0.188	1.305-01	19,196	
9.50E 01	0.882	8. 22E-02	0.940	4-37E-02	4.21E 05	0.147	1.056-01	19,866	
1.COE 12	0.891	6 765-00	0.045		· · · • · ·				
1.05E 12	0.000	0 / 15C - 22 5 / 05 - 05	0.940	3.54E-02	3.646 05	0.115	8.50E-02	20.455	
	0.007	7. CYE-02	0.949	3.00E-02	3.19E 05	0.092	7.00E-02	20.974	
1 165 00	5 01/	4. 188-02	0.953	2.51E-02	2.808 05	0.075	5.79E-02	21.431	
1.125 32	0.914	3,926-02	0.956	2.058-02	2.39E 05	0.061	4,685-02	21.826	
1.205 02	0+922	3. 26E - C2	0.960	1.705-02	2.07E 05	0.049	3.84E-02	22.165	
1.256 02	0.929	2.76E-02	0.964	1.435-02	1 825 05	0 030	3 305 03	22.442	
1.30F 02	0.934	2.36F-02	0-966	1.225-02	1 615 05	0.027	3,200-02	22.403	
1.35E 02	0.939	2.01E+02	0.969	1 045-02	1.630.05	0.033	2. PJE-02	22+121	
1.40E 02	0.944	1_616+02	0 072	9 675-02	1 335 65	0+027	2.285-02	22.959	Table 7, page 2
1.45E 02	0.949	1.415-02	0.07/	8.6/E-03	1.232 05	0.023	1.89E-CZ	23+162	14010 /, page -
		20412-02	··• • • • •	1.200-03	1.07E 05	0.019	1.575-02	23.339	
1.50E 02	0.953	1.18E-02	0.976	6.03F-03	9-17E 04	0.015	1.305-02	73 401	
1.60E 02	0.961	3.79E-03	C. 980	4-48E-03	7.275 04	0.010	1. JUL-02	234491	
1.70E 02	C.967	7.49E-03	0.984	3 815-03	4 E4E 04	0.027	9.922-03	2.34 146	
1.80E 02	0.972	5 54F-03	1986	3 31 5-03	6 DEC 04	0.007	Be UC = US	23.952	
1.905 02	0.977	5 575 03	C 600	3.005-03	0.00E 14	0.035	6.9LE-03	24.150	
			28 700	2.996-03	5.10t V4	0.004	6• 36E-03	24.347	
2+00E 02	C.980	5.6CE-03	0.990	2-835-03	5-74E 04	0.003	5 945-03	24 531	
2.108 02	0.983	5.54E-03	0.991	2.79F-03	5 94E 04	0.002	5 335-02	24+371	
2.205 02	0.985	5.555-03	C. 993	2.795-03	6.73E 04	0.002	5 7 5 07	24+ /2//	
2.305.02	C•987	5.675-03	0.994	2 855-32	6 65E 04	0.001	5.025.03	24.919	
2.40E 02	0.989	5.82F=03	0 005	2.035.03	3 1 2 04	0.001	3. 8XF-03	6 De 12 5	
		2 C C C C C C C C C C C C C C C C C C C	V. • 7 7 J	2.936-03	(+12E U4	0.091	5.956-03	25.354	
2+50E 12	0.991	6.275-03	0.996	3.156-03	7.985 04	0-001	6-39E-03	25,600	
2+60E 02	0.993	7.266-03	0.996	3.64E-03	9.60F 04	0.001	T. 365-03	25 996	
2.70E 32	0+993	3. C25-03	0.996	4.03F-03	1.10E-05	0.001	9.145-07	24 333	
2.80E 02	0.993	P. 215-03	0.996	4-17E-03	1,175 05	0.001	0 225 07	1004/7	
2.905 02	0.993	8.325-03	0.997	4.17E-03	1.23E.05	0.001	0.000-000 R 670-000	26-0123	
					INC US	0.0.01	0.43E=U3	/0, //0	
3.03E 32	0.993	8.34E-03	0.997	4.18E-03	1.27E 05	0.001	8.45F-03	27.407	
4.19E 02	0.993	8.295-03	0,997	4.16F-03	1-31E 05	0.001	R 405-03	27 420	
3.20F 02	0.994	8.205-03	0.997	4.11F-03	1.336 05	0.001	9 305-07	210 010	
3.335.32	0.994	8. C8E-03	0.997	4_056-07	1.365 05	0.001	0. 10C-00	20.201	
3.40E 02	0.994	7.946-03	0.997	3,985-03	1.275 AS	0.001	0 0/E 00	28.191	
	-		UU 2 7 F	30 700-03	10010 00	0.001	8. U4E-03	29.144	
3+ 575 72	0.994	7. 73E-03	0.997	3.875-03	1.37E 05	0.011	7.825-03	29 <u>5</u> 580	
3+60E 02	0,094	7.5CE-03	0.997	3.765-03	1.37F 05	0.031	7.605-03	270 JOJ	
3.70E 02	0.594	7, 295-03	0,997	3.655-03	1.375 05	0.001	7.376-03	30.475	
3+ 80E - 12	0.994	7. C 8E- 03	0.997	3,555-01	1.375.05	0.001	7.165-03	20.017	
3.935 02	0.995	6.88E-03	0.997	3.455-02	1.345 45	0.000	19100203	21. 250	
		•			10205 00	いたいいい	たん うつき テリ う	11 . 174	

a .

OPTICAL CONSTANTS OF BI

ENERGY	1EPSL1	EPSILCN2	1. - N	к	ABSCOEFF	REFLECTS	ENERGYLOSS	N-EFF	
4. COE 02	0.006	6.68E-03	0.003	3.355-03	1.36E 05	0-010	6 755-07	31 705	
4.20E 02	C. CC 5	6.2 ćE-03	0.003	3-145-03	1.346 05	0.000	6.796-03	214142	
4.40E 02	0.005	5 879-03	0.003	7.94E-03		0.000	5.336-03	32,663	
4.69E 92	0.005	5_ 50E=03	0.003	2 765-02	1.005 05	0.000	5.935-03	33.512	
4.895 02	0.005	5 175-02	0.000	2. 100-03	1.298.05	D•000	5.56E-03	74.345	
4000	0.019	241(5-05	0.002	2.595-03	1.26E 05	0.000	5.22F-03	35,163	
5.COE 02	0.005	4. 88E-03	0.002	2.45E-03	1-24F 05	0,000	4 535-02	35 0/7	
5.50E 02	0.004	4.26E-03	0.002	2 14E-03	1-195-05	1.000	6 205 03	374 90 1	
6.CDE 02	0.004	3.75E-C3	0_002	1.885-03	1.146.05	0.000		57.915	
6,50E 02	0.004	3.2 EF- C3	0-062	1.645-03	1 005 05	0.000	4. / <u>5</u> E-03	3 4 7 74 7	
7.00E 02	0.003	7.89E-03	0-002	1 655-03	1.000 00	0.000	3.3CE-03	41,470	
-			00002	10405-00	1.02E Q5	2.000	2.91E-03	43.042	
7.50E C2	0.003	2.525+03	0.002	1.26E=03	9.59E 04	0.000	2.54F=03	66.613	
8.00E 02	0.003	2 .23E- 03	0.001	1.125-03	8.99F 04	0.000	2 245-02	45 000	
8.50E 02	0.002	1.94E-03	0+001	9-73F-04	H. 386 04	0.000	2.246-03	47.403	
9.00E 02	0.002	1.68E-03	0.001	8-305-04	7 625 04	V. VU)	1.925-03	47.338	
9.50E 02	0-002	1 405-03	0.001		7.03E 04	0.000	I.685-03	48.529	
		10 HGL - 00	00001	/=015=04	6.12E Q4	0.000	1.416-03	49 . 590	
1.00E 03	0.002	1.14E-03	0+001	5.79E-04	5.85E 04	0.000	1.16E-03	50.574	
1.10E 03	0.002	8.66E-04	0.001	4.34E-04	4.81E 04	0.000	8.695-04	5 0 0 0 F	
1.20E 03	0.001	6.585-04	0.001	3-295-04	4 COF 04	0 000		20 793	
1.30E 03	0,001	5.116-04	0.001	2-54E-04	3.365.04	0.000	0.000-04	35.445	
1.40E 03	0.001	3- 56E-04	0 001	1 005-04	24202 04	0.000	5+12E-74	54.509	
				1 70 C - U 4	2000E U4	0.000	3. 975-04	55.412	
1.60E 03	0.001	2.57E-04	0.000	1.29E-04	2.08E 04	0.0	2 575-04	51 023	
1,80E 03	0+001	1.76F-C4	0.000	8.825-05	1-60E 04	0.0		20+ 512	
2.00E 03	0.000	1.25E-04	0.000	6-275-05	1.275 04	0.0	1. 775-04	57.6855	Table 7. page 3
2.20E 03	0.000	9- 085-05	0.000	6.54Em05		0.0	1+255-04	58.746	, page 3
2.40E 03	0.000	6.685-05	0 000	3 345-64	14016 04	0U	9.09E-05	59 . 42A	
			0.000	3.346-03	8.11E 03	0• 0	6.68E-05	59 . 978	
2.45E 03	0.000	1.296-04	0+000	6.45E-05	1.60E 04	0.0	1 205-04	40.140	
2.50E 03	0.000	1.48E-04	0.000	7.395-05	1.87E 04	0.0	1.296-04	51.144	
2.60E 03	-0.000	1.336-04	-0.000	6.675-05	1 745 04	0.0	1.455-04	50.432	
2.80F 03	0-000	1.38E-04	0.000	6 925-05	1.705.04	0.0	1.335-04	50,993	
3.00E 03	0.000	1 115-04	0.000		1.96E 04	0•0	1.38E+04	6?.292	
	5.010	TELECOT	0.000	2.215-03	1.698 04	0*0	1.125-04	63.324	
3.10E 03	0.000	1.04E-04	0.000	5.18E-05	1.63E 04	0.0	1.04F-04	63.960	
3.20E 03	-0.000	1.C8E-04	-0.000	5.426-05	1.76E 04	0.0	1 085-04	46 663	
3.30E 03	-0.000	1.056-04	-0.000	5.23E-05	1.746 04	0.0	1 046-04	11 01 E	
3.50E 03	- C. 000	9.015-05	-0.000	4.50 E-0.5	1.585 04	0.0	L Q 4 5 7 9 4	04+ 94 7	
4.00E 03	0.000	5-87E-05	0.000	2 935-05	1.105.04	0.0	9. UIE~35	55. UST	
_					1.18E 04	0.0	5.815-05	57.954	
6+09E 03	-0.000	1.54E-05	-0.00C	7.695-06	4.65E 03	0.0	1.546+05	77 797	
8.00E 03	-0.000	5.28E-06	-0,000	2.645-06	2.13E 03	D. 0	5 276-04	128217	
1.00E 04	-0.001	2.41E-06	-9,000	1-215-06	1.215 03	0.0		79.125	
1.20E 04	-0.001	1.336-06	-0.000	6-635-07	9 045 00	0.0	2 41 E = 06	75.073	
1.30E 04	-0.001	9. STE+07	-0-000	4.955-07		0+0	1.335-96	75.672	
			0.000	TO 7 20-07	0.51E UZ	0.0	9.905-07	75.887	
1.40E 04	- C+ 000	1.E7E-C6	-0.000	9.36E-07	1.33E 03	0.0	1.876-04	76 200	
1.50E 04	-0.000	1.416-06	-0.000	7.04E-07	1-07E 03	0.0		70 290	
2.00E 04	-0.000	8.266-07	-0.000	4-135-07	9 345 02	0.0	1.4410700	10.040	
3.00E 04	-0.000	1.905-07	-0.000	9.495-09	2 95E 02	0.0	0.20t-07	78.352	
5= COE 04	-0.000	3.2CE-08	-0.000	1.60E-08	2.03E 02 8.07E 01	9+0	1.895-07	79.724	
0 655 6-							De LUCTUR	סעס∎עס	
0.005 04	-0,000	5.12E-09	-0.000	2.56E-09	2.20E 01	0.0	5.12E-09	81.031	
7. UUE U4	- 0, 000	1.43E-C8	-0.000	7.135-09	6.53E 01	0.0	1.435-08	91,112	
1. CUE 05	-0+000	1.14E-08	-0.000	5.71E-09	5.76E 01	0.0	1.14F-08	81.303	
3.00E 05	-0,000	2.39E-10	-0.000	1.195-10	3+62E 00	0.0	2.306-10	03 143	
5.00E 05	-0.001	4.03E-11	-0.000	2-025-11	1.01E 00	0 0	6005 IV	72.143	
		· · · · · · ·			TODIE AA	V • U	4.035-11	32.251	

• •

OPTICAL CONSTANTS OF C

1.00 C2 -3-42E C2 2 -3-42E C2 3 -3-64 C2 5.03 1 -42E 01 1-99E 04 94.825 1-26F-C2 0.0C 3.00 C2 -1.03E 02 1.77E 03 7.113 1.24E 01 2.32E 04 77.092 4.16F-C3 0.0C 3.00 C2 -1.03E 02 1.77E 03 7.113 1.24E 01 2.32E 04 77.093 4.46C-C3 0.0C 5.00 C2 -1.03E 02 1.77E 03 7.113 1.24E 01 2.32E 04 87.633 4.46C-C3 0.0C 4.16F-C3 0.0C 4.16F-C3 0.0C 4.00 C2 -3.54E 01 7.53E 01 4.939 4.949 7.112E 01 2.48E 04 87.630 1.42E-02 0.0C 4.00 C2 -3.54E 01 7.53E 01 4.939 4.949 7.31E 00 2.48E 04 87.630 1.42E-02 0.0C 4.00 C2 -1.17E 01 2.44E 01 2.44E 01 2.48E 04 87.480 1.42E-02 0.0C 4.00 C2 -1.17E 01 2.44E 01 2.44E 01 2.47E 01 4.45E 00 2.48E 04 87.630 1.42E-02 0.0C 4.00 C2 -1.17E 01 2.44E 01 2.47E 01 3.159 4.465E 00 2.48E 04 87.630 1.42E-02 0.0C 4.00 C1 -1.17E 01 2.44E 01 2.47E 01 3.169 4.465E 00 2.47E 04 4.423 7.11E-02 0.0C 4.00 C1 -1.17E 01 2.44E 01 2.47E 11.29E 00 3.42E 04 11.423 7.1EE-02 0.0C 4.00 C1 -0.23E 7.22E 7.2E 7.13E 7.2E 7.13E 7.2E 7.2E 7.2E 7.2E 7.2E 7.2E 7.2E 7.2	ENERGY	EPS ILON 1	EP SILON 2	N	к	ABSCOEFF	REFLECT%	ENERGYLOSS	N-EFF	
1+00 02 -1-15 02 1:466 02 7:469 1:415 01 1:45 04 87:409 3:46-01 0.000 2:400 02 -1.010 02 1:120 02 4:007 1:120 01 2:44 07 1:120 01 2:44 04 87:409 4:46-01 0.000 4:006 02 -1.010 02 1:120 02 4:007 1:120 01 2:44 04 87:409 4:46-01 0.000 4:006 02 -3.556 01 4:77 01 3:472 4:40 01 2:410 01 83:420 7:256 00 4:468-00 2:060 1:468-00 2:060 1:468-00 1:468-	1.00E 02	-3.42E 02	2.C4E 02	5-303	1.925 01	1,956.04	94.825	1 265-01	0.0	
2:00 c2 -1:01 c2 1:17 c2 2:7:115 1:22 c1 2:24 c4 6 87.630 2:14 c5 c5 0:000 2:05 c2 -1:01 c2 2:4:07 4:07 2:24 c4 67 87.630 2:4:00 0:2.000 2:000	1.50F 02	-1-15E 02	1.54E 02	7 499	1 315 01	1 005 04	07 403	3 305-03	0.000	
2:00 02 -1:01 02 1:122 02 4:007 1:122 01 2:460 04 0:030 4:4600 0 3:070 02 -3.546 01 4:770 01 3:472 4:400 2:480 04 8:422 7:250 0 4:00 02 -3.546 01 4:770 01 3:472 4:400 2:480 04 8:422 7:250 0 4:00 02 -3.547 01 4:770 01 3:472 4:465 00 2:476 04 7:900 1:446 02 0:000 0 4:00 02 -3.547 01 4:770 01 3:472 4:465 00 2:476 04 7:900 1:446 02 0:000 0 4:00 02 -4.4103 4:00 01 3:472 4:465 00 2:476 04 7:900 1:446 02 0:000 0 4:00 01 6:709 9:018 00 1:310 0:000 1:310 0:000 1:310 0 4:00 01 6:709 9:018 00 2:490 0 4:00 00 3:775 4:970 0 5:00 01 6:709 9:018 0 5:00 01 1:016 0 5:00 0 0 5:00 0 5	2.005 02	-1-03E 02	1.775 02	7 115	14310 01	7 676 04	074072	3.190-00	0.000	
3. OPC 612 -7. OPC 61 1.532 01 4.775 01 3.472 4.916 00 2.000 1.94400 1.95400 7.44000 1.44000 2.0000 4.7175 01 3.452 4.656 00 2.085 04 67.559 2.6400 1.44000 2.0000 1.44000 2.0000 1.4100 2.090 01 2.972 3.666 00 2.885 04 95.251 4.4200 2.0000 1.4000 0.1000 1.4000 00 1.4000 0.1000 2.0000 2.0000 2.0000 2.0000 1.4000 1.4000 0.10000 1.4000 0.10000 2.0000 2.0000 2.0000 2.0000 1.4000 1.4000 0.10000 1.4000 0.10000 2.0000 2.0000 2.0000 2.0000 1.4000 0.10000 1.4000 0.10000 1.4000 0.10000 1.4000 0.10000 1.4000 0.10000 1.4000 0.10000 2.0000 2.0000 2.0000 2.0000 1.4000 1.4000 0.10000 1.4000 0.10000 1.4000 0.10000 1.4000 0.10000 1.4000 0.10000 2.0000 1.4000 0.10000 2.0000 1.4000 0.10000 1.4000 0.10000 1.4000 0.10000 2.0000 2.0000 1.4000 0.10000 2.0000 1.4000 0.10000 2.0000 1.4000 0.10000 2.0000 1.4000 0.1000 0.1000 0.1000 0.1000 0.10000 0.0000 0.10000 0.10000 0.10000 0.10000 0.10000 0.10000 0.10000 0.10000 0.10000 0.10000 0.10000 0.10000 0.0000 0.10000 0.10000 0.0000 0.10000 0.10000 0.10000 0.10000 0.00000 0.10000 0.10000 0.10000 0.00000 0.10000 0.00000 0.10000 0.00000 0.10000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.000000	2.50E 02	-1.01E 02	1 115 02	/ 007	1+246 01	2.745 04	07+099	4.195-03	0.000	
Along of the set of t	3.006.02	-7 095 01	7 502 01	4.771	1.126 01	2.04E U4	87.630	4.542-01	C.CCC	
4.06 02 -3-5.46 01 4.77E 01 3.472 6.66 00 2.78E 04 779.060 1.4CE-02 C.CCC 0.CC1 1.17E 01 2.497 3.159 4.65E 00 2.48E 04 67.559 2.494-03 0.CC1 2.497 0.201 2.497 0.2	3.000 UE	-1.085 01	1.53E UI	4, 974	9.31E 00	2.81E 04	85.426	7.29E-03	0.000	
6.00 02 -1.17 01 2.494 01 3.159 4.655 00 2.885 04 67.59 2.444-02 0.000 1 1.00 01 0.778 1.645 01 2.970 2.796 04 2.462 4.23 4.245-00 0.000 1 2.00 01 0.708 1.645 01 2.970 2.796 04 2.462 4.24 03 4.245-00 0.000 1 2.00 01 0.653 4.76 02 2.494 1.297 03 2.026 04 31.666 7.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.0000 0.0000 0.000 0.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0	4.00E 02	-3.54E 01	4.77E 01	3.472	6.86E 00	2.76E 04	79,060	1.408-02	c.ccc	
8.00 02 -4.103 2.092 01 2.932 3.566 00 2.486 04 49.231 4.227-02 0.000 2.000 01 0.270 9.087 05 3.000 1.516 00 2.090 04 49.423 7.11E-02 0.000 4.000 01 0.570 9.087 05 3.000 1.516 00 3.090 04 4.4.333 7.11E-02 0.000 4.000 01 0.537 0.677 00 2.098 00 3.090 04 9.4.930 0 7.455-00 0.000 1.000 01 5.890 06 6.777 00 2.098 00 1.056 05 12.331 1.305-01 0.000 1.000 00 3.777 4.597 00 2.232 1.1305-01 1.256 05 14.4229 1.677-01 0.000 2.000 00 2.446 2.328 00 1.475 0 6.466-01 1.266 05 12.353 1.756-01 0.0115 3.000 00 2.446 2.328 00 1.476 01 2.492 05 1.677 0.0115 1.438 7.328-01 2.936 05 12.339 2.768-01 0.015 4.000 00 2.446 2.328 00 1.478 05 3.488 05 12.393 2.768-01 0.216 3.000 00	6.00E 02	-1+17E 01	2.94E 01	3.159	4.65E 00	2.83E 04	67.559	2.945-02	0.001	
1:006 01 0.278 1.44E 01 2.470 2.79E 00 3.02E 04 31.445 7.1E-02 0.000 3:006 01 6.703 7.62E 00 2.444 1.29E 00 3.02E 04 31.463 7.00E 02 0.000 4:006 01 6.433 6.890 6.2330 0.22431 1.22E 00 4.43E 04 24.910 7.00E 0. 0.000 1:51E 00 3.775 4.970 0.2431 1.22E 00 4.43E 04 24.910 7.00E 0.000 1:50E 00 3.722 1.22E 00 1.074 1.12E 00 4.43E 04 24.910 7.00E 0. 0.000 1:50E 00 3.775 4.970 0.2431 1.12E 00 4.43E 04 24.910 7.00E 0. 0.00E 0.0	8.00E 02	-4.103	2.C9E 01	2.932	3.56E 00	2.88E 04	58.251	4.63F-02	0.001	
2.00 E 01 6.703 9.63E 0C 3.000 1.55E 00 3.05E 04 34.363 7.11E-02 0.002 3.00E 01 7.028 7.62E 0C 2.444 1.29E 00 3.02E 04 31.663 7.65E-02 0.003 5.000 01 5.080 6.377 0C 2.494 1.22E 00 4.93E 04 29.910 7.45E-02 0.000 5.000 01 5.080 6.377 1C 2.294 1.042 00 1.05E 04 29.910 7.45E-01 0.000 5.000 01 5.080 6.377 1C 2.294 1.042 00 1.05E 04 29.910 7.45E-01 0.000 5.000 01 5.222 5.22E 0C 1.977 9.106-01 1.22E 05 14.920 1.45Te-01 0.000 2.906 0C 2.792 7.52E 0C 1.977 9.106-01 1.50E 05 14.920 1.45Te-01 0.000 2.906 0C 2.410 7.45E 0C 1.977 9.106-01 1.50E 05 14.920 1.45Te-01 0.000 2.400 7.445 7.32E 0C 1.977 6.966-01 1.50E 05 14.920 1.45Te-01 0.000 3.50E 0C 2.445 7.32E 0C 1.977 6.966-01 2.00E 51 12.763 1.976-01 0.000 7.45E 0C 2.445 7.32E 0C 1.978 7.394-01 2.90E 05 12.493 7.45E-01 0.116 4.00E 0C 1.4722 7.52E 0C 1.518 7.04E-01 3.48E 05 12.309 7.76F-01 0.116 4.00E 0C 1.4722 7.52E 0C 1.518 7.04E-01 3.48E 05 12.309 7.76F-01 0.116 4.00E 0C 1.4722 7.52E 0C 1.518 7.04E-01 3.48E 05 12.309 7.76F-01 0.126 4.00E 0C 1.403 7.04E-01 1.154 7.54E-01 3.48E 05 12.309 7.76F-01 0.128 4.00E 0C 1.403 7.04E-01 1.444 7.54E-01 3.48E 05 12.309 7.76F-01 0.228 4.00E 0C 1.403 7.04E-01 1.459 7.23E-01 7.06E 7.094 4.76F-01 0.228 4.00E 0C 1.403 7.04E-01 1.459 7.23E-01 1.428 05 1.239 7.76F-01 0.228 4.00E 0C 1.403 7.04E-01 1.459 7.23E-01 1.428 05 7.2384 7.36E-01 0.228 4.50E 0C 1.403 7.04E-01 1.459 7.23E-01 1.428 05 7.2384 7.36E-01 0.228 4.50E 0C 1.403 7.41E-01 1.459 7.23E-01 1.428 05 7.2384 7.36E-01 0.228 4.50E 0C 1.403 7.41E-01 1.439 7.53E-01 1.428 05 7.2384 7.36E-01 0.228 4.50E 0C 1.403 7.41E-01 1.459 7.23E-01 7.05E 7.4 2.94E-01 7.226 4.50E 0C 1.403 7.74E-01 1.429 7.35E-01 7.05E 7.4 7.96E-01 0.228 4.50E 0C 2.403 7.74E-01 1.429 7.35E-01 6.108 7.4 2.94E-01 7.35E 7.228 4.50E 0C 7.603 7.74E-01 1.439 7.56E-01 7.05E 7.4 2.94E-01 7.35E 7.228 4.50E 01 3.4773 1.64F 0C 1.773 6.66E-01 7.05E 7.4 2.94E-01 7.35E 7.228 4.50E 01 3.4773 1.64F 0C 1.773 6.66E-01 7.35E 7.2285 7.228 7.25E-01 7.35E 7.4428 7.35E 7.25E 7.25E 7.25E 7.25E 7.25E 7.25E 7.25E 7.25E 7.25E	1.00E 01	0.278	1.61E 01	2.870	2.79E 00	2.79E 04	49.423	6.26E=02	0.001	
1.00E 01 7.028 7.65E 0C 2.949 1.29E 00 3.92E 04 31.663 7.65E-02 0.003 4.00E 01 5.390 6.87E 0C 2.930 1.122E 00 4.98E 04 30.63 7.65E-02 0.003 4.00E 01 5.390 6.87E 0C 2.930 1.122E 00 4.98E 04 30.910 7.65E-02 0.003 1.00E 00 3.775 4.57E 0C 2.200 1.479 3.16E-01 1.22E 05 16.094 1.55E-01 0.003 2.00E 0C 2.386 2.37E 0C 1.879 7.39E-01 1.20E 05 13.555 1.77E-01 C.173 3.00E 0C 2.416 2.38E 02 1.775 6.78E-01 2.40E 05 12.431 1.61E-01 0.116 4.90E 0C 1.423 2.02E 0C 1.618 7.54E-01 3.82E 05 11.221 0.221 1.225 0.214 1.665 1.233 2.36E-01 1.246 0.2337 2.36E-01 1.246 0.2337 2.36E-01 1.256 1.077 3.92E 0.2146-01	2.00E 01	6.703	9.C3E 00	3.000	1.51E 00	3.05E 04	34.393	7.11E-02	0.002	
4:000 6:337 6:472 0:423 <td< td=""><td>3-00E-01</td><td>7.028</td><td>7.625.00</td><td>2 94 9</td><td>1 205 00</td><td>2 0 2 5 0 4</td><td>21 4 4 3</td><td>7</td><td></td><td></td></td<>	3-00E-01	7.028	7.625.00	2 94 9	1 205 00	2 0 2 5 0 4	21 4 4 3	7		
1.002 01 2.600 2.711 1.225 00 4.732 04 2.840 05 2.840 05 4.620 0 6.620 6.627 6.627 6.627 1.005 00 3.222 3.225 01 1.974 01 1.245 05 16.994 1.255-01 9.621 2.005 00 3.222 3.225 01 1.974 01 1.245 05 16.994 1.255-01 0.621 2.005 00 2.736 02 1.876 01 1.245 05 16.994 1.255-01 0.623 3.005 00 2.461 2.335 01 1.752 6.785-01 2.046 05 12.354 1.615-01 0.764 4.005 00 1.232 2.025 01 1.605 6.127-01 2.431 2.357-01 0.115 4.506 00 1.722 2.325 01 1.656 1.232 0.215 05 1.234 2.357-01 0.216 4.506 00 1.232 2.016 01 1.358 7.034 0.55 1.322 2.357 0.216 1.344 5.900 00 1.636 1.436 0 1.936 1.1265 0.5 1.039 1.946 05 1.239 <td< td=""><td>4.00E.01</td><td>6 630</td><td>4 935 00</td><td>2 . 7 . 7</td><td>1.298 00</td><td>5.94C V4</td><td>11.003</td><td>7.652-02</td><td>0.003</td><td></td></td<>	4.00E.01	6 630	4 935 00	2 . 7 . 7	1.298 00	5.94C V4	11.003	7.652-02	0.003	
1.100 2.103 3.112 1.12 2.034 1.120 5.900 3.222 3.226 01 1.246 00 5.900 3.222 1.226 01 1.246 01 1.230 1.246 01 1.230 1.246 01 1.246 01 1.246 01 1.246 01 1.246 01 <td>5 00E 01</td> <td>5 800</td> <td>0.03E UU</td> <td>2.00</td> <td>1.228 00</td> <td>4.936 04</td> <td>29.910</td> <td>/.65E-02</td> <td>0.000</td> <td></td>	5 00E 01	5 800	0.03E UU	2.00	1.228 00	4.936 04	29.910	/.65E-02	0.000	
1.02 00 3.222 3.221 0.2 2.434 1.386 00 1.656 05 22.221 1.36E-C1 0.021 1.980 00 3.222 3.221 0.2 1.974 3.16E-C1 1.50E 05 14.929 1.67E-C1 0.023 2.00E 0C 2.782 2.55E 0C 1.479 7.30E-C1 1.50E 05 12.934 1.67E-C1 0.023 3.00E 0C 2.440 2.38E 0C 1.472 6.78E-C1 2.06E 05 12.763 1.75E-C1 0.023 4.00E 0C 2.440 2.38E 0C 1.475 6.777 3.00E 0C 2.445 2.35E 0C 1.478 7.66E-C1 2.06E 05 12.763 1.75E-C1 0.021 4.00E 0C 2.441 2.37E 0C 1.519 7.66E-C1 2.40E 05 12.394 2.7EE-C1 0.115 4.00E 0C 2.445 2.35E 0C 1.458 7.23E-C1 2.49E 05 12.491 2.36E-C1 0.115 4.00E 0C 1.233 2.05E 0C 1.359 7.66E-C1 3.44E 05 12.397 2.7EE-C1 0.115 5.00E 0C 1.233 2.05E 0C 1.359 7.64E-C1 3.44E 05 12.397 2.7EE-C1 0.121 5.00E 0C 1.233 2.05E 0C 1.359 7.64E-C1 3.44E 05 12.491 2.36E-C1 0.23E 4.00E 0C 1.233 2.05E 0C 1.359 7.64E-C1 3.44E 05 12.491 2.36E-C1 0.225 5.00E 0C 1.233 2.05E 0C 1.359 7.64E-C1 3.44E 05 7.4004 4.56E-C1 0.23E 7.60E 0C 1.464 4.55E-01 1.256 4.00E 0C 1.464 4.55E-01 1.256 4.00E 0C 1.464 4.55E-01 1.256 4.4655 1.661 1.46E-C1 0.225 7.00E 0C 1.643 2.43E-01 1.379 1.395-01 1.48F 05 2.335 2.54E-C1 0.225 7.00E 0C 1.643 4.65E-01 1.575 1.44E-01 7.465 3 4.294 4.56E-C1 0.225 7.00E 0C 1.644 4.55E-01 1.575 0.23E-01 1.48F 05 2.332 7.00E 0C 2.643 4.75E-01 1.576 3.23E-01 2.055 7.885 8.225E-C2 0.322 4.00E 0C 2.643 4.75E-01 1.576 3.23E-01 2.055 7.885 8.225E-C2 0.322 9.00E 0C 2.643 4.75E-01 1.576 3.23E-01 4.55E 05 10.606 1.34E-C1 0.45E 1.00E 0C 3.673 1.22E 0C 1.773 3.34E-01 3.22E 05 1.25E 0.5 1.34E-01 0.45E 1.00E 0C 3.673 1.22E 0C 1.773 5.22E-01 4.55E 05 10.606 1.34E-C1 0.45E 1.00E 01 3.773 1.65E 0C 1.783 9.34E-01 3.22E 05 1.25E-02 0.323 9.00E 01 2.643 4.75E-01 1.539 7.84E-01 7.465 05 12.342 1.67E-C1 0.45E 1.55E 01 1.464 2.25E 0C 1.573 9.34E-01 1.18E 06 14.764 3.16E-C1 0.45E 1.45E 01 2.45E 01 1.45E 01 1.457 4.45E-01 1.555 1.45E 01 2.45E 01 1.457 4.45E-01 1.555 1.45E 01 2.45E 01 1.457 4.45E-01 1.555 1.45E 01 1.45E 01 1.45E 01 1.45E 06 1.45E 01 1.45E 06 1.45E 01 1.45E 1.45E 01 1.45E 02 1.575 3.34E-01 1.14E 06 16.4754 4.16E-01 1.14E 1.45E 01 1.45E 02	1 30E 00	2,030	0.378 JG	2.598	1.18E 00	5.98E 04	28.380	8.46E-02	0.007	
1.900 00 3.222 3.220 01 1.974 9.166-01 1.246 05 16.934 1.55E-01 0.034 2.905 00 2.946 2.735 02 1.979 7.396-01 1.505 05 14.929 1.67F-01 0.034 3.905 00 2.461 2.335 02 1.979 6.0570 1.905 13.985 1.765-01 0.037 4.905 00 2.461 2.335 02 1.972 6.785-01 2.905 03 13.763 1.51E-1 0.064 4.905 00 2.461 2.337 02 1.458 6.815-01 2.462 03 12.354 2.46E+01 0.115 4.905 00 1.722 3.325 00 1.919 6.103-01 3.925 03 12.451 2.325+0 0.115 5.905 00 1.252 1.455 01 1.956 6.103-01 3.925 03 12.451 2.325+0 0.115 5.905 00 1.253 1.455 01 1.956 6.103-01 3.925 05 11.329 2.325+01 0.211 5.905 00 1.453 7.615-01 1.353 4.155+01 2.525 05 4.993 4.255+01 0.211 5.905 00 1.455 7.455-01 1.553 4.155+01 2.525 05 4.993 4.255+01 0.211 7.905 00 1.453 7.615-01 1.53 4.155+01 2.525 05 4.993 4.255+01 0.255 7.906 00 1.453 7.615-01 1.537 4.155+01 1.484 05 2.335 2.546+01 0.275 7.905 00 1.454 4.735+01 1.239 1.585+01 1.484 05 2.335 2.546+01 0.275 7.905 00 1.4614 4.735+01 1.239 1.585+01 1.484 05 2.335 2.546+01 0.275 7.905 00 1.464 3.935+01 1.463 1.455+01 1.425 05 1.991 1.465+01 0.275 7.905 00 2.963 4.755+01 1.453 1.465+01 2.2015 05 7.865 9.225 0.522 0.327 7.905 00 2.963 4.755+01 1.463 1.465+01 2.245 05 4.993 4.425+01 0.275 7.905 00 2.963 4.755+01 1.463 1.465+01 3.225 05 9.235 1.656+01 0.357 1.905 00 2.963 4.755+01 1.463 1.465+01 3.225 05 9.235 1.656+01 0.357 1.905 00 2.963 4.755+01 1.463 1.465+01 3.225 05 9.235 1.656+01 0.357 1.905 00 2.963 4.755+01 1.735 5.825+01 3.925+05 1.9066 1.245+01 0.2657 1.905 00 2.963 4.755+01 1.735 5.825+01 3.925+05 1.9066 1.945+01 0.956 1.905 00 2.963 4.755+00 1.937 7.965+01 3.225+05 1.9066 1.945+01 0.956 1.905 00 2.963 4.755+00 1.937 7.965+01 3.225+05 1.9066 1.945+01 0.956 1.905 01 2.922 2.915 00 1.735 5.935+05 1.936+01 1.936 0.125+01 0.956 1.905 01 2.922 2.915 00 1.937 7.965+01 1.455 05 1.2764 2.237+01 0.957 1.955 01 2.922 2.915 00 1.937 7.965+01 1.455 05 1.2764 2.237+01 0.934 1.905 01 1.945 2.925 00 1.933 7.965+01 1.455 06 17.334 4.164+01 1.947 1.956 01 1.969 2.915 0.7.938 7.935+01 1.945 06 1.4764 3.925+01 1.445 1.90	1.000 00	3.1/3	4.598 00	2.294	1.34E 00	1.05E 05	22.321	1.3CE-C1	0.021	
2.00E 0C 2.086 2.782 0. 1.479 7.306-01 1.506 05 14.029 1.47F-C1 0.677 3.00E 0C 2.782 7.52E 0C 1.477 4.306-01 1.766 05 13.585 1.476-C1 0.757 3.00E 0C 2.442 2.33E 0C 1.752 4.785-01 2.066 05 12.753 1.516-C1 0.755 4.00E 0C 2.445 2.33E 0C 1.766 4.815-01 2.462 05 12.336 2.766-01 0.115 4.00E 0C 1.722 2.32E 0C 1.919 7.64E-01 3.48E 05 12.309 2.766-C1 0.211 5.00E 0C 1.233 2.03E 0C 1.444 7.54E-01 3.49E 05 12.309 2.766-C1 0.211 5.00E 0C 1.233 2.03E 0C 1.444 7.54E-01 3.49E 05 12.309 2.766-C1 0.211 5.00E 0C 1.255 1.45E 0C 1.195 4.105-01 2.452 05 1.2395 2.556-C1 0.221 5.00E 0C 1.155 1.45E 0C 1.195 4.105-01 2.52E 05 4.033 4.276-C1 0.221 5.00E 0C 1.163 7.64E-01 1.196 4.105-01 2.52E 05 4.033 4.276-C1 0.221 5.00E 0C 1.464 4.55E-01 1.197 4.346-01 1.265 1.951 1.46E-C1 0.225 7.00E 0C 1.644 4.55E-01 1.197 4.301 1.58E-01 1.12E 05 1.951 1.46E-C1 0.225 8.00E 0C 2.337 2.66E-01 1.631 9.60E-02 7.05E 04 4.518 4.81E-C2 0.228 8.00E 0C 2.337 2.66E-01 1.631 9.60E-02 7.05E 04 4.518 4.81E-C2 0.258 8.00E 0C 2.493 7.74E-01 1.736 2.23E-01 2.03E 05 7.865 8.225E-C2 0.327 9.50E 0C 3.693 4.75E-01 1.643 4.45E-01 3.22E 05 4.255 1.0696 1.2467 1.0.477 1.056 0D 3.693 1.22E 0C 1.791 3.34E-01 3.22E 05 4.255 0.5 1.0696 1.2467 1.0.477 1.056 0D 3.693 1.22E 0C 1.771 5.34E-01 3.22E 05 4.255 0.5 1.0696 1.2467 1.0.477 1.956 0D 3.693 1.22E 0C 1.772 6.465-01 1.746 0.5 11.796 1.47F-1 0.477 1.956 01 3.673 1.62E 0C 1.771 5.542E-01 6.197 5.11.796 1.647F-1 0.477 1.955 01 1.645 2.243E 0C 1.773 6.485-01 9.565 13.711 2.467C-1 7.552 1.155 01 2.522 2.31E 0C 1.773 6.485-01 9.565 13.745 4.22EF-C1 0.552 1.155 01 2.552 2.31E 0C 1.773 6.485-01 1.286 05 11.796 1.677C 1.552 1.155 01 1.452 2.243E 0C 1.542 8.64E-01 1.886 06 14.764 3.02EF-C1 0.552 1.155 01 1.652 2.243E 0C 1.643 7.30E-01 9.565 05 13.7311 2.46E-C1 1.257 1.466 01 0.575 2.243E 0C 1.464 8.94E-01 1.886 06 14.764 3.02EF-C1 0.573 1.466 01 0.575 2.243E 0C 1.464 8.94E-01 1.886 06 14.764 3.02EF-C1 0.573 1.466 01 0.575 2.243E 0C 1.464 8.94E-01 1.455 06 17.334 4.21E-C1 1.167 1.466 01 0.575 2.243E 0C 1.246 8	1.502 00	3.232	3.22E 0C	1.974	9.165-01	1.24E 05	16.934	1.556-01	0.036	
2.59E 00 2.412 2.52E 00 1.007 6.06E-01 1.76E 05 13.585 1.76E-01 0.004 3.00E 00 2.412 2.32E 00 1.775 6.07E-01 2.06E 05 12.763 1.01E-10 0.004 4.00E 00 2.414 2.32E 00 1.775 6.01E-01 2.42E 05 12.334 2.46E-01 0.114 4.00E 00 1.232 2.32E 00 1.518 7.04E-01 3.49E 05 12.309 2.7EE-01 0.114 4.50E 00 1.232 2.03E 00 1.344 7.56E-01 3.49E 05 12.309 2.7EE-01 0.211 5.00E 00 1.232 2.03E 00 1.344 7.56E-01 3.40E 05 12.309 2.7EE-01 0.211 5.00E 00 1.232 2.03E 00 1.344 7.56E-01 3.40E 05 12.309 2.7EE-01 0.211 5.00E 00 1.165 7.61E-01 1.159 6.102-01 3.40E 05 12.339 2.55E-01 0.211 6.00E 00 1.165 7.61E-01 1.159 6.102-01 3.40E 05 12.339 2.55E-01 0.211 7.00E 00 1.165 7.61E-01 1.159 6.102-01 1.484 05 2.339 2.55E-01 0.221 7.00E 00 1.4514 4.05E-01 1.230 1.59E-01 1.484 05 2.339 2.55E-01 7.225 7.00E 00 1.4514 2.337 2.65E-01 1.230 1.59E-01 1.42E 05 1.091 1.46E-01 7.276 8.00E 00 2.4337 2.65E-01 1.230 1.59E-01 1.426 05 4.6517 4.255 0.229 8.00E 00 2.4337 2.65E-01 1.230 1.59E-01 1.426 05 4.6517 4.255 0.229 8.00E 00 2.4337 2.65E-01 1.731 0.31E-01 7.68E 0.4 2.944 7.36E-02 0.329 9.00E 00 2.4363 7.14E-01 1.736 2.23E-01 2.03E 05 7.845 8.25E-02 0.357 9.00E 00 3.073 1.65E 00 1.411 4.49E-01 3.22E 05 9.225 1.000 1.345E-01 0.235 9.00E 00 3.073 1.65E 00 1.745 5.22E-01 0.1345E 00 1.345E-01 0.407 1.35E 01 2.447 2.03E 00 1.745 5.22E-01 0.1345E 01 1.246E 05 11.796 1.67E-01 0.35E 1.00E 01 3.073 1.65E 00 1.745 5.22E-01 0.1345E 01 1.047E-01 0.457E 1.35E 01 2.447 2.03E 00 1.745 5.22E-01 0.1345E 01 1.246E-01 1.346E 1.30E 01 3.073 1.65E 00 1.1745 5.22E-01 0.1345E 01 1.246E-01 1.347E 1.35E 01 2.457 2.457E 00 1.737 5.42E-01 1.246E 05 13.311 2.46E-01 7.751 1.35E 01 2.452 2.45E 00 1.463 7.30E-01 8.51E 05 12.754 2.23E-01 1.42E 1.45E 01 1.467 2.55E 02 1.463 8.94E-01 1.34E 06 14.764 3.02E-01 1.755 1.45E 01 0.467 2.55E 02 1.463 8.94E-01 1.34E 06 14.764 3.02E-01 1.347 1.46E 01 0.467 2.55E 01 1.465 8.494E-01 1.34E 06 14.764 3.02E-01 1.347 1.46E 01 0.467 2.55E 01 1.455 8.494E-01 1.34E 06 14.764 3.25E-01 1.428 1.46E 01 0.467 2.25E 00 1.254 8.94E-01 1.34E 0	2.00E 00	2.986	2.73E 00	1.979	7.396-01	1.50E 05	14.929	1.67E-C1	0.053	
3.00E 00 2.410 2.38E 0C 1.752 6.78E-01 2.06E 05 12.763 1.61E-01 0.056 4.00E 00 2.443 2.33E 0C 1.706 6.815-01 2.42E 05 12.354 2.62E-01 0.116 4.00E 00 1.233 2.03E 0C 1.618 7.44E-01 3.42E 05 12.309 2.78E-01 0.116 4.00E 00 1.233 2.03E 0C 1.344 7.54E-01 3.42E 05 11.329 3.55E-01 0.211 5.00E 00 1.233 2.03E 0C 1.344 7.54E-01 3.42E 05 11.329 3.55E-01 0.211 5.00E 00 1.235 1.455 0C 1.195 6.102-01 3.40E 05 7.904 4.5CE-01 7.255 6.00E 00 1.235 5.77E-01 1.195 6.102-01 1.846 05 7.904 4.5CE-01 7.255 6.00E 00 1.233 7.25E-01 1.195 6.102-01 1.846 05 7.904 4.5CE-01 7.255 6.00E 00 1.235 5.77E-01 1.195 6.102-01 1.846 05 7.904 4.5CE-01 7.255 7.00E 00 1.4614 4.55E-01 1.195 6.102-01 1.846 05 2.335 2.56E-01 7.267 7.00E 00 1.4614 2.337 2.65E-01 1.397 1.31E-01 7.66E 04 2.944 7.36CE-02 7.252 8.00E 00 2.337 2.65E-01 1.531 9.60E-02 7.056 4.4518 4.81E-02 7.255 9.00E 00 2.437 2.65E-01 1.531 9.60E-02 7.056 4.4518 4.81E-02 7.255 9.00E 00 3.603 4.75E-01 1.473 2.32E-01 2.038 05 7.845 8.22E-02 0.323 9.00E 00 3.605 1.22E 0C 1.791 3.342E-01 2.038 05 7.845 8.22E-02 0.323 9.00E 00 3.605 1.22E 0C 1.771 3.542E-01 2.038 05 7.845 8.22E-02 0.323 9.00E 00 3.605 1.22E 0C 1.773 5.42E-01 6.107 05 11.796 1.64F-01 0.467 1.756 01 3.607 1.63E 0C 1.735 5.42E-01 6.107 05 11.796 1.64F-01 0.467 1.756 01 2.267 2.31E 0C 1.773 5.42E-01 6.107 05 11.796 1.64F-01 0.467 1.756 01 2.222 2.31E 0C 1.773 5.42E-01 8.51E 05 10.606 1.34E-01 0.467 1.756 01 1.469 2.59E 0C 1.633 7.96E-01 9.56E 05 13.311 2.46E-01 0.467 1.756 01 1.469 2.59E 0C 1.633 7.96E-01 9.56E 05 13.311 2.46E-01 0.731 1.255 01 1.452 2.42E 0C 1.603 7.30E-01 9.56E 05 13.714 2.42E-01 0.475 1.355 01 1.452 2.42E 0C 1.562 7.96E-01 1.08E 06 14.764 3.02E-01 0.731 1.355 01 1.452 2.45E 0C 1.603 7.30E-01 1.86E 05 13.731 2.46E-01 0.731 1.355 01 1.452 2.45E 0C 1.563 7.96E-01 1.28E 06 13.731 2.46E-01 0.731 1.355 01 1.452 2.45E 0C 1.563 7.96E-01 1.28E 06 14.764 3.02E-01 0.731 1.355 01 1.452 2.45E 0C 1.603 7.30E-01 1.45E 06 16.224 3.74E-01 1.255 1.465 01 0.735 3.34E-01 1.36E 06 14.764 3.02E-01 1.452 1.465	2.50E 0C	2.782	2.52E 0C	1.907	6.965-01	1.76E 05	13.585	1.796-01	0.072	
3.50E 00 2.445 2.33E 0C 1.706 6.415-01 2.42E 05 12.354 2.62E-01 C.146 4.00E 00 2.161 2.37E 0C 1.638 7.23E-01 2.93E 05 12.391 2.35E-01 C.146 4.50E 00 1.232 2.33E 0C 1.518 7.24E-01 3.48E 05 12.309 2.75E-01 0.211 5.00E 00 1.233 2.03E 0C 1.344 7.54E-01 3.48E 05 11.329 3.55E-01 0.211 5.00E 00 1.233 2.03E 0C 1.344 7.54E-01 2.52E 05 4.083 4.27E+01 7.256 6.00E 0C 1.453 7.61E-01 1.195 6.102-01 3.40E 05 7.904 4.5CE-01 7.256 6.00E 0C 1.452 5.77E-01 1.195 6.102-01 2.48E 05 1.991 1.44E-01 7.256 7.00E 0C 1.451 7.5E-01 1.200 1.58E-01 2.52E 05 4.083 4.27E+01 7.256 7.00E 0C 1.451 7.5E-01 1.199 7.58E-01 1.426 75 1.991 1.44E-01 7.27E 7.00E 0C 1.454 7.3CE-01 1.439 1.316-01 7.68E 0.4 2.944 7.3CE-02 7.256 4.00E 0C 2.337 2.656-01 1.642 1.44E-01 1.24E 05 6.279 4.518 4.81E-02 7.256 7.00E 0C 2.337 2.656-11 1.631 7.46E-01 1.24E 05 6.279 4.53E-02 0.327 9.50E 0C 3.693 4.75E-01 1.643 1.44E-01 1.24E 05 6.279 4.53E-02 0.327 9.50E 0C 3.693 4.75E-01 1.643 1.44E-01 3.22E 05 9.325 1.CCE-01 7.356 1.00E 0 3.695 1.25E 0C 1.791 3.34E-01 3.22E 05 9.325 1.CCE-01 7.356 1.00E 0 3.695 1.25E 0C 1.791 5.3E2-01 4.65E 05 10.609 1.34E-01 7.456 1.00E 0 3.695 1.25E 0C 1.773 5.42E-01 4.55E 05 10.609 1.34E-01 7.456 1.00E 0 3.695 1.25E 0C 1.773 5.42E-01 4.55E 05 10.609 1.34E-01 7.456 1.00E 0 2.522 2.31E 0C 1.773 5.496-01 7.46E 05 12.342 1.67E-01 7.552 1.00E 01 2.522 2.31E 0C 1.735 5.496-01 7.46E 05 12.342 1.67E-01 7.552 1.15E 01 1.652 2.62E 0C 1.736 6.496-01 1.28E 06 14.164 2.73E-01 7.552 1.30E 01 1.34E 0C 1.603 7.66E-01 9.56E 05 13.311 2.46E-01 7.751 1.30E 01 1.246 00 1.254 7.55E 01 1.604 7.666 5.12.342 1.67E-01 7.552 1.30E 01 1.34E 0C 1.522 7.35E 0C 1.603 7.66E-01 9.55E 05 10.6024 1.34E-01 7.552 1.30E 01 1.34E 0C 1.645 7.646E-01 1.28E 06 14.164 2.73E-01 0.643 1.35E 01 1.652 2.62E 0C 1.542 7.56E-01 1.42E 06 15.553 3.35E-01 1.642 1.45E 01 0.241 7.55E 0C 1.793 7.66E-01 1.28E 06 14.764 7.67E-01 1.25C 1.55E 01 1.257 2.55E-01 1.452 7.55E-01 1.45E 06 14.745 7.5EE-01 1.427 1.66E 01 0.021 1.26E 0C 1.793 7.55E-01 1.45E 06 15.553 3.35E-01 1.46E	3.00E 00	2.610	2.38E 0C	1.752	6.785-01	2.06E 05	12.763	1.516-01	0.054	
4.00E C0 2.161 2.37E 0C 1.638 7.23E-01 2.93E 05 12.431 2.32E-01 C.14E 4.00E C0 1.722 2.32E 0C 1.518 7.64E-01 3.48E 05 12.309 2.7EE-C1 C.14E 5.00E 00 1.233 2.03E 0C 1.344 7.64E-01 3.48E 05 12.309 2.7EE-C1 0.211 5.00E 00 1.655 1.45E 0C 1.995 6.10E-01 3.48E 05 7.004 4.5EE-C1 0.224 6.50E 0C 1.655 1.45E 01 1.133 4.15E-01 2.63E 04 2.294E 0.264E 7.026 7.00E 0C 1.614 4.5EE-01 1.230 1.58E-01 1.12E 05 1.091 1.46E-C1 0.276 7.56E 0D 1.644 4.5EE-01 1.240 1.54E-01 2.24E 05 4.23E-02 0.261 9.00E 0C 2.633 7.34E-01 1.240 1.44E-01 2.24E 05 4.23E-02 0.261 9.00E 0C 2.633 7.34E-01 1.24E 03 5.22E 05 9.325 1.02E-01 0.267 9.00E 0C 2.647 2.03E 02	3.50E 00	2.445	2.328 00	1.706	6.815-01	2.42E 05	12 354	2.C4F-01	0.115	
4.50E CC 1.722 2.32E 0C 1.518 7.64E-01 3.49E 05 12.309 2.7EF-C1 0.1EC 5.00E 0C 1.233 2.03E 0C 1.344 7.54E-01 3.40E 05 11.299 3.55E-C1 0.211 6.00F 0C 1.163 7.61E-01 1.153 4.15E-01 2.52E 05 4.003 4.27E-C1 7.25E 7.00E 0C 1.644 4.03E-01 1.194 2.40E-01 1.48E 7.36E-C1 0.237 7.00E 0C 1.644 4.03E-01 1.53E-01 1.2252 1.991 1.46E-C1 7.27E 7.00E 0C 1.644 4.03E-01 1.53E-01 1.22E 05 4.991 1.44E-C1 7.27E 7.00E 0C 2.643 4.75E-01 1.649 1.44E-01 1.24E 05 6.279 6.23E-C2 0.028 7.00E 0C 2.643 4.75E-01 1.449=-01 1.24E 05 6.279 6.23E-C2 0.010 7.00E 0C 2.643 4.75E-01 1.649 1.44E-01 1.24E 05 6.279 6.23E-C2 0.101 7.00E 0C 2.658 7.74E-01 1.23E 0.10	4.90E CO	2.161	2+37E 0C	1.638	7.235-01	2.93E 05	12,431	2.3CF-01	C.14E	
5.000 1.233 1.234 1.244 7.244-01 3.924 05 11.229 3.554-01 0.211 5.505 00 1.055 1.465 00 1.195 6.102-01 3.942 05 11.229 3.554-01 0.211 5.505 00 1.055 1.465 00 1.195 6.102-01 3.942 05 4.0694 4.524-01 0.211 6.005 00 1.633 7.645 0.252 5.305 2.335 2.546-01 0.2267 7.305 00 1.644 4.055-01 1.339 1.016-01 7.686 2.944 7.306-02 0.282 8.005 00 2.337 2.656-01 1.631 9.069-02 7.356 4.518 4.818-02 0.282 9.005 00 2.963 7.34E-01 1.246 03 6.279 6.228-02 0.327 9.506 00 3.073 1.636 0.232-03 9.325 1.066-01 9.325 9.506 01 3.646-01 3.246-01 3.246 0.577-01 0.327	4.505 00	1.722	2 32E OF	1 51 9	7 665-01	3 495 06	12 200	1 205-01		
2.500 1.205 1.436 0.217 7.367 7.367 7.367 7.367 7.367 7.367 7.367 7.367 7.367 7.367 7.366 7.366 7.366 7.366 7.366 7.367 <td< td=""><td>5.00E 00</td><td>1.233</td><td>2030 00</td><td>1 244</td><td>7.645-01</td><td>3 035 A5</td><td>12+307</td><td>2. Jer-U!</td><td>0.180</td><td></td></td<>	5.00E 00	1.233	2030 00	1 244	7.645-01	3 035 A5	12+307	2. Jer-U!	0.180	
2.001 1.003 1.003 1.003 1.003 1.004 4.004 4.004 4.004 4.004 0.226 Table 8, page 1 6.005 001 1.252 5.772-31 1.193 4.155-01 2.525 0.005 0.233 2.646-01 7.266 7.266 7.366 0.1614 4.055-01 1.230 1.535-01 1.126 0.516 1.4846 95 2.335 2.646-01 7.276 7.366 0.233 7.366 0.2337 2.665-01 1.531 9.696-02 7.695 0.4 4.516 4.518 4.616-02 0.246 0.01 9.325 0.01 9.325 0.01 9.325 0.01 9.327 0.01 9.327 0.01 9.327 0.01 9.327 0.01 9.327 0.01 9.325 1.004-01 1.246 0.5 0.236 1.327 0.327 0.327 0.327 0.327 0.327 0.327 0.327 0.327 0.327 0.327 0.326 0.228 0.325 0.228 0.325 0.228 0.325 0.228 0.325 0.228 0.325 0.228 <	5 505 10	1 055	2.00 DC 1.645 00	1.105	7.548-01	3.82E US	11.329	3.552-01	9.211	
0.000 1.000 7.612-01 1.100 2.021 0.000 4.000 4.221-01 2.242 05 4.000 4.000 4.221-01 2.242 05 4.000	5,000 00		1.400 00	1.195	6.102-01	3.40E 05	7.904	4.5CE-C1	0.236	Table 8, page 1
0.0001.3225.72=311.1962.305=011.3465.3352.44E-010.7677.30E 0C1.6144.05E-011.2301.58E-011.12E 051.9911.44E-017.2767.50E 0C2.3372.66E-011.319.69E-027.68E 342.9447.35E-020.2828.00E 0C2.3637.14E-011.646-011.24E 056.2796.23E-020.3019.00E 0C2.9637.14E-011.6762.23E-012.03E 057.8458.25E-020.3219.50E 0C3.0951.21E 0C1.7913.34E-013.22E 059.3251.00E-010.4071.05E 012.4672.03E 021.7355.32E-010.4061.34F-010.4071.05E 012.4672.03E 021.7355.32E-016.1096 0512.3421.67F-010.4071.05E 012.4272.03E 021.7236.69E-017.46E 0512.3421.67F-010.4671.15E 012.5222.31E 021.6637.30E-018.51E 0513.3112.46E-010.4631.20E 011.6622.62E 021.6637.30E-011.08E 0614.1642.72F-010.4321.35E 011.6522.62E 021.6438.94E-011.28E 0616.2243.74E-011.14E1.35E 011.0272.57F0.14579.56E-011.48E 0616.2243.74E-011.24E1.35E 011.0272.57F0.14579.56E-011.48E 0616.2243.74	6.00E UC	1.00	3+61E-01	1.159	4.158-01	2.5ZE 05	4.083	4.208-01	0.254	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.50E UC	L.252	5.70E-01	1.196	2.805-01	1.845 05	2.335	2.54E-C1	0.267	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	7.90E 0C	1.614	4.05E-01	1.280	1.585-01	1.12E 05	1.991	1.465-01	7.276	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	7.50E 00	1.948	2.83E-01	1.399	1.01E-01	7.688 04	2.944	7.305-02	0.282	
a, 50E 00 $2, 693$ $4, 75E-01$ $1, 643$ $1, 44E-01$ $1, 24E 05$ $6, 2759$ $6, 32E-02$ $0, 301$ $9, 50E 00$ $2, 663$ $7, 74E-01$ $1, 776$ $2, 23E-01$ $2, 03E 05$ $7, 845$ $E, 22E-C2$ $0, 327$ $9, 50E 00$ $3, 073$ $1, 26E 00$ $1, 771$ $3, 34E-01$ $3, 22E 05$ $9, 325$ $1, CCE-C1$ $0, 366$ $1, 05E 01$ $2, 647$ $2, 03E 00$ $1, 773$ $5, 82E-01$ $6, 19E 05$ $11, 796$ $1, 67E-01$ $0, 467$ $1, 05E 01$ $2, 522$ $2, 31E 00$ $1, 773$ $5, 82E-01$ $6, 19E 05$ $11, 796$ $1, 67E-01$ $0, 467$ $1, 15E 01$ $2, 522$ $2, 31E 00$ $1, 773$ $6, 49E-01$ $9, 56E 05$ $13, 311$ $2, 46E-01$ $0, 552$ $1, 15E 01$ $2, 522$ $2, 41E 01$ $1, 663$ $7, 36E-01$ $9, 56E 05$ $13, 311$ $2, 46E-01$ $0, 791$ $1, 25E 01$ $1, 663$ $7, 86E-01$ $9, 56E 05$ $13, 311$ $2, 46E-01$ $0, 791$ $1, 25E 01$ $1, 662$ $2, 62E 00$ $1, 463$ $8, 94E-01$ $1, 28E 06$ $14, 764$ $3, 22E-01$ $0, 924$ $1, 30E 01$ $1, 246$ $1, 262$ $0, 25E-01$ $1, 284$ $0, 34E-01$ $1, 28E 04$ $1, 24E-01$ $0, 924$ $1, 30E 01$ $1, 24E 03$ $1, 448$ $3, 34E-01$ $1, 286 06$ $16, 224$ $3, 145-01$ $1, 148$ $1, 40E 01$ $0, 735$ $2, 46E 00$ $1, 284$ $7, 56E-01$ $1, 286 06$ $16, 224$	8.00E 00	2.337	2.66E-01	1,531	9.69E-02	7.05E 04	4.518	4.815+02	0.269	
9.00E002.9637.74E-011.7362.23E-012.03E 057.8458.25E-020.3279.50E003.0731.63E001.8114.49E-013.22E059.3251.00E-010.4071.00E013.0731.63E001.8114.49E-014.55E0510.6061.34F-010.4071.05E012.8872.08E001.7755.82E-016.19E0511.7961.67E-010.4071.00E012.5222.31E001.7736.64E-017.46E0512.3421.67E-010.4071.15E012.5222.31E001.6637.30E-018.51E0512.7542.23E-010.66361.20E011.9692.53E0.01.6637.30E-018.51E0513.3112.46E-010.7311.25E011.6522.62E021.4638.94E-011.98E0614.1642.72E-010.4321.35E011.6422.57E021.4638.94E-011.28E0615.5533.35E-011.0421.35E010.4962.29E001.2847.56E-011.36E0616.2243.14E-011.14E1.45E010.4962.29E021.4627.56E-011.3555.2EE-011.2471.45E010.4962.29E001.999.55E-011.45E0616.7454.1EE-01 <td>8.50E 00</td> <td>2.698</td> <td>4.758-01</td> <td>1.649</td> <td>1.44E-01</td> <td>1.24E 05</td> <td>6.279</td> <td>A 335-02</td> <td>0.301</td> <td></td>	8.50E 00	2.698	4.758-01	1.649	1.44E-01	1.24E 05	6.279	A 335-02	0.301	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	9.00E 00	2.963	7.74E-01	1.736	2.235-01	2.03E 35	7 845	0.25E-C2	0.322	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	9.50E 00	3,695	1.216.00	1 791	3 345-01	3 335 05	0 225	1 665 61	0.25/	
1.35E 01 2.447 2.03E 0.0 1.735 5.82E-01 6.19E 05 11.376 1.647-01 0.4474 1.10E 01 2.522 2.31E 0.0 1.723 6.69E-01 7.46E 05 12.342 1.67E-01 0.474 1.15E 01 2.232 2.43E 0.0 1.663 7.30E-01 8.51E 05 12.754 2.23F-01 0.636 1.20E 01 1.969 2.53E 0.0 1.663 7.30E-01 9.56E 05 13.311 2.46E-01 0.437 1.25E 01 1.652 2.62E 0.0 1.5643 8.94E-01 1.18E 06 14.164 2.73E-01 0.934 1.30E 01 1.341 2.62E 0.0 1.463 8.94E-01 1.18E 06 14.764 0.0224 0.934 1.30E 01 1.027 2.57E 0.0 1.378 9.34E-01 1.28E 06 15.553 3.35E-01 1.642 1.46E 01 0.496 2.19E 0.0 1.284 7.56E-01 1.45E 06 17.334 4.67E-01 1.242 1.45E 01 0.496 2.19E 0.0 1.999 9.55E-01 1.45E 06 17.334 4.67E-01 1.247 1	1.00E 01	3.073	1 435 00	1 011	5.542-01	3.22E 09 A EEE 05	9.327	1.345.01	0.000	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1.056 01	2 467		1.705	4.492-01	4.000 00	10 000	1.345-01	0.407	
1.15E 01 2.232 2.43E 0C 1.723 6.89E-01 7.46E 05 12.442 1.97E-01 7.552 1.15E 01 2.232 2.43E 0C 1.663 7.30E-01 8.51E 05 12.754 2.23E-01 6.63E 1.20E 01 1.969 2.53E 0C 1.603 7.86E-01 9.56E 05 13.311 2.46E-01 0.731 1.30E 01 1.341 2.62E 0C 1.542 8.51E-01 1.08E 06 14.164 2.73E-01 0.432 1.30E 01 1.341 2.62E 0C 1.463 8.94E-01 1.18E 06 14.764 3.02E-01 0.934 1.35E 01 1.027 2.57E 0C 1.378 9.34E-01 1.28E 06 15.553 3.35E-01 1.643 1.40E 01 9.735 2.46E 00 1.284 7.56E-01 1.36E 06 16.745 4.1EE-01 1.14E 1.45E 01 0.496 2.29E 0C 1.199 9.55E-01 1.45E 06 17.334 4.67E-01 1.44E 1.45E 01 0.496 2.99E 02 1.999 9.38E-01 1.47E 06 17.955 5.26E-01 1.427 <td< td=""><td>1. TOE 01</td><td>2 6 2 7</td><td>2.000 00</td><td>1.737</td><td>5.82E-01</td><td>6.19E UD</td><td>11.796</td><td>1.0/0-01</td><td>0.474</td><td></td></td<>	1. TOE 01	2 6 2 7	2.000 00	1.737	5.82E-01	6.19E UD	11.796	1.0/0-01	0.474	
1.20E 01 1.432 2.43E 0C 1.603 7.30E-01 8.51E 05 12.754 2.23E-01 C.644 1.20E 01 1.969 2.53E 0C 1.603 7.86E-01 9.56E 05 13.311 2.46E-C1 0.731 1.30E 01 1.652 2.62E 0C 1.542 8.51E-01 1.08E 06 14.164 2.72E-01 C.632 1.30E 01 1.341 2.62E 0C 1.463 8.94E-01 1.18E 06 14.764 3.02E-01 0.934 1.35E 01 1.027 2.57E 0C 1.378 9.34E-01 1.286 06 15.553 3.35E-01 1.642 1.40E 01 9.735 2.46E 00 1.284 7.56E-01 1.36E 06 16.745 4.18E-01 1.25C 1.40E 01 0.496 2.29E 0C 1.191 9.60E-01 1.41E 06 16.745 4.18E-01 1.25C 1.55E 01 0.496 2.19E 0C 1.099 9.55E-01 1.45E 06 17.334 4.67E-01 1.347 1.60E 01 0.131 1.89E 00 1.095 9.38E-01 1.47E 06 17.955 5.26E-01 1.427 <td< td=""><td>1 156 01</td><td>2022</td><td>2.310 00</td><td>2.123</td><td>6.696-01</td><td>7.46E 05</td><td>12.342</td><td>1.976-01</td><td>0.552</td><td></td></td<>	1 156 01	2022	2.310 00	2.123	6.696-01	7.46E 05	12.342	1.976-01	0.552	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10170 91		2.436 90	1.003	7.308-01	8.51E 05	12.754	2.23E-01	6.636	
1.455 01 1.652 2.62E 0C 1.542 8.51E-01 1.08E 06 14.164 2.73E-01 0.632 1.30E 01 1.341 2.62E 0C 1.463 8.94E-01 1.18E 06 14.764 3.02E-01 0.934 1.35E 01 1.027 2.57E 0C 1.378 9.34E-01 1.286 06 15.553 3.35E-01 1.043 1.40E 01 0.496 2.29E 0C 1.284 7.56E-01 1.36E 06 16.745 4.16E-01 1.14E 1.45E 01 0.496 2.29E 0C 1.099 2.55E-01 1.36E 06 16.745 4.16E-01 1.347 1.55E 01 0.496 2.29E 0C 1.099 2.55E-01 1.45E 06 17.334 4.67E-01 1.347 1.55E 01 0.131 1.89E 02 1.099 2.55E-01 1.45E 06 17.334 4.67E-01 1.437 1.60E 01 0.139 3.25E-01 0.733 6.31E-01 1.4	1.20E 01	1.969	2.53E 00	1.603	7.86E-01	9.56E 05	13.311	2.46E-C1	0.731	
1.30E 01 1.341 2.42E 00 1.463 8.94E-01 1.18E 06 14.764 3.02E-01 0.934 1.35E 01 1.027 2.57E 00 1.378 9.34E-01 1.28E 06 15.553 3.35E-01 1.043 1.40E 01 0.735 2.46E 00 1.284 3.56E-01 1.36E 06 16.224 3.74E-01 1.14E 1.40E 01 0.496 2.29E 00 1.191 9.60E-01 1.41E 06 16.745 4.1EE-01 1.250 1.50E 01 0.496 2.29E 00 1.099 0.55E-01 1.45E 06 17.334 4.67E-01 1.347 1.55E 01 0.131 1.89E 00 1.005 9.38E-01 1.47E 06 17.955 5.2EE-01 1.437 1.60E 01 0.139 3.25E-01 0.733 6.31E-01 1.46E 06 18.490 6.10E-01 1.517 1.80E 01 0.139 3.25E-01 0.707 4.51E-01 9.14E 05 9.286 1.29E 00 1.97E 2.00E 01 0.296 6.38E-01 0.707 4.51E-01 7.03E 05 5.439 1.13E 00 2.023 2	1.25E 01	1.652	2.62E 0C	1.542	8.518-01	1.08E 06	14.164	2.735-01	0.632	
1.35E 011.0272.57E 0C1.378 $9.34E-01$ 1.28E 0615.553 $3.3EE-01$ 1.C431.40E 01 9.735 $2.46E 0C$ 1.284 $9.56E-01$ $1.36E 06$ 16.224 $3.74E-01$ $1.14E$ 1.45E 01 0.496 $2.29E 0C$ 1.191 $9.60E-01$ $1.41E 06$ 16.745 $4.1EE-01$ $1.25C$ 1.50E 01 0.256 $2.10E 0C$ 1.099 $9.55E-01$ $1.45E 06$ 17.334 $4.67E-01$ 1.347 1.55E 01 0.131 $1.89E 00$ 1.009 $9.55E-01$ $1.45E 06$ 17.955 $5.2EE-01$ 1.437 1.60E 01 0.009 $1.64E 9C$ 7.908 $9.38E-01$ $1.46E 06$ 18.490 $6.10E-01$ 1.517 1.80E 01 0.139 $3.25E-01$ 0.733 $6.31E-01$ $1.15E 06$ 13.795 $1.26E 0C$ $1.87E$ 2.00E 01 0.296 $6.39E-01$ 0.707 $4.51E-01$ $9.14E 05$ 9.286 $1.25E 0C$ $1.87E$ 2.00E 01 0.441 $4.61E-01$ 0.707 $4.51E-01$ $9.14E 05$ 9.286 $1.25E 0C$ $1.87E$ 2.40E 01 0.531 $3.94E-01$ 0.772 $2.55E-01$ $6.20E 05$ 3.645 $9.00E-01$ 2.115 2.40E 01 0.531 $3.94E-01$ 0.772 $2.55E-01$ $6.20E 05$ 3.6455 $9.00E-01$ 2.224 2.40E 01 0.587 $3.29E-01$ 0.774 $2.07E-01$ $5.45E 05$ 2.622 $7.22E-01$ 2.224 2.805 01 0.638 $2.71E-0$	1.30E 01	1.341	2.62E 00	1.463	8.94E-01	1.18E 06	14.764	3.026-01	0.934	
1.40E 01 9.735 $2.46E 00$ 1.284 $7.56E-01$ $1.36E 06$ 16.224 $3.74E-01$ $1.14E$ $1.45E 01$ 0.496 $2.29E 00$ 1.191 $9.60E-01$ $1.41E 06$ 16.745 $4.1EE-01$ 1.250 $1.50E 01$ 0.296 $2.10E 00$ 1.099 $9.55E-01$ $1.45E 06$ 17.334 $4.67E-01$ 1.347 $1.55E 01$ 0.131 $1.89E 00$ 1.099 $9.55E-01$ $1.45E 06$ 17.334 $4.67E-01$ 1.347 $1.55E 01$ 0.131 $1.89E 00$ 1.005 $9.38E-01$ $1.47E 06$ 17.955 $5.2EE-01$ 1.427 $1.60E 01$ 0.139 $7.25E-01$ 0.733 $6.31E-01$ $1.46E 06$ 18.490 $6.10E-01$ 1.517 $1.80E 01$ 0.139 $7.25E-01$ 0.707 $4.51E-01$ $9.14E 05$ 9.286 $1.25E 00$ $1.97E$ $2.00E 01$ 0.296 $6.38E-01$ 0.707 $4.51E-01$ $9.14E 05$ 9.286 $1.25E 00$ $1.97E$ $2.20E 01$ 0.441 $4.61E-01$ 0.772 $2.55E-01$ $6.20E 05$ 5.439 $1.12E 00$ 2.003 $2.40E 01$ 0.531 $3.94E-01$ 0.772 $2.55E-01$ $6.20E 05$ 3.6455 $9.00E-01$ 2.224 $2.60E 01$ 0.587 $3.29E-01$ 0.774 $2.07E-01$ $5.45E 05$ 2.622 $7.22E-01$ 2.224 $2.805 01$ 0.638 $2.71E-01$ 0.794 $2.07E-01$ $5.45E 05$ 2.622 $7.22E-01$ 2.217 <td>1.35E Ol</td> <td>1.027</td> <td>2.57E 00</td> <td>1.378</td> <td>9.345-01</td> <td>1.28E 06</td> <td>15 553</td> <td>3.356-01</td> <td>1.047</td> <td></td>	1.35E Ol	1.027	2.57E 00	1.378	9.345-01	1.28E 06	15 553	3.356-01	1.047	
1.45E 01 0.496 2.29E 0C 1.191 9.60E-01 1.41E 06 16.745 4.1EE-01 1.25C 1.50E 01 0.256 2.10E 0C 1.099 9.55E-01 1.45E 06 17.334 4.67E-01 1.347 1.55E 01 0.131 1.89E 00 1.005 9.38E-01 1.47E 06 17.955 5.2EE-01 1.437 1.60E 01 0.009 1.64E 90 0.993 3.03E-01 1.46E 06 18.490 6.10E-01 1.517 1.80E 01 0.139 3.25E-01 0.733 6.31E-01 1.15E 06 13.795 1.06E 0C 1.972 2.00E 01 0.296 6.39E-01 0.707 4.51E-01 9.14E 05 9.286 1.25E 0C 1.87E 2.20E 01 0.441 4.61E-01 0.735 3.14E-01 7.00E 05 5.439 1.12E 0C 2.003 2.40E 01 0.531 3.94E-01 0.772 2.55E-01 6.20E 05 3.645 9.00E-01 2.115 2.60E 01 0.587 3.29E-01 0.774 2.07E-01 5.45E 05 2.622 7.26E-01 2.224 2.8	1.40E 01	0.735	2.46E 00	1.284	3.56E-01	1.36E 06	16.224	3.745-01	1.14E	
1.502 0.174 0.002 1.171 0.00201 1.412 0.002 1.412 0.16.745 4.1257 1.250 1.502 0.131 1.892 00 1.099 0.555-01 1.452 06 17.334 4.67E-01 1.347 1.555 0.131 1.892 00 1.095 9.38E-01 1.472 06 17.955 5.26E-01 1.437 1.605 0.009 1.64E 00 0.908 9.03E-01 1.46E 06 18.490 6.10E-01 1.517 1.805 01 0.139 9.25E-01 0.733 6.31E-01 1.15E 06 13.795 1.06E 00 1.722 2.005 01 0.441 4.61E-01 0.735 3.14E-01 7.00E 9.286 1.25E 00 1.876 2.405 01 0.531 3.94E-01 0.772 2.55E-01 6.20E 0.5439 1.12E 00 2.003 2.605 01 0.531 3.94E-01 0.772 2.55E-01 6.20E 0.5455 9.00E-01 2.115	1.458 01	0.496	2.29E ar	1 101	9 605-01	1 415 04	14 745	4 105 01	1 250	
1.55E 0.131 1.89E 00 1.999 9.55E-01 1.45E 06 17.334 4.67E-01 1.347 1.55E 0.131 1.89E 00 1.005 9.38E-01 1.47E 06 17.955 5.22E-01 1.437 1.66E 0.0079 1.64E 00 0.903 9.03E-01 1.46E 06 17.955 5.22E-01 1.437 1.80E 01 0.139 7.25E-01 0.733 6.31E-01 1.46E 06 18.490 6.10E-01 1.517 1.80E 01 0.139 7.25E-01 0.707 4.51E-01 9.14E 05 9.286 1.25E 0C 1.87E 2.00E 01 0.296 6.38E-01 0.707 4.51E-01 9.14E 05 9.286 1.25E 0C 1.87E 2.20E 01 0.441 4.61E-01 0.735 3.14E-01 7.03E 9.5439 1.13E 0C 2.003 2.40E 01 0.531 3.94E-01 0.772 2.55E-01 6.20E 3.6455 9.00E-01 2.118	1.505 01	1.764	2 1 1E AA	1.000	7.0UE-UI	1.4418 00	10.(4)	4.188-01	1 250	
1.60E 0.101 1.60E 00 1.60E 9.38E=01 1.47E 06 17.955 5.2EE=01 1.437 1.60E 0.009 1.64E 00 0.908 9.08E=01 1.46E 06 18.490 6.10E=01 1.517 1.80E 01 0.139 9.25E=01 0.733 6.31E=01 1.15E 06 13.795 1.06E 00 1.722 2.00E 01 0.296 6.39E=01 0.707 4.51E=01 9.14E 05 9.286 1.25E 00 1.87E 2.00E 01 0.441 4.61E=01 0.735 3.14E=01 7.00E 05 5.439 1.13E 00 2.003 2.40E 01 0.531 3.94E=01 0.772 2.55E=01 6.20E 05 3.6455 9.00E=01 2.116 2.60E 01 0.537 3.29E=01 0.774 2.07E=01 5.45E 05 2.6622 7.26E=01 2.224 2.80E 01 0.638 2.71E=01 0.816 1.66E=01 4.71E 05 1.850 5.44E=01 <td>3.55F 01</td> <td>J. 270 A 171</td> <td>1 005 00</td> <td>1:399</td> <td>9.75E-UL</td> <td>1.402 06</td> <td>17+534</td> <td>4.c/E-01</td> <td>1.347</td> <td></td>	3.55F 01	J. 270 A 171	1 005 00	1:399	9.75E-UL	1.402 06	17+534	4.c/E-01	1.347	
1.001 01 0.003 1.041 30 9.993 9.031-01 1.465 36 18.490 6.101-01 1.517 1.805 01 0.139 9.250-01 0.733 6.310-01 1.150 06 13.795 1.065 00 1.722 2.005 01 0.296 6.390-01 0.707 4.510-01 9.140 05 9.286 1.250 00 1.976 2.005 01 0.441 4.610-01 0.735 3.140-01 7.000 95 5.439 1.130 00 2.003 2.405 01 0.531 3.540-01 0.772 2.550-01 6.200 55 3.6455 9.000-01 2.115 2.605 01 0.587 3.290-01 0.774 2.070-01 5.450 5.420 7.200-01 2.317 2.805 01 0.638 2.710-01 0.916 1.660-01 4.716 05 1.850 5.440-01 2.317	1 405 01	V.131 0.000	1.89E 00	1. 105	9.38±-01	1.47E 06	17.955	5.2EE-C1	1.437	
1:00: 01 0:139 9:25E-01 0:733 6:31E-01 1:15E 06 13:795 1:06E 00 1:722 2:00E 01 0:296 6:38E-01 0:707 4:51E-01 9:14E 05 9:286 1:25E 00 1:876 2:00E 01 0:441 4:61E-01 0:735 3:14E-01 7:00E 05 5:439 1:13E 00 2:003 2:40E 01 0:531 3:54E-01 0:772 2:55E-01 6:20E 05 3:645 9:00E-01 2:115 2:60E 01 0:587 3:29E-01 0:774 2:07E-01 5:45E 05 2:622 7:26E-01 2:224 2:80E 01 0:638 2:71E-01 0:816 1:66E-01 4:71E 05 1:850 5:44E-01 2:317	1 anr 01	0.000	1.046 90	0.908	9.03E-01	1.46E 06	18.470	6.1CE+01	1.517	
2.00E 01 0.296 6.39E-01 0.707 4.51E-01 9.14E 05 9.286 1.25E 0C 1.97E 2.20E 01 0.441 4.61E-01 0.735 3.14E-01 7.00E 05 5.439 1.13E 0C 2.003 2.40E 01 0.531 3.54E-01 0.772 2.55E-01 6.20E 05 3.6455 9.00E-01 2.115 2.60E 01 0.587 3.29E-01 0.774 2.07E-01 5.45E 05 2.622 7.26E-01 2.224 2.80E 01 0.638 2.71E-01 0.816 1.66E-01 4.71E 05 1.850 5.44F-01 2.317	THOOF OI	N•138	9+25E-01	9.733	6.31E-01	1.15E 06	13.795	1.065 00	1.722	
2.20E 01 0.441 4.61E=01 0.735 3.14E=01 7.00E 05 5.439 1.13E 0C 2.0C3 2.40E 01 0.531 3.94E=01 0.772 2.55E=01 6.20E 05 3.645 9.0CE=01 2.119 2.60E 01 0.587 3.29E=01 0.794 2.07E=01 5.45E 05 2.622 7.26E=01 2.224 2.80E 01 0.638 2.71E=01 0.816 1.66E=01 4.71E 05 1.850 5.64F=01 2.317	2.00E 01	0.296	6.38E-01	0.707	4.51E-01	9.14E 05	9.286	1.29E 0C	1.878	
2.40E 01 0.531 3.94E-01 0.772 2.55E-01 6.20E 05 3.645 9.00E-01 2.119 2.60E 01 0.587 3.29E-01 0.794 2.07E-01 5.45E 05 2.622 7.26E-01 2.224 2.80E 01 0.638 2.71E-01 0.816 1.66E-01 4.71E 05 1.850 5.64E-01 2.317	2.208 01	0.441	4.61E-01	3.735	3.14E=01	7.00E 05	5,439	1.13E CC	2.003	
2.60E 01 0.587 3.29E-01 0.794 2.07E-01 5.45E 05 2.622 7.26E-01 2.224 2.80E 01 0.638 2.71E-01 0.816 1.66E-01 4.71E 05 1.850 5.64E-01 2.317	2.40E 01	0.531	3.946-01	0.772	2.556-01	6.20E 05	3 645	9.CCE-C1	2.115	
2.805 01 0.638 2.715-01 0.816 1.665-01 4.715 05 1.850 5.445-01 2.317	2.60E 01	0.587	3.29E-01	0.794	2.07E-01	5.45F 05	2 622	7.265-01	2.774	
	2.80E 01	0.638	2.71E-01	0.816	1.66E-01	4.715 05	1.850	5.64E-01	2.317	

.

• и

NPTICAL CONSTANTS OF C

N-EFF 2.463 2.463 2.562 2.562 2.641 2.112 2.776 2.837 2.655 2.555 3.061 3.171 3.264 3.34C 3.45C 3.566 3.566 3.566 3.662 3.652 3.7C6 3.745 3.745 3.756 3.617 3.617 3.975 4.744 5.276 5.432 5.625 5.8655 5.8655 5.963 6.062 6.053 6.115 6.132 4.103 4.441 4.655 4.654 6.136 6.137 6.135 6.135 6.135 EN EP GYLD SS 4.525-C1 3.616-01 3.186-01 2.535-01 2.456-01 8.615-02 6.486-02 4.705-02 3.445-02 2.735-02 2.CZF-C1 1.74E-01 1.65E-01 1.51E-C1 1.14E-01 2.275-02 1.886-02 1.586-02 1.326-02 1.326-02 7.56F-03 5.56E-03 4.896E-03 3.996E-03 3.996E-03 3.996E-03 3.996E-03 3.996E-03 1.736-03 1.156-03 5.486-04 4.146-04 1.566-04 7.036-03 9.576-03 7.416-03 5.586-03 4.756-03 4.3CE-03 1.69E-03 6.66E-04 1.57E-04 8.45E-05 1.72E-05 4.81E-05 8.55E-07 1.008F-07 2.67E-0E 1.0CE-CE 1.44E-05 4.35E-10 4.35E-10 ECT? 1.360 0.994 0.799 0.710 0.590 0.465 0.370 0.325 0.294 0.155 0.114 0.083 0.059 0.043 0.004 0.004 0.004 0.003 0.003 0.033 0.026 0.020 0.015 0.013 0.001 0.000 0.000 0.000 0.000 0.0000 0.000.0 REFL 00000 00000 022005 00000 BSCCEFF 00000 44444 44444 44664 00000 9.45E 00 4.54E 00 1.09E 00 4.38E-01 1.00E-01 44440 00003 4.26E 3.83E 3.76E 3.72E 3.31E 2.96E 2.77E 2.81E 2.81E 2.70E 1.95E 1.64E 1.32E 1.06E 9.21E 8.29E 7.38E 6.61E 5.89E 5.25E .19E .43E .09E .72E 1.54E 1.17E 6.79E 5.53E 2.34E .08E .56E .19E .25E 7.56E 3.78E 2.83E 1.91E 7.87E 4.13E 1.29E 4.30E 1.36E 2.72E 1.40E-01 1.18E-01 1.09E-01 1.02E-01 3.60E-02 7.30E-02 6.50E-02 6.30E-02 5.30E-02 5.30E-02 3.50E-02 2.70E-02 2.30E-02 1.50E-02 1.21E-02 1.02E-02 8.58E-03 7.25E-03 6.13E-03 5.19E-03 3.77E-03 2.82E-03 2.35E-03 2.35E-03 1.93E-03 1.93E-03 1.21E-03 8.48E-04 5.85E-04 2.72E-04 2.06E-04 7.94E-04 3.54E-03 4.97E-03 3.68E-03 2.77E-03 2.77E-03 2.36E-03 2.135-03 8.396-04 5.696-04 3.326-04 3.856-04 4.22E-05 8.62E-06 2.41E-06 4.48E-07 5.38E-08 1.34E-08 5.00E-09 7.20E-10 2.17E-10 3.29E-11 0.8873 0.873 0.873 0.873 0.873 7.973 7.974 7.911 0.914 0.932 0.948 0.948 0.955 0.961 0.966 C.973 0.973 0.973 2.978 0.982 0.987 0.987 0.987 0.987 0.994 0.998 0.998 0.998 1.001 1.002 0.999 0.998 0.998 0.998 0.999 9.999 0.999 0.999 0.999 1.000 0000-1 2.346-01 2.026-01 1.936-01 1.796-01 1.137E-01 1.135E-01 1.155E-01 1.55E-01 8.37E-02 6.53E-02 5.03E-02 3.79E-02 2.96E-02 2.33E-02 1. 93E-92 1. 65E-92 1. 41E-92 1. 21E-92 1. 21E-92 7.476-03 5.556-03 4.556-03 3.916-03 3.916-03 1.69E-03 1.16E-03 5.43E-04 4.12E-04 1.59E-03 SILON 2 7.096-03 9.936-03 7.356-03 5.526-03 4.736-03 4.26E-03 1.67E-03 1.14E-03 6.63E-04 1.57E-04 3.44E-05 1.72E-05 4.91E-06 3.95E-07 1.03E-07 2.67E-0E 1.07E-0E 1.44E-09 4.35E-1C 6.53E-11 0 EPS TLON 0.750 0.750 0.750 0.750 7.793 7.813 7.826 7.932 7.932 0.884 0.893 0.893 0.893 0.893 0.893 0.933 0.933 0.946 0.552 0.552 7.564 0.575 7.573 7.584 0.9983 0.996 0.999 7.999 1.004 0.9997 0.9997 0.9997 0.9997 1.000 1.000 100010 88825 00000 55555 00000 NNNNN ENERGY NNNNN 000000 00000 000000 3.20E 3.40E 3.40E 5.50E 6.50E 7.00E 7.50E 8.705 8.505 9.006 9.505 1.005 4.20F 4.40E 5.30F .105 .305 .405 2.905 2.506 2.506 2.906 3.205 3.205 3.205 3.405 3.50E 4.50E 5.00E 8.00E 1.00E 1.50E 2.00E 3.00E 7.00E 9.00E 1.50E 2.00E 3.00E

8, page 2

Table

OPTICAL CONSTANTS OF AL2C3

ENEP GY	EPSILONI	EPSILCN2	N	ĸ	ABSCOEFF	REFLECTS	ENERGYLOSS	N-EFF	
6.COE 00	3.155	8. 5CE-03	1.774	2.20E-03	1.57E 03	7.794	6.14E-04	0,002	
7.00F 00	3.704	3-18E=02	1.924	8-24F-03	5.87E 03	9,993	2.305-03	0.007	
S CCE NO	4.236	1.165-01	2.058	2-80E-02	2.29E 04	11.976	6.345-03	0.022	
9.5CE 00	4-636	2. C6E-01	2,153	4-78E-02	4.1°F 04	13.397	9.49F-03	0.040	
9.005 00	5,268	4.12E-01	2.297	8.95E-02	8.17E 04	15.537	1.475-02	0,077	
9. 50E 00	6.304	1.28F (0	2.524	2.53F-01	2.44E 05	19.120	3.07F-02	0.160	
1.035.01	6.308	3. CAE CO	2.582	5-97F-C1	6.05E 05	21.680	6-26F-02	0.445	
1.055 01	5-265	4.72E 00	2.484	9.516-01	1.01E 06	27.833	9. 43F- 02	0.925	
1.10E 01	3-688	4.525 00	2.219	1-115 00	1.24F 06	23.449	1.305-01	1.523	
1.15E 01	2.731	4.66E CO	2.017	1.165 00	1.35E 06	22.723	1.605-01	2.124	
1 20F 01	2, 133	4.34F CO	1.868	1.17E 00	1.42E 06	22.036	1-85E-01	2.711	
1 255 01	1.702	6 105 00	1 762	1 175 00	1 695 06	21.660	2 095-01	7.295	
1 205 01	1 267	3 875 00	1 440	1 175 00	1 666 06	21 616	2 216-01	2 940	
1 350 01	1.053		1+044		1.570 00	21.4417	2.515-01	4 300	
1.07 01	1.000	2.02E 00	1.222	1+115 00	140UC UQ	21.207	20 245701	4	
14 HUE 01	0.009	3843E VV	1+411	1.105 00	1.075 00	21+147	2. 105-01	4.421	
1.45E 01	0.553	3.2CE 00	1.379	1.16E CO	1.70E 06	21.254	3.035-01	5.460	
1.50E 01	C. 379	2.94E CO	1.293	1.14E 00	1.735 06	21.065	3.34E-01	5.960	
1.678 11	0.165	2.47F CC	1.148	1.075 00	1.74E 06	20.376	4.045-01	6.877	
1,70E 01	0.077	2.075.00	1.035	9.975-01	1.725 06	19.337	4. 84E- C1	7,691	
1.805 01	0.064	1.73E 00	0.947	9.12E-01	1.66E 06	19.072	5. 78E- 01	8.419	
1.90E 01	0.122	1.485 00	0.896	8-25E-01	1,59E C6	16.179	6.71F-C1	9.057	
1 95E 01	0.144	1.4CE (0	0.880	7.94E-01	1.57E 06	15.485	7.085+01	9. 272	
2 0 35 31	0.153	1.375 00	0.862	7.69E-01	1.56E 06	15.026	7.45E-01	9.667	Toble D
2.055.01	0.150	1.26F CO	0.841	7.475-01	1.55E 06	14.771	7.855-01	9, 556	rabie 9, page i
2.105 01	C.137	1.17E CO	0.812	7.236-01	1.545 06	14.653	8. 40E-01	10.235	
2.2)E 01	0.162	9. 97F-01	0.765	6-51E=01	1-455 06	13, 533	9. 77E-01	10.746	
2.40F 01	0.269	7. 255-01	6.722	5.02E-01	1.225 06	10-245	1.215 00	274.11	
2. 605 01	0.405	5. 88E-01	0.748	2 026-01	1 045 06	6 797	1 155 00	12.324	
2.835 31	0.402	5.045-01	0.774	3.275-01	0 295 05	6 967	1 025 00	12.072	
3.00E 01	0.551	4,49E+01	0.794	2,825-01	8∎59€ 05	3.708	8.89F+01	13.583	
3.505 01	0 634	3 345-01	0 0 2 2	2 035-01	7 105 05	3 155	6 675-01	14 070	
A COE OT	0.407	2+2457 UL	0.070	2.035701	1+19E 00	2.100	0+475-01	14+7/4	
4 5 1 11	C 749	24 910701	0.070	1 115-01	0.000 US	1.009	3 336 01	17 310	
5 005 01	0 700	1. 905 701	V.872	1.110-01	2.00E 02	0.014	2. 205 DI	10 114	
5 60E 01	0.000	1.346401	J.872		9030E 07	0.000	2.595-01	10.110	
0+07E 1	0.819	1.206401	2.907	0.805-02	1.83E UD	C. 157	1.525-01	194 410	
5.COE 01	0.844	9.56E-72	0.920	5.415-02	3,298 05	^. 252	1.38E-01	19.621	
6.50E 11	0.863	3.17E-02	Ċ.933	4.38E-02	2.886 05	0.172	1.076-01	20.240	
7.005.01	C.89)	6, SCE-02	. 94 4	3.655-02	2.598 05	0.119	8.665-02	20. 798	
7.20E 01	0,898	6.47F=02	0.948	3.416-02	2.49E 05	0.101	7.985-02	21.000	
10 פינּיי	0.903	5.26E-02	0.951	3,295-02	2.43E 05	0+092	7. 64F-02	21.111	
7.43E 31	0.908	6.C4E-02	0.953	3.175-02	2.38F 05	0.083	7.305-02	21-211	
7.45F 01	0-911	5.955-02	0,955	3.115-02	2.35= 05	0.079	7.145-17	21, 261	
7.50E 11	0.014	5.865-02	0.057	3.045-02	2.325 05	0.074	6. GOF - 02	21.310	
7.55E 31	0.014	5.795- <i>0</i> 2	1.050 1.050	3_036_02	2.315 05	0.040	6.845-07	21.250	
7.60E 01	0.923	5.735-02	0.961	2.98E=02	2.30E 05	0.062	6.70E-02	21.407	
7 455 01	0.022					n 054	/ 3/6 00		
7 705 01	C. 432	5.50Em12	0.966	3.05E-02	2.372 05	0.054	6. 70H-02	21.450	
7 - 1 JL - 11	5.9.54 0.000	7 ZUE - 02		3.726=02	Z.916 05	0.063	H. 20 - 02	21.613	
7 8 7 75 G1	C.925	7. 55t=7Z	• 96 3	3 9ZE=0Z	3.08E 05	0.075	9.74F=C2	21.579	
7.875 91	0.925	6.58E-02	6.963	3.635-02	2.97E 05	0.070	8,115-32	21.641	
7+855-01	0.930	7+175+02	0.965	3.725-02	2.965 05	0.067	B 24E-02	21.703	

OPTICAL CONSTANTS OF AL2C3

EN ER GY	EPSILON1	EPSILON2	N	к	ABSCOSEF	REFLECITS	ENERGYLOSS	V-EEE	
7.90E 01	0.932	7.69E-02	0.966	3.985-02	3,198 05	0 071	0 005 00		
7.95E 01	0.930	8 29E - 02	0.965	4-30E-02	3 445 05	0.070	······································	1 • 77r	
A.COE 01	0.922	8.555-02	0.061	4 655-03	20402 00	9.079	9.515-02	21,442	
8,05E 01	0.916	2 245-02	0.701	+++2t=02	3.010 35	0.040	4.57F-02	21.919	
	3 01 3	9.200TUZ	0.958	9+3IE=02	3.525 05	0.094	9.776-02	21,903	
8*105 OT	0.913	7.725-02	C ,95 6	4.048-02	3.31E 05	J* JA2	9 .1 95-05	22,064	
3+20E 01	0.915	7,00E-02	0.957	3.65E-02	3.046.05	0 092	8 305 63		
8.30F 01	C.919	6.725-02	0.959	3.505-02	2 055 05	0.036	8. 3198 - 5.3	22.134	
8.40E 01	0.921	6. 55E-02	0.960	3 435-02	20720 02	11 + 12 7 P	7.925-02	22,319	
8.50E 01	9.923	6. 4PE= 02	0 941	3 375 63	2.92 <u>2</u> 00	2.2.1	7.736-02	22,442	
8.60E 01	n. 024	6 345-03	0.701	3.315-02	2.90E 75	0•023	7.585-07	72,565	
0.010 01	00 724	0.042-02	Je 902	3.366-12	2.878 05	0.165	7.405-02	22.697	
8.70E 01	0.925	6.1 CE - 02	0.962	3.20 5-0 2	2.82E 05	0.064	7-175-02	22 967	
8.80E 01	0.925	5,915-02	2.963	3.07E-02	2.745 05	1,060	6 040-07		
8.90E 01	0.929	5.69E-02	0.964	2,955=12	2.665 05	3 654		12.974	
9.00F 01	0.932	5.53E-02	0-966	2.845-02	2 410 00		C	23.024	
9.10E 01	0.936	5.495-02	0 04 0	2 8/5 02	2.010 0.3	1 • 2 • 1	6. 44 - 92	21,140	
		20 4 M. 02	¢∎900	2:042702	2.625 05	ذ+ن∙ت	6.255-02	23, 261	
3.20E 31	C. 940	5.646-02	C.970	2.915-02	2.715 05	0.045	6 • 355 - 92	27. 275	
4 40E UL	0.943	6.1CE-02	0+972	3.145-02	2,995,05	1.045	6.84F-02	73. 676	
9 . 605 01	0.942	6. £2E-02	0.971	3.41E-02	3.325 05	0.052	7.435-02	13 002	
9.80E 01	0.938	6.7CE-02	0.989	3,465-02	3-435 05	0.056	7 505 03	24 7 1	
1.COE 02	0.933	6. 42E-02	0.966	3-325-02	3 375 06	5.050		24 193	
				JU JE C-C E	20275 00	• 195	7.346-02	24 494	
1,05E C2	0,932	5.3CE-02	0.956	2.756-02	2.92E 05	2.049	6. F3E-02	75 114	
1.10E 02	0.936	4+515-02	C, 968	2.335-02	2.60E 05	0.04t	5 146-07	05 710	Table 9 name
1.15E 02	0.941	3.56E-02	0.970	2-04E=02	2.385 05	0.074	0.140-02 ((30 AB	2 3 • 71 ¹⁰	Table 2. pop
1.20E 02	0.946	3.59E - 02	0.973	1.85E-02	2,000 75	0.000	4+4rc=02	254232	
1.22E 02	0.947	3.55F-02	0.973	1 925-02	2.00 05	N • 02 5	4 JF - 7	75.732	
				10002-12	20205 00	0.027	3 . 965 - 02	26. at 5	
1.24E 02	0.947	3 • 52E - 02	C.974	1,815-02	2.27E 05	0.026	3 015-02	27.110	
1.26E C2	0.948	3.34E-02	0.974	1.715-02	2.195.05	A A 25	3 310 02	07.000	
1.30E 02	0.950	3. C4F-02	0.975	1.565-02	2 040 06	0.020	1.715+72	5.4 5.86	
1.34E 02	0.953	2.795-02	0.976	1.435-02	2000 00	V + V 2 3	3.375-02	27,563	
1.36E 02	0.954	2.71E=02	0.977	1 305-02	1.946 05	0.020	3.075-02	5 4° 0 0 3	
	0.,,,,,	LUTIC VL	0.0711	1.395-02	1.915 05	6•010	2.975-02	28 . 148	
1.38E 02	0.955	2.65E-02	0.978	1.35E-02	1.898 05	0.018	2.90E-02	29.331	
1.40E 02	0.956	2.616-02	0.978	1.335-02	1.89E 05	0.017	2.855-02	28 404	
1.50E C2	C.960	2 a 22E - 02	0.980	1.13E-02	1.776.05	0.014	2 615 02	20 231	
1.60E 02	0.963	1.926-02	0.982	9.775-03	1.57E 05	0.011	1 076 01	29.205	
1.80£ C2	0.970	1.40E-02	0.985	7 COF-03	1 205 45	0.007	2+176=12	24.845	
					10295 /J	1. O. F	1.495-02	41 . 003	
2.00E 0Z	0.974	I. C 5E-02	0.987	5.335-03	1.06E 05	0.005	1.115-02	31. 797	
2. 50E 0Z	0•98Z	6.45E-03	0.991	3.265-03	7.555 04	0.013	6 73E 03	22 041	
3.00E 02	0.987	3.605-03	0.994	1.816-03	5.29E 04	0.001	3 705-03	10.01	
3.50E 02	0.990	2.46E-03	0.995	1.245-03	4.05E 04	0 0.01	3 535 63	14.1111	
4.00E 02	0.993	1.45E-C3	C.997	7.295-04	2 036 04	0.000	2.028-03	34. 735	
				1 4 2 <i>1</i> 2 - 0 4	(•97 <u>5</u> -94	0.005	1.476-03	35.351	
5.00E 02	0.996	9.C3E-04	0.998	4.028-04	1.95E 04	0.000	8.10E-04	36. 000	
5.50E 02	0.998	1.62E-03	0.999	8.095-04	4.51E 04	0.000	1.675-03	34 700	
6.COE 02	0.997	1.556-03	0.999	9.77E-04	5,935,04	0.000	1.946-03	204/09	
8.00E 02	0.098	6.97E-04	0.999	3.49=-04	2 874 04	0.000	7 000 01	5 5 6 17 5 4	
1.COE 03	0.999	3.216-04	0.999	1.61F-04	1.616 04	0.000	1 005-04	41.225	
					14072 04	H = 1 3.2	2+225-04	42.926	
1.20E 03	0,999	1.62E-04	1.000	8.10E-05	9.81E 03	0.0	1.625-04	43.881	
1.40E 03	0.999	9. OCE- 05	1.000	4.505-05	6.38E 03	0.0	9.016-05	44 600	
1.50E 03	1.000	6.798-05	1.000	3.40E-05	5.15E 03	0-0			
1.55E 03	1.000	5. \$3E+05	1.000	2.975-05	4.65E 03	0.0		44.741	
1.60E 03	1.000	1.035-04	1.000	9.145-05	1.495 04	••	2 945 03	44.931	
					19402 04	**• U	1.83F=04	45,000	

• •



ŧ

đ









1

.

ī,



Fig. 3



Fig. 4



Fig. 5





.



Fig. 8



Fig. 9



Fig. 10


Fig. 11

.



.

Fig. 12



Fig. 13



đ

Fig. 14









Fig. 17







Fig. 19

.

é



Fig. 20



Fig. 21









Fig. 24

•

ŧ



2

. .



Fig. 26

Fig. 27



1. ie.

.



ę

ð i

2

Fig. 28



Fig. 29

ħ



÷

ŧ

ŧ٩

\$







Fig. 32



Fig. 33



Fig. 34

ć



Fig. 35





гi,

ţ









! }

•





۰,

~ . •••



e 🗸 🐖 🦻



Fig. 43

ŧ

 $\frac{1}{2}$

Ņ

у р 1

đ

1 1 \$

* įì

×,

*

\$

d.

5;