

# Dominant factors for the pinning enhancement by large artificial partial and complete antidots in superconducting films

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## Abstract

Partially (blind) or fully perforated antidots (BADs or ADs, respectively) fabricated by laser lithography and ion beam etching in superconducting  $\text{YBa}_2\text{Cu}_3\text{O}_7$  (YBCO) films possess a cumulative circumference wall surface, which is found to be responsible for pinning vortices and/or magnetic flux, whereby increasing the critical current density ( $J_c$ ) relative to corresponding plain (unpatterned) films. Using a variety of contrastingly shaped, relatively large 2–5  $\mu\text{m}$  BADs and ADs, the  $J_c$  of YBCO thin films has been effectively increased within the relatively narrow band of wall surfaces of antidots, independent whether patterns are AD or BAD type. Independence of antidot types indicates that enhancement is insensitive whether magnetic flux is inside the ADs, or vortices are inside the BADs. Within this AD wall surface band region a clear shape dependence also emerges. This finding may also provide a guide for superconducting devices requiring maximal  $J_c$  and reduced associated vortex movement noise.

Keywords: antidot, critical current density, flux pinning, defect wall, YBCO thin films

(Some figures may appear in colour only in the online journal)

## 1. Introduction

Improving, modifying and controlling the critical current density ( $J_c$ ) of superconductors is necessary for existing and potential devices. Tailored flux pinning in  $\text{YBa}_2\text{Cu}_3\text{O}_7$  (YBCO) using artificial and natural defects can provide the necessary  $J_c$  enhancements. Major studies in film microstructure alterations such as multilayering [1, 2], addition of secondary phase nanocomposites [3–6], nanorods [7–9] or ion irradiation [10–12] have proved successful.

Lithographic nanofabrication techniques by the complete or partial removal of the superconductor provide vortex and/or flux trapping in small and controlled locations [13–22], which allows more regulated and, possibly, complementary vortex manipulation and guidance. The so-named antidots (ADs) provide areas of reduced, or zero, superconducting potential and may be specifically designed to match vortex

lattices, further increasing the energy required to move the vortices. Due to the flux pinning capabilities of the ADs, generally their use has been in both reduction of vortex movement and its associated noise [23–25] and enhancement of  $J_c$  [15, 18].

Progress with this type of defect has been limited by the size of the AD, which has generally been around tens to hundreds of nanometers with one reason being that ADs could accommodate only one or a few vortices. This limits  $J_c$  and vortex control to only tiny applied magnetic field ( $B_a$ ) range, mainly around the so-called single vortex pinning regime. Another problem lies with the difficulty of producing AD on such a scale, in both time and expenditure, in particularly on an industrial scale [26]. One obvious way to fix this would be to increase the size of the AD. In doing so optical laser lithography (with  $\mu\text{m}$  resolution) can be used rather than electron beam lithography (with nm resolution). However, the

most important aspect of this size increase is to ensure the  $J_c$  is reliably and controllably increased. Defects this large have been shown to increase the  $J_c$  of YBCO thin films. This includes both modifying the location of the ADs to a graded or non-uniform landscape [15] and by reducing the size of the hole to  $2\ \mu\text{m}$  to around the resolution limit of laser lithography [18]. Another application of micron sized holes is the ability to create a ratchet effect [19, 27].

In this work, micron-sized defects much larger than the magnetic field penetration depth ( $\lambda$ ) provide the pinning landscape such that the  $J_c$  enhancement can be investigated, so that some generalization of such behavior can be drawn. We have found that partially (or blind BADs) or fully perforated antidots (ADs) fabricated by laser lithography and ion etching in YBCO films produce a consistent  $J_c$  enhancement if the circumference wall of antidots has the rather narrow optimal surface area, which is independent of shape and type of antidots.

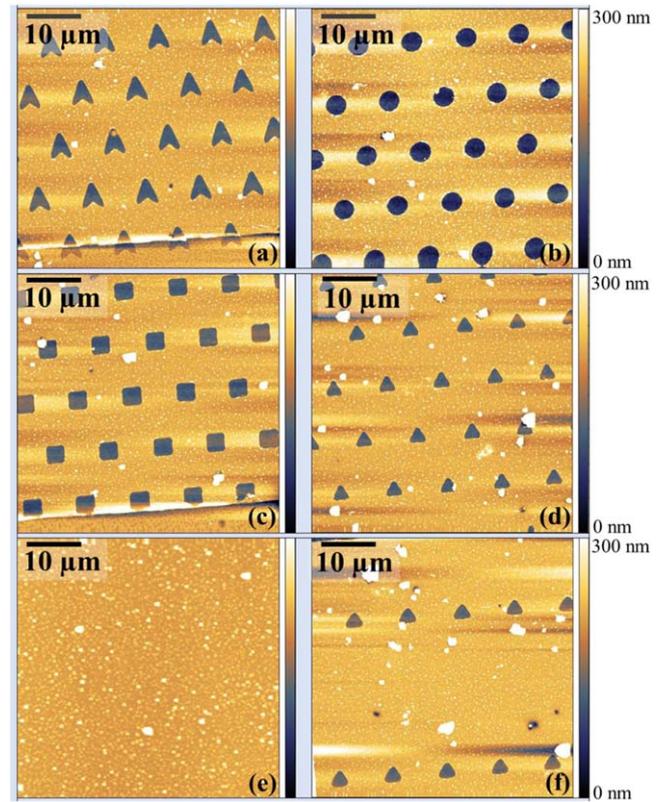
## 2. Experimental details

YBCO thin films of  $\sim 250\ \text{nm}$  thickness have been grown on  $5 \times 5\ \text{mm}^2$  LaAlO<sub>3</sub> (LAO) substrates by our well-established PLD process, which is described elsewhere [1, 28, 29]. Their critical temperature and critical current density are typically  $T_c = (91.5 \pm 0.5)\ \text{K}$  and  $J_c \simeq 3.5 \times 10^{10}\ \text{Am}^{-2}$  at 77 K, respectively showing consistent high quality.

Laser lithography (Heidelberg Instruments  $\mu\text{PG 101}$ ) and ion beam etching (IBE) were used to define the bridges and patterns [30, 29]. The two families of samples used were created with artificial defects being etched entirely through the YBCO (fully perforated ADs) and etched partially through the YBCO (blind hole ADs denoted as BADs). The shapes and sizes of the artificial defects were the same for both families with the all blind patterns used are shown in figure 1. Note the typical rounded edges for samples BB, SB, TB and T2B are due to the limited resolution of the laser lithography used.

The sizes of the respective defects are defined by the height of the  $5\ \mu\text{m}$  boomerangs denoted as B (figure 1(a)); by the diameter of the  $2\text{--}3\ \mu\text{m}$  circles denoted as C (figure 1(b)), and by the long edge of the pattern for  $2\text{--}3\ \mu\text{m}$  squares (S) and triangles (T and T2) shown in figures 1(c)–(f), respectively. The nomenclature of the blind hole patterns was defined by an additional B, e.g. circles would be CB. If size is not specified it represents the  $3\ \mu\text{m}$  patterns, as these made up the majority of artificial defects investigated. In all bridge samples, a control unetched plain (P) region was also present (figure 1(e)).

Standard equilateral triangle, circle and square shapes were used. For the boomerang shapes, an equilateral triangle is initially defined, with the base removed in a triangle shape as well. The apex of the inside elbow is 40% of the maximum height to give a typical boomerang look. The boomerang shape has been tested with a view to achieve ratcheting effects in the future, and to maximize the circumference of the shape to volume removed. The lattice period was  $10\ \mu\text{m}$  in a



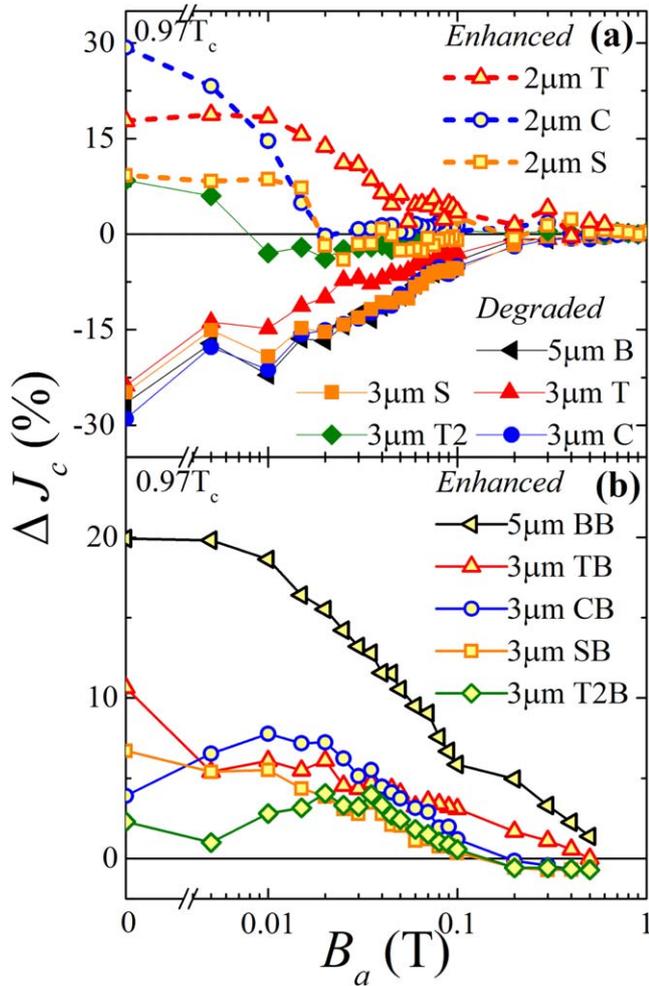
**Figure 1.** AFM images for blind (a) boomerangs (BB), (b) circles (CB), (c) squares (SB), (d) triangles (TB), (e) plain (P) and (f) triangles 2 (T2B).

triangular array for all patterns, except T2 which had a  $10\ \mu\text{m}$  horizontal period and a  $30\ \mu\text{m}$  vertical spacing in a triangular array.

The fully perforated AD patterns were etched at the same time as bridge definition to ensure complete removal of YBCO. For the BAD patterns, the bridges were defined first by lithography and IBE, and then the patterns applied on top of the bridge to be etched again. Cross sectional examination of BAD in figure 1 reveals an etch depth of  $100\ \text{nm}$  for all blind holes, meaning  $150\ \text{nm}$  of YBCO left within the defect. Patterning of bridges with either blind or fully perforated holes did not change the  $T_c$  characteristics. Both sample types were very similar, starting the superconducting transition at  $(91.5 \pm 0.5)\ \text{K}$  and reaching zero resistance at  $(88.5 \pm 0.5)\ \text{K}$ .

Resistance measurements were performed in a Quantum Design Magnetic Properties Measurement System. For  $T_c$  measurements a current of  $10\ \mu\text{A}$  was applied and temperature sweep rate of  $2\ \text{K min}^{-1}$ . A critical voltage of  $10\ \mu\text{V cm}^{-1}$  between contacts was used to determine  $I_c$ .

The  $J_c$  of each bridge was taken as  $I_c/(w_p \times d_p)$ , where  $w_p$  is the bridge width and  $d_p$  the bridge thickness, with the volume removed by the etched defects taken into account. The difference in  $J_c$  is given by  $\Delta J_c = (J_c^{\text{pattern}} - J_c^{\text{plain}})/J_c^{\text{plain}} \times 100(\%)$ .



**Figure 2.**  $J_c$  difference calculated by magnetisation measurements at 86 K ( $0.97 T_c$ ) for (a) fully perforated ADs and (b) blind holes.

### 3. Results and discussion

#### 3.1. Comparison of fully perforated AD and BAD patterns

A clear  $\Delta J_c$  dependence on defect type and shape is observed across all  $B_a$  up to 1 T (figure 2). The degradation of  $J_c$  caused by the larger (3–5  $\mu\text{m}$ ) patterns in figure 2(a) appears to somewhat uniformly follow the amount of volume removed. The highest etched volume for boomerang shaped ADs has caused the most  $J_c$  degradation, and T2 the least. Table 1 shows the volume per hole removed for each shape of AD, as well as the total removed volume compared to the volume of the entire film. On the other hand, reducing the volume of the ADs to that of the 2  $\mu\text{m}$  shapes leads to an increased  $J_c$  relative to the plain film. This is consistent with the results found in [18], as well as converging to the apparent optimal AD size  $\sim \lambda$  [13, 31].

The 2  $\mu\text{m}$  patterns also provide evidence for a pinning potential shape dependence. The 2  $\mu\text{m}$  T sample has less enhancement at lower fields compared to 2  $\mu\text{m}$  C, but the enhancement extends over a much broader  $B_a$ , even though the volume removed is much lower for 2  $\mu\text{m}$  T (table 1). The 2  $\mu\text{m}$  S, with the largest volume removed, shows the least  $J_c$

**Table 1.** Volume statistics for all samples measured. Where  $V_{total}$  is the total volume removed from etching,  $V_{film} = 3750 \mu\text{m}^3$  and  $D_w$  is the area of the pinning wall.

Sample	Shape	$V_{hole}$ ( $\mu\text{m}^3$ )	$V_{total}/V_{film}$ (%)	$D_w$ ( $\mu\text{m}^2$ )
T2B	Triangle	0.46	0.61	0.90
T2	Triangle	1.14	1.52	2.25
TB	Triangle	0.46	1.84	2.90
CB	Circle	0.94	3.76	3.26
SB	Square	0.96	3.84	3.72
2 $\mu\text{m}$ T	Triangle	0.42	1.68	4.50
BB	Boomerang	1.00	4.00	4.93
2 $\mu\text{m}$ C	Circle	1.01	4.05	5.34
2 $\mu\text{m}$ S	Square	1.10	4.40	6.30
T	Triangle	1.14	4.56	7.25
C	Circle	2.35	9.40	8.17
S	Square	2.40	9.60	9.30
B	Boomerang	2.50	10.00	12.30

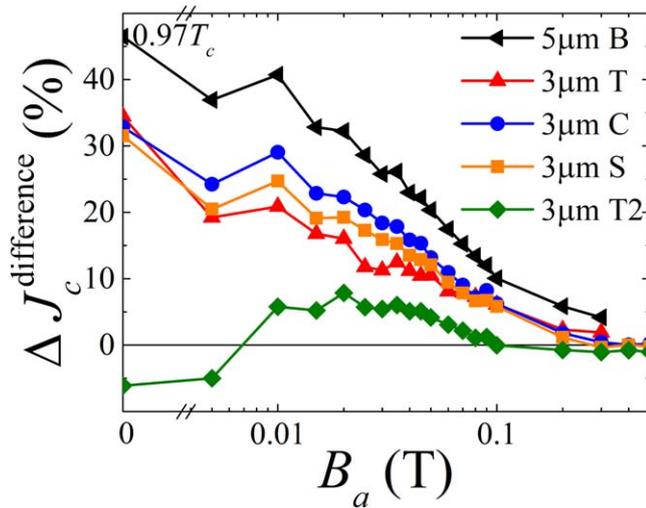
increase. Shape/volume dependence is discussed further in the ‘Pinning model’ section.

The  $J_c$  enhancement over a broader range of  $B_a$  for all the shapes of BADs in figure 2(b) is in direct contrast to that of ADs in figure 2(a). It is also contrary to the behavior of much smaller holes being only a few coherence length ( $\xi$ ) large [32], for which fully perforated holes were found to be more effective. Surprisingly, the 5  $\mu\text{m}$  BB sample displays the highest magnitude and broadest  $\Delta J_c$  enhancement even though the largest volume was removed within the blind sample family. No current rectification was observed in the asymmetrical samples, likely due to the low density of BADs or ADs, the large size of the defects relative to the size of a vortex and the rounded edges in figures 1(a), (d), (f). Similar measurements were also taken at  $T = 84 \text{ K}$  ( $\approx 0.95 T_c$ ) for nearly identical results.

#### 3.2. Comparison between shapes of ADs

The difference is taken between  $\Delta J_c$  values of the respective BAD and AD shapes, that is,  $\Delta J_c^{\text{BAD}}(\%) - \Delta J_c^{\text{AD}}(\%) = \Delta J_c^{\text{difference}}(\%)$ , and plotted in figure 3. The difference shows how much more effective the respective blind patterns are compared to the AD. The BAD patterns are obviously more effective at increases  $J_c$  over the entire field range, with some relatively minor exceptions for T2 type samples, which have had the smallest number of artificial defects introduced and resulted in the smallest  $\Delta J_c$ . The higher degree of effectiveness for blind holes is in contrary to the effectiveness of small blind holes (of the order of a few  $\xi$ ) found in [32].

Figure 3 generally shows three distinct areas of difference, again based on the amount of volume removed. As expected the largest difference in effectiveness is displayed by the B patterns. This is due to fact that it is the most effective blind pattern, and most degraded AD pattern. The likely cause of this is that the largest volume etched from its AD causes the highest level of degradation. On the other hand, the BB provides an effective patterns with the longest additional



**Figure 3.** Comparison of  $J_c$  differences calculated by magnetisation measurements for  $3 \mu\text{m}$  patterns between fully perforated AD patterns and BAD patterns.

pinning at the walls on the edges of the etched BAD regions [28, 30, 33], while maintaining [34] the inherent vortex pinning natural to PLD YBCO thin films [1, 29, 35] within the BAD regions that are intact and still about  $\sim 150$  nm thick for all the BAD patterns.

While it would be straightforward to conclude that the  $J_c$  enhancement directly depends on the volume of removed superconductor, this is clearly not the case. The C pattern have the second highest  $\Delta J_c$  difference, while the third largest volume removed (table 1).

In addition, it appears that the larger the degradation is for AD patterns in figure 2(a), the larger the enhancement is observed for BAD patterns in figure 2(b), which leads to the largest  $\Delta J_c$  difference in figure 3. One exception to this dependence appears to be for  $3 \mu\text{m}$  T2, where the AD case is more effective for  $B_a < 0.01$  T and  $B_a > 0.1$  T, showing that ADs can be better pinning centers than BADs in some cases. This is likely due to the reduced AD density in the T2 case.

General shape of the curve was again similar to that at  $0.95 T_c$ , hence not shown. However, this effectiveness reversal between the defect types occurred at a higher field (possibly due to lower  $T$  of these measurements).

### 3.3. Comparison between magnetic and transport measurements

For a better understanding of the effect large ADs incur onto a YBCO thin film, magnetic (*mag*) and transport (*trans*) have been performed. Indeed, samples with fully perforated AD patterns can be expected to respond differently to magnetic measurements [36], which may produce meaningful signals even for granular samples, and to transport measurements, which favor structurally continuous samples with continuous current paths. In addition, while either method may give an accurate value for  $J_c$ , certain considerations of electric field criteria used for different types of measurements may be required [37]. Obviously, different electric field criteria used

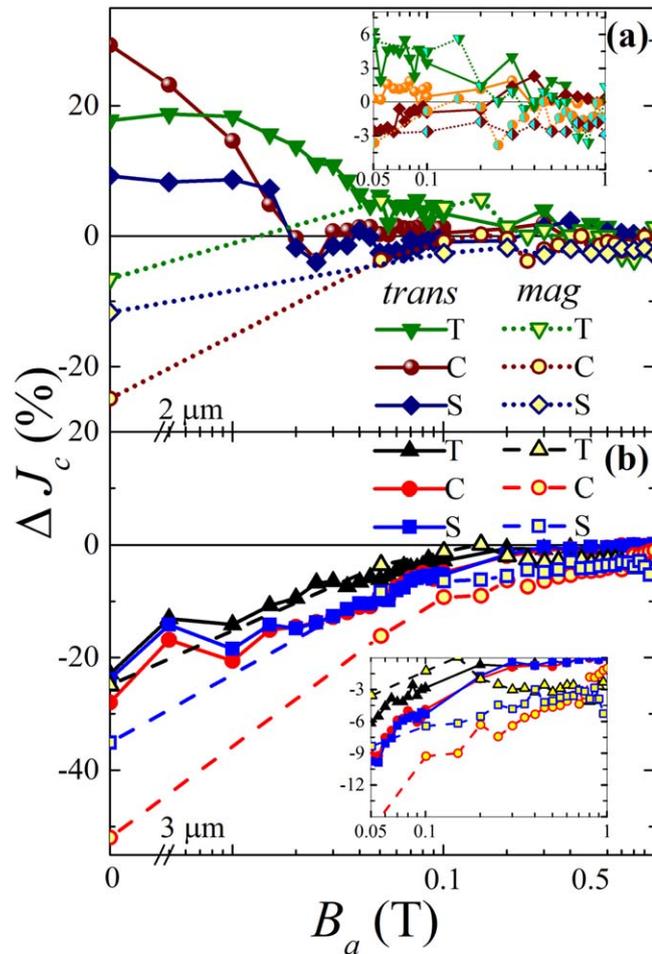
in magnetic and transport measurements assume different degrees of vortex motion involved, generating energy losses [37, 38]. Different vortex motions can be exacerbated by vortex creep and thermally activated flux flow [39–42]. Dynamics of vortices interacting with ADs and BADs is also expected to be quite different, hence dissipation involved, corresponding electric field criteria, and respective measurement type can respond differently to samples having ADs and BADs. Finally, slightly differing directions of the Lorentz forces with respect to some AD shapes may be considered. *Trans* measurements induce a Lorentz force perpendicular to either the top or bottom of each shape. On the other hand, the circulating current around the entire square film during *mag* measurements directs the vortices toward the center. In a regular triangular array like that seen in figure 1, vortices would experience a Lorentz force orientated at every point around the shape. All these effects together potentially can cause a notable difference between the two measurement types.

Both measurements types are restricted in the temperature range that they can measure (*mag* measurements need a high signal, therefore lower temperature, the *trans* experimental set-up is limited to  $\sim 100$  mA to avoid excessive heating, thus require to be close to  $T_c$ ). Due to this, the comparison temperatures are  $0.87 T_c$  (77 K) for magnetic and  $0.97 T_c$  for transport. Further differences are expected between these temperature ranges, however, a qualitative comparison may prove being useful. *Mag* samples were prepared on  $5 \times 5$  mm<sup>2</sup> substrates. This was reduced to  $3 \times 3$  mm<sup>2</sup> in the center to remove any edge effects, with the patterns in regular triangle arrays like that shown in figure 1 throughout the entire film. The width of the magnetization loops is determined by  $\Delta M(B_a, T) = |M^+| + |M^-|$ , and using the critical state model  $J_c(B_a, T) = 3\Delta M/w$ , where  $w_p$  is the length of one side of the square sample [37].

The  $\Delta J_c$  between the respective measurement types correlate very strongly in both magnitude and shape for  $3 \mu\text{m}$  patterns (figure 4(b)), but not for the  $2 \mu\text{m}$  patterns (figure 4(a)) with the  $\Delta J_c$  being approximately the same between *trans* and *mag* measurements only above  $\sim 0.05$  T. Aside from a slight change in magnitude in figure 4(b), the only apparent difference is the large separation in  $\Delta J_c$  between the patterns for the *mag* measurements. The *trans* measurements on the other hand show a fairly close grouping in  $\Delta J_c$  across all  $B_a$ .

The circular hole  $3 \mu\text{m}$  sample in figure 4(b) degrades the most upon magnetic measurements even though they do not have the largest volume removed ( $2.35 \mu\text{m}^3$  compared to  $2.40 \mu\text{m}^3$  of a square). This suggests that there is a AD shape dependence, more than just due to AD volume removed.

One shape dependence explanation may be due to triangle and square ADs both having straight edges, which might present more of a pinning barrier for the vortex to overcome compared to circular ADs. Circle hole circumferences would always allow a tangential component of the Lorentz force to exist allowing vortices to slip around easier regardless of the current path upon magnetic or transport measurements. This would mean the circles would be



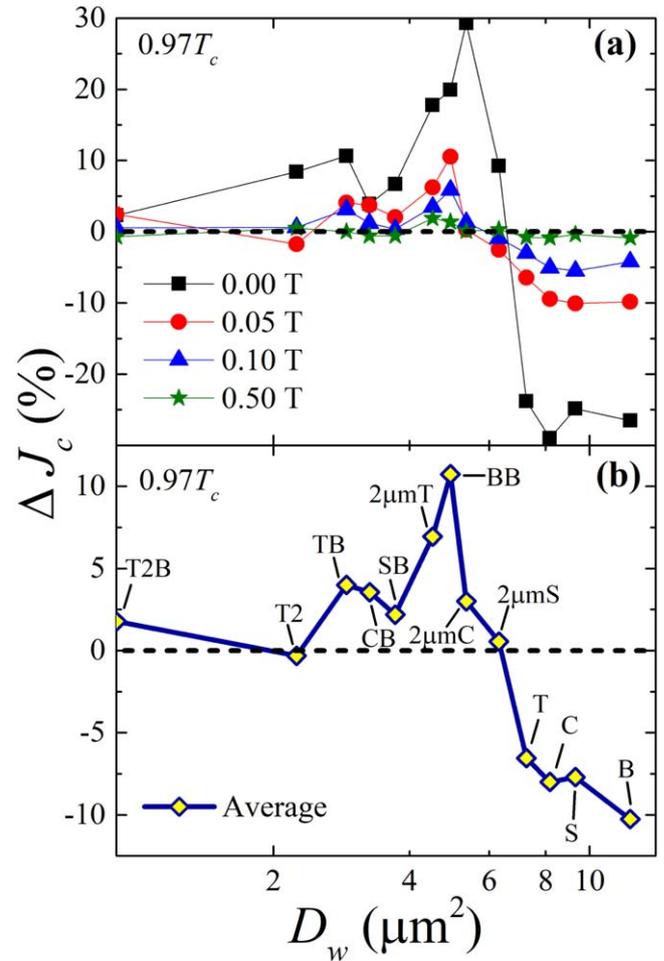
**Figure 4.** Comparison of  $\Delta J_c$  for (a)  $2 \mu\text{m}$  and (b)  $3 \mu\text{m}$  patterns between transport (*trans*) and magnetic (*mag*) measurements. Transport measurements taken at 86 K ( $0.97 T_c$ ) and magnetic measurements at 77 K ( $0.87 T_c$ ). Inset shows the corresponding high field ( $>0.05$  T) data.

consistently worse pinning sites for all sizes. One apparent exception for  $2 \mu\text{m}$  C measured by transport occurs at low field range ( $<0.02$  T) where pinning plays less important role than current flow transparency [43, 44].

Slight discrepancies between measurement types, especially in low fields, are likely the result of these different measurement modalities discussed above in these fully perforated samples. Overall, *mag* measurements show consistently lower  $\Delta J_c$  than the *trans* measurements. This is likely due to both difference in the respective electric field criteria [37] and different measurement temperatures. However, it is currently impossible to completely disentangle these influences.

### 3.4. Consideration of vortex pinning by ADs and BADs

To explain the different pinning effectiveness between the different types and shapes of AD defects,  $\Delta J_c$  was plotted as a function of the etched defect wall area ( $D_w$ ) calculated for each AD defect (table 1) in figure 5. The  $D_w$  value is given by a corresponding circumference multiplied by the depth of the AD or BAD defect. For instance the  $D_w$  of sample S would be



**Figure 5.** (a) The  $J_c$  difference as a function of the AD etched wall area for several applied magnetic fields. (b) The  $\Delta J_c(D_w)$  dependence averaged over all the applied field values displayed in (a). The AD pattern types marked in (b) for each symbol correspond to those plotted in (a).

$3.1 \mu\text{m}$  (optically measured length of one side)  $\times$  4 (sides)  $\times$  250 nm (etched depth)  $\times$  3 (ADs) =  $9.30 \mu\text{m}^2$ , whereas the  $D_w$  of sample SB would be  $3.1 \mu\text{m} \times 4 \times 100 \text{ nm} \times 3 = 3.72 \mu\text{m}^2$ . The junction between the etched and non-etched regions being the area of additional nano-wall pinning [34]. The obtained values for  $D_w$  are given in table 1 in order of increasing  $D_w$ . In figure 5(a), the  $\Delta J_c(D_w)$  is shown at different  $B_a$  values, which displays a similar trend at all the field values with the magnitude of the  $\Delta J_c$  suppressed towards 0% at higher fields.

As expected, removing a very small volume of the superconductor (T2B) has least enhancing effect on the  $J_c$  in the superconductor compared to the corresponding plain film. On the contrary, removing relatively large volumes (all fully perforated  $3 \mu\text{m}$  patterns and  $5 \mu\text{m}$  B) causes a large  $J_c$  degradation relative to a plain film rather than enhancement. T2 has fully perforated AD pattern, however the full perforation is counterbalanced by a relatively small number of ADs in this pattern, so that its  $\Delta J_c \approx 0\%$ .

Between T2 and  $2 \mu\text{m}$  S, there appears to be the optimal region of the AD wall area with  $D_w$  being between  $\sim 2 \mu\text{m}^2$

and  $\sim 6 \mu\text{m}^2$ . This optimal AD defect wall area region appears for defects that have much greater size than the ‘optimal’ ( $\simeq \lambda$ , the magnetic field penetration depth) vortex (or/and flux) pinning [13, 31, 43, 44], which may generally complement the  $\xi$ -optimal vortex pinning.

Further emphasized in figure 5(b) are the two main factors of the defects dependence on  $\Delta J_c$ , being the pinning AD wall area, as well as, the geometrical shape of the AD defects. Within  $D_w$  of  $\sim 2 \mu\text{m}^2$  to  $\sim 6 \mu\text{m}^2$ , the shape of the defect becomes the dominant factor affecting  $\Delta J_c$ . In this region, samples TB, 2  $\mu\text{mT}$  and BB are more effective than CB, SB, 2  $\mu\text{mC}$  and 2  $\mu\text{mS}$ . This shows that  $J_c$  in the patterned samples is not entirely determined within  $D_w$ , perhaps also being dependent on the angle of this defect wall to Lorentz force direction. In general, triangles have the highest surface area to the volume ratio, meaning that samples T and B, for instance, have the most additional pinning regions compared to the volume which has been removed of the patterns measured. This implies that removing the least amount of YBCO with already huge number of intrinsic pinning defects [2, 35, 45, 46], while adding the additional pinning AD wall area, is the main guiding principle for choosing the shape, size and type of AD patterns.

The fact that an optimal region of  $D_w$  exists should not be underestimated. The entirely different pinning mechanisms between large blind holes [28, 30], where vortices exist within the hole, and large fully perforated ADs, where vortices cannot exist inside, should be appreciated. Furthermore, the size of the individual defect of T and T2 is the same, however, with the increased vertical period of T2 the value of  $D_w$  is reduced to below  $6 \mu\text{m}^2$  and enhancement to  $J_c$  [15, 47] can occur (figure 5(a)). This is opposed to T where  $J_c$  is consistently reduced (figures 5(a), (b)).

The fact that the BADs and the ADs show approximately the same  $\Delta J_c$  (on average) as long as they are within the optimal  $D_w$  region is extremely useful when designing further defect experiments and defect patterned devices. It appears that the individual defect (shape, size and type) is less important than their entire pattern, which renders a significantly simplified path of their manufacturing for the resolution dependent fabrication equipment.

#### 4. Conclusion

Partially and fully perforated antidots of different shapes and micron-large sizes fabricated by laser lithography and ion etching in YBCO films have been shown to significantly affect their  $J_c$ . The detrimental factor responsible for critical current enhancement of up to  $\sim 30\%$  in the patterned films compared to their as-grown counterparts is found to be the area of the circumference wall of the antidots etched. The enhancing AD wall area is found only within  $\sim 2 \mu\text{m}^2$  and  $\sim 6 \mu\text{m}^2$ , which can even effectively counteract the completely removed superconducting volume within ADs. However, one of the most effective  $J_c$  enhancing patterns investigated was blind boomerangs (BB). Overall, the optimal  $J_c$  enhancing surface wall area was found independent of

partial or full perforation. The enhancement effect on  $J_c$  appears less dependent on the individual hole shape, but rather on the overall pattern. However, within the optimal  $D_w$  some shape dependence occurs, indicating that the geometry of the AD circumferences effectively contribute to vortex pinning as well. Further optimization of the  $D_w$  factor incorporating shape dependence would give insights on optimal AD patterns for  $J_c$  enhancement. When designing superconducting devices it becomes clear that optimization of AD positions is important to consider depending on the modality used or device created (e.g. superconducting bridge or pick-up loops [48]).

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