

# *Ab initio* study of structural, electronic, thermo-elastic and optical properties of Pt<sub>3</sub>Zr intermetallic compound

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Structural, elastic, electronic and optical properties of the Pt<sub>3</sub>Zr intermetallic compound are investigated using first principles calculations based on the density functional theory (DFT) within the generalized gradient approximation (GGA) and the local density approximation (LDA). The Pt<sub>3</sub>Zr compound is predicted to be of cubic L1<sub>2</sub> and hexagonal D0<sub>24</sub> structures. The calculated equilibrium ground-state properties (lattice parameters  $a$  and  $c$ , bulk modulus  $B$  and its pressure derivative  $B'$ , formation enthalpy  $\Delta H$ ) of the Pt<sub>3</sub>Zr compound, for both cubic and hexagonal phases, show good agreement with the experimental results and other theoretical data. Elastic constants ( $C_{11}$ ,  $C_{12}$ ,  $C_{13}$ ,  $C_{33}$ ,  $C_{44}$ , and  $C_{55}$ ) are calculated. The predicted elastic properties such as Young's modulus  $E$  and shear modulus  $G_H$ , Poisson ratio  $\nu$ , anisotropic ratio  $A$ , Kleinman parameter  $\xi$ , Cauchy pressure ( $C_{12} - C_{44}$ ), ratios  $B/C_{44}$  and  $B/G$ , and Vickers hardness  $H_v$  indicate the stiffness, hardness and ductility of the compound. Thermal characteristic parameters such as Debye temperature  $\theta_D$  and melting temperature  $T_m$  are computed. Electronic properties such as density of states (DOS) and electronic specific heat  $\gamma$  are also reported. The calculated results reveal that the Fermi level is on the pseudogap for the D0<sub>24</sub> structure and on the antibonding side for the L1<sub>2</sub> structure. The optical property functions (real part  $\epsilon_1(\omega)$  and imaginary part  $\epsilon_2(\omega)$  of dielectric function), optical conductivity  $\sigma(\omega)$ , refraction index  $n(\omega)$ , reflectivity  $R(\omega)$ , absorption  $\alpha(\omega)$  and extinction coefficients  $k(\omega)$  and loss function  $L(\omega)$  are also investigated for the first time for Pt<sub>3</sub>Zr in a large range of energy from 0 to 70 eV.

**Keywords:** density functional theory, intermetallic, density of states, L1<sub>2</sub>, D0<sub>24</sub>, optical properties

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## 1. Introduction

Platinum group metals (PGMs) and platinum-based alloys, as high temperature structural materials, have attracted considerable attention in industrial applications<sup>[1–6]</sup> (automotive, aeronautic, aerospace, catalysis etc.). They exhibit exceptional physical, chemical and mechanical properties such as high melting point, high density, high strength, low reactivity and good oxidation and corrosion resistance.<sup>[5–16]</sup> Melting point of Pt is about 1760 °C, which is higher than that of pure nickel (1450 °C), and a young modulus is about 164 GPa.<sup>[17–20]</sup> Alloyed Pt (early transition metal) with an element from groups 4B and 5B such as Ti, V, Zr, Nb, Hf, and Ta (late transition metals) could form very stable alloys (Engel–Brewer alloys).<sup>[21,22]</sup> Pt–Zr alloys, especially Pt<sub>3</sub>Zr, show enhanced thermal and mechanical properties compared with Ni-based alloys. The Pt<sub>3</sub>Zr melting temperature in the L1<sub>2</sub> cubic structure is up to 2600 °C and the Young modulus is about 260 GPa, which are much higher than those of other Pt-based compounds.<sup>[23,24]</sup>

Many experimental and theoretical works have been effected to investigate basic properties of Pt<sub>3</sub>Zr in the L1<sub>2</sub> and D0<sub>24</sub> structures. Bai *et al.* have studied the structural properties, formation enthalpies, elastic constants and bulk modulus of Pt–Zr alloys in stable and hypothetical phases using the CASTEP code.<sup>[25]</sup> First principles calculations have been im-

plemented with the CASTEP code by Pan *et al.* to study a new structure and oxidation mechanism of the Pt<sub>3</sub>Zr compound.<sup>[26]</sup> Interfacial stability, electronic structure and bond characteristics of Pt<sub>3</sub>Zr (111)/Pt (111) interfaces have been investigated by Pan *et al.* using ab-initio calculations.<sup>[27]</sup> Using high resolution x-ray photoelectron spectroscopy, temperature programmed desorption, scanning tunneling microscopy and density functional theory, Li *et al.* studied growth of an ultrathin zirconia film on Pt<sub>3</sub>Zr.<sup>[28]</sup> Antlanger *et al.* investigated the surface of pure and oxidized Pt<sub>3</sub>Zr (0001) by scanning tunneling microscopy (STM).<sup>[29]</sup> However, there are insufficient experimental and computational data for realizing Pt<sub>3</sub>Zr electronic and elastic properties. Moreover, neither experimental nor theoretical results on their optical properties are available in the literature.

In this article, we investigate structural, elastic, thermal, electronic and optical properties of the Pt<sub>3</sub>Zr intermetallic compound in cubic and hexagonal structures. Our work is based on the first principles calculations considered as the most powerful method for research of materials properties.<sup>[30,31]</sup>

## 2. Computational details

In the present paper, computations of structural, elastic, electronic and optical properties of the Pt<sub>3</sub>Zr intermetallic

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compound were carried out using first principle calculations. All calculations are based on density functional theory (DFT) employing the full potential linearized augmented plane wave (FP-LAPW) method implemented in the WIEN2k code.<sup>[32,33]</sup> Exchange correlation functional was treated within the generalized gradient approximation (GGA) with the Perdew–Burke–Emzerhof (PBE) and the local density approximation (LDA).<sup>[34,35]</sup> The  $\text{Pt}_3\text{Zr}$  compound is found to be crystalline in the  $L1_2$  cubic structure (space group of  $Pm\bar{3}m$ ) with lattice parameter  $a = 4.051 \text{ \AA}$ <sup>[36]</sup> and in the  $\text{D0}_{24}$  hexagonal structure (space group of  $P6_3/mmc$ ) with lattice parameters  $a = 5.653 \text{ \AA}$  and  $b = 9.347 \text{ \AA}$ .<sup>[5]</sup> Muffin–Tin (MT) spheres radii  $R_{\text{MT}}$  were taken as 2.5 a.u. for Pt and Zr atoms. Total energies are converged at  $10^{-4}$  Ry. Integrations in the Brillouin zone were performed using special  $k$ -point generated with  $12 \times 12 \times 12$  and  $10 \times 10 \times 5$  mesh grids for cubic and hexagonal structures, respectively. The plane wave expansion parameter  $R_{\text{MT}} \times K_{\text{max}}$ , which controls the size of the basis sets in our calculations, was taken to be 7. The wave function inside the MT spheres was chosen up to  $l_{\text{max}} = 10$ . The charge density was expanded up to  $G_{\text{max}} = 12$ . The valence electron configurations were  $[\text{Zr}] = 4d^2 5s^2$  and  $[\text{Pt}] = 5d^9 6s^1$ .

### 3. Results and discussion

#### 3.1. Structural properties

Crystal structures of  $\text{Pt}_3\text{Zr}$  in Cubic and hexagonal phases are shown in Fig. 1. For the  $L1_2$  structure, Pt and Zr occupying the Wyckoff site of  $3c$  ( $0, 1/2, 1/2$ ) and  $1a$  ( $0, 0, 0$ ), respectively. For the  $\text{D0}_{24}$  structure, the atomic positions are  $6g$  ( $1/2, 0, 0$ ),  $6h$  ( $0.83, 2/3, 1/4$ ) and  $2a$  ( $0, 0, 0$ ),  $2c$  ( $1/3, 2/3, 1/4$ ) for Pt and Zr, respectively. The equilibrium lattice constants of the  $\text{Pt}_3\text{Zr}$  compound have been computed by optimizing volume through Murnaghan’s equation of state. The calculated total energies versus volume for cubic and hexagonal  $\text{Pt}_3\text{Zr}$  using (a) PBE-GGA and (b) LDA approximations are plotted in Fig. 2. We show that the  $\text{D0}_{24}$  phase of the  $\text{Pt}_3\text{Zr}$  compound is slightly lower in energy than the  $L1_2$  phase. The optimized ground state properties such as lattice parameters  $a$  and  $c$ , bulk modulus  $B$  and its pressure derivative  $B'$ , formation enthalpy  $\Delta H_f$  compared with the experimental and theoretical data are listed in Table 1. We find that there is an excellent agreement between our results and the available data. It can be seen that the calculated equilibrium lattice parameter  $a$  of the  $\text{Pt}_3\text{Zr}$   $L1_2$  structure using GGA (LDA) deviates from the experimental value by  $+0.12\%$  ( $-2.02\%$ ). However, the calculated equilibrium lattice parameters  $a$  and  $c$  of  $\text{D0}_{24}$ - $\text{Pt}_3\text{Zr}$  deviate from the experimental value by  $+1.23\%$  ( $-0.61\%$ ) and  $-0.18\%$  ( $-1.57\%$ ), respectively, using the GGA (LDA) method. We have not found experimental values of  $B'$  to confirm our results.

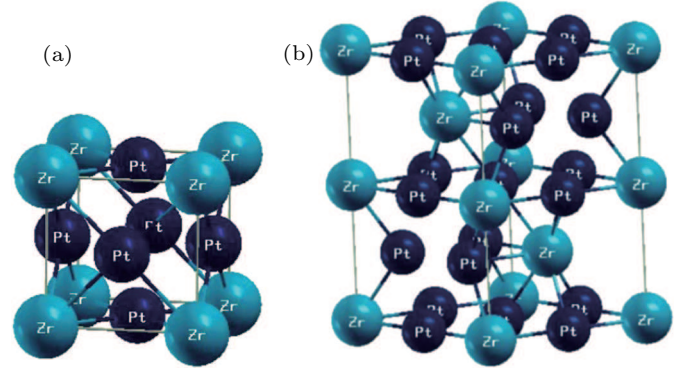


Fig. 1. Crystal structures of  $\text{Pt}_3\text{Zr}$ : (a) cubic  $L1_2$  and (b) hexagonal  $\text{D0}_{24}$ .

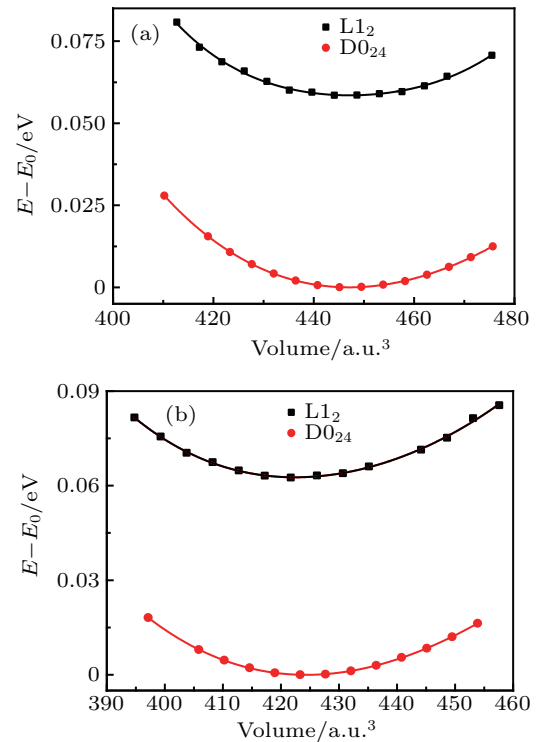


Fig. 2. Total energy versus volume per unit cell of  $L1_2$ - $\text{Pt}_3\text{Zr}$  and  $\text{D0}_{24}$ - $\text{Pt}_3\text{Zr}$  using (a) PBE-GGA and (b) LDA.

From the ground-state total energy, the formation enthalpy of  $\text{Pt}_3\text{Zr}$  is given as follows:<sup>[37]</sup>

$$\Delta H_f^\phi(\text{Pt}_3\text{Zr}) = \frac{1}{4}E_{\text{Pt}_3\text{Zr}}^\phi - \left[ \frac{3}{4}E_{\text{Pt}}^\phi + \frac{1}{4}E_{\text{Zr}}^\phi \right], \quad (1)$$

where  $E_{\text{Pt}_3\text{Zr}}^\phi$  is the total energy of the  $\text{Pt}_3\text{Zr}$  compound with  $\phi$  structure,  $E_{\text{Pt}}^\phi$  and  $E_{\text{Zr}}^\phi$  are total energies per atom of Pt and Zr with  $\phi$  and  $\phi$  structures, respectively. The calculated values of  $\Delta H_f$  for the cubic structure are in good agreement with other theoretical data. However, our result for hexagonal structure is relatively smaller than those reported in Ref. [25]. We find that the  $\Delta H_f$  of the  $\text{Pt}_3\text{Zr}$  compound in the  $\text{D0}_{24}$  phase is lower than that in the  $L1_2$  phase, which indicates that  $\text{Pt}_3\text{Zr}$  in the hexagonal structure is more stable than that in the cubic structure.

**Table 1.** Calculated equilibrium elastic constants ( $a$ ,  $c$ ), bulk modulus  $B$  and its derivative  $B'$ , and formation enthalpy  $\Delta H_f$  for cubic and hexagonal Pt<sub>3</sub>Zr.

Compound		Crystalline parameters		$B/\text{GPa}$	$B'$	$\Delta H_f/(\text{eV/atm})$
		$a/\text{\AA}$	$c/\text{\AA}$			
Pt <sub>3</sub> Zr in L1 <sub>2</sub>	present GGA	4.046		219.07	4.66	−1.105
	present LDA	3.969		262.25	5.46	−1.140
	experimental <sup>[36]</sup>	4.051				
	other <sup>[5,24–27,38,39]</sup>	4.055 <sup>a</sup> , 4.061 <sup>a</sup> , 3.980 <sup>b</sup>		232 <sup>a</sup> , 230 <sup>a</sup>		−1.100 <sup>a</sup> , −0.98 <sup>a</sup> , −1.03 <sup>a</sup>
Pt <sub>3</sub> Zr in D0 <sub>24</sub>	present GGA	5.723	9.330	226.39	4.54	−1.322
	present LDA	5.618	9.200	265.00	5.00	−1.356
	experimental <sup>[5]</sup>	5.653	9.347 <sup>[5]</sup>			
	other <sup>[25,26,29]</sup>	5.729 <sup>a</sup> , 5.742 <sup>a</sup>	9.364 <sup>a</sup> , 9.398 <sup>a</sup>	226 <sup>a</sup>		−1.108 <sup>a</sup>

<sup>a</sup>Data from the PBE-GGA method. <sup>b</sup>Data from the LDA method.

### 3.2. Elastic properties

Elastic constants can be used to measure material's resistance and mechanical stability under compression. Moreover, elastic constants of materials can offer important information about their mechanical and dynamical behavior. For cubic systems, there are three independent elastic constants  $C_{ij}$ , namely  $C_{11}$ ,  $C_{12}$  and  $C_{44}$ . However, there are five independent elastic constants  $C_{ij}$  for hexagonal structures, namely  $C_{11}$ ,  $C_{12}$ ,  $C_{13}$ ,  $C_{33}$ , and  $C_{55}$ . Necessary mechanical stability criteria for cubic and hexagonal crystal systems are  $C_{11} - C_{12} > 0$ ,  $C_{11} + 2C_{12} > 0$ ,  $C_{44} > 0$  and  $C_{11} > |C_{12}|$ ,  $2C_{13}^2 < C_{33}(C_{11} + C_{12})$ ,  $C_{55} > 0$ , respectively.<sup>[40,41]</sup> The IRelast package contributed by Jamal *et al.*<sup>[42]</sup> has been used to calculate the equilibrium elastic constants of Pt<sub>3</sub>Zr using the GGA and LDA approximations. We use a dense mesh of 165 and 84  $k$ -points in the irreducible Brillouin zone for cubic and hexagonal structures, respectively. The equilibrium calculated values of  $C_{ij}$  for cubic and hexagonal Pt<sub>3</sub>Zr using the GGA and LDA methods are given in Table 2. It is clear that our results coincide very well with the experimental and theoretical data. Moreover, our results satisfy the mechanical stability conditions indicating the stability of the studied compound in cubic and hexagonal structures. It is known that  $C_{11}$  and  $C_{33}$  reflect the unidirectional compression resistance along the principle crystallographic direction while  $C_{44}$  ( $C_{55}$  for hexagonal phase) describes the crystal resistance to the shear strain. It is found that  $C_{11}$  in the cubic (hexagonal) system is 2.5 (5) times higher than  $C_{44}$  ( $C_{55}$ ), signifying that this compound presents a stronger resistance to the unidirectional compression compared to the pure shear deformation.

Elastic properties were investigated using the Voigt–Reuss–Hill (VRH) approximation.<sup>[43]</sup> Hill's shear  $G_H$  and bulk moduli  $B_H$  can be expressed as the average between the Voigt<sup>[44]</sup> and Reuss<sup>[45]</sup> bounds as follows:  $G_H = \frac{1}{2}(G_V + G_R)$ ,  $B_H = \frac{1}{2}(B_V + B_R)$ . For cubic phases,  $G_V$ ,  $B_V$ ,  $G_R$  and  $B_R$  can be written as

$$B_V = B_R = \frac{1}{3}(C_{11} + 2C_{12}), \quad (2)$$

$$G_V = \frac{1}{5}(C_{11} - C_{12} + 3C_{44}), \quad (3)$$

$$G_R = \frac{5(C_{11} - C_{12})C_{44}}{4C_{44} + 3(C_{11} - C_{12})}. \quad (4)$$

For the hexagonal system, the corresponding formulas are as follows:

$$G_V = \frac{1}{30}[M + 12C_{55} + 6(C_{11} - C_{12})], \quad (5)$$

$$B_V = \frac{1}{9}[2(C_{11} + C_{12}) + 4C_{13} + C_{33}], \quad (6)$$

$$G_R = \frac{\frac{5}{4}[C^2 C_{55}(C_{11} - C_{12})]}{[\frac{3}{2}B_V C_{55}(C_{11} - C_{12}) + C^2[C_{55} + \frac{1}{2}(C_{11} - C_{12})]}], \quad (7)$$

$$B_R = \frac{C^2}{M}, \quad (8)$$

where  $C^2 = (C_{11} + C_{12})C_{33} - 2C_{13}^2$  and  $M = C_{11} + 2C_{33} - 4C_{13}$ .

**Table 2.** Calculated elastic constants of Pt<sub>3</sub>Zr (in units of GPa).

Structure		$C_{11}$	$C_{12}$	$C_{13}$	$C_{33}$	$C_{44}$	$C_{55}$
L1 <sub>2</sub>	present GGA	357.38	181.96			139.86	
	present LDA	401.52	206.17			156.65	
	other <sup>[25]</sup>	340 <sup>a</sup>	175 <sup>a</sup>			98 <sup>a</sup> , 119 <sup>a</sup>	
D0 <sub>24</sub>	present GGA	357.19	177.97	154.85	399.22		70.32
	present LDA	416.31	219.57	151.05	448.75		77.21
	other <sup>[25]</sup>	337 <sup>a</sup>	159 <sup>a</sup>	147 <sup>a</sup>	375 <sup>a</sup>		88 <sup>a</sup>

<sup>a</sup> Data from the PBE-GGA method. <sup>b</sup>Data from the LDA method.

The calculated bulk modulus  $B_H$  and shear modulus  $G_H$  of cubic and hexagonal Pt<sub>3</sub>Zr are listed in Table 2. The bulk moduli represent the material resistance to the volume change under pressure, however the shear moduli are measure of resistance to shape change under shear stress. Moreover, these parameters can measure the crystal hardness. Therefore, our results indicate that the Pt<sub>3</sub>Zr has higher hardness in the cubic structure than that in the hexagonal one. The shear modulus values imply that Pt<sub>3</sub>Zr has excellent shear deformation resistance.

Other significant elastic parameters such as Young's modulus  $E$ , Poisson's ratio  $\nu$ , Pugh's index  $G/B$ , machinability index  $B/C_{44}$ , Cauchy pressure  $C_{12} - C_{44}$  ( $C_{12} - C_{55}$  for the hexagonal structure), anisotropic ratio  $A$ , Kleinman parameter  $\xi$ , and Vickers hardness  $H_V$  are investigated for the cubic and hexagonal structures using the GGA and LDA approximations. The calculated elastic properties together with other experimental and theoretical data are given in Table 3. From Table 3, the LDA calculations are larger than those of GGA. We can conclude that the smaller the lattice parameter, the higher

the elastic properties. Young's modulus and Poisson's ratio  $\nu$  are calculated using the following relations:<sup>[46,47]</sup>

$$E = \frac{9B_H G_H}{3B_H + G_H}, \quad (9)$$

$$\nu = \frac{3B - 2G}{6B + 2G}. \quad (10)$$

Young's modulus  $E$ , namely elasticity modulus, is defined as the ratio of the tensile stress to the corresponding tensile strain. It is an important property providing the material stiffness. The calculated Young moduli with the GGA (LDA) method are 300 GPa (335 GPa) for the  $L1_2$  structure and 230 GPa (261 GPa) for the  $D0_{24}$  phase, indicating that  $Pt_3Zr$  has a strong stiffness higher than other<sup>[24]</sup> Pt–Zr alloys. Moreover,  $Pt_3Zr$  in the cubic structure is stiffer than that in the hexagonal structure. Our result for the  $L1_2$  structure coincides well with that obtained by Pan *et al.*<sup>[24,27]</sup> Poisson's ratio, Pugh's index and the Cauchy pressure are good indicators for ductile/brittle nature of materials. Poisson's ratio is smaller than 0.26 for brittle materials, otherwise the material behaves in a ductile manner. Furthermore, Poisson's ratio gives information about the characteristics of the bonding in materials. For covalent materials, Poisson's ratio has a small value ( $\nu = 0.1$ ), whereas for ionic compounds, it has a typical value of 0.25. For metallic materials, the  $\nu$  value is typically 0.33. In our case, the  $\nu$  values for cubic and hexagonal structures are 0.29 and 0.33, respectively, indicating a considerable metallic contribution to intra-atomic bonding for the  $Pt_3Zr$  compound. According to Pugh's index, the material will be brittle (ductile) if the  $B/G$  ratio is smaller (higher) than 1.75. Our calculated  $B/G$  values are above 1.75 for the cubic and hexagonal structures, indicating a ductile character. The mechanability index<sup>[48]</sup>  $B/C_{44}$  ( $C_{55}$  for the hexagonal structure) may be used as a measure of plasticity and a good indicator of lubricating properties.<sup>[49,50]</sup> For the cubic and hexagonal structures, the  $B/C_{44}$  values are 1.72 and 3.29, respectively. This means that  $Pt_3Zr$  is a good lubricant in the hexagonal structure while it has a low lubricating ratio in the cubic structure (compared to gold which has a wonderful lubricating properties of 4.17).<sup>[51]</sup> Moreover, the calculated values of Cauchy pressure are positive, which proves the ductile and metallic behavior of the  $Pt_3Zr$  compound.

The Zener anisotropy factor  $A$  is an elastic parameter used to measure the degree of elastic anisotropy in solids.  $A$

is highly correlated with the possibility to introduce micro-cracks in materials. For completely isotropic materials,  $A$  takes the value of 1, however for anisotropic materials,  $A$  differs from the unity.<sup>[48]</sup> For the cubic structure,  $A$  reads<sup>[52]</sup>

$$A = \frac{2C_{44}}{C_{11} - C_{12}}. \quad (11)$$

However, for the hexagonal structure, there are three anisotropy factors  $A_1$ ,  $A_2$  and  $A_3$  corresponding to three shear planes:  $\{100\}$ ,  $\{010\}$  and  $\{001\}$  between  $\langle 011 \rangle$  and  $\langle 010 \rangle$ ,  $\langle 101 \rangle$  and  $\langle 001 \rangle$ ,  $\langle 110 \rangle$  and  $\langle 010 \rangle$  directions, respectively,<sup>[53–55]</sup>

$$A_1 = A_2 = \frac{2C_{55}}{C_{11} - C_{13}}, \quad (12)$$

$$A_3 = \frac{4C_{55}}{C_{11} + C_{33} - 2C_{13}}. \quad (13)$$

Values of  $A$ ,  $A_1$ ,  $A_2$ , and  $A_3$  differ from 1, indicating the anisotropic character of the cubic and hexagonal structures. The Kleinman parameter  $\xi$  is an important parameter to describe the relative position of cation and anion sub-lattices and the material resistance to bond bending against bond stretching. Here the  $\xi$  parameter can be expressed as<sup>[56]</sup>

$$\xi = \frac{C_{11} + 8C_{12}}{7C_{11} + 2C_{12}}. \quad (14)$$

The  $\xi$  value in the  $L1_2$  structure is found to be very close to that in the  $D0_{24}$  structure. To better define the hardness of our compound, Vickers hardness  $H_v$  is calculated using a theoretical model,<sup>[57–59]</sup>

$$H_v = 0.92 \left( \frac{G}{B} \right)^{1.137} G^{0.708}. \quad (15)$$

The calculated hardness value for the cubic structure is 11.62 GPa (12.44 GPa) using the GGA (LDA) method. The values for the hexagonal structure are 6.99 GPa using the GGA and 6.86 GPa using the LDA, indicating that hardness of cubic  $Pt_3Zr$  is the highest. The calculated  $H_v$  values for  $L1_2$  and  $D0_{24}$  are under the superhardness limit ( $\geq 40$  GPa). There are no experimental or theoretical results available about the mechanability index, anisotropy factor, Kleinman parameter and hardness for comparison.

**Table 3.** Calculated bulk modulus  $B$  (GPa), shear modulus  $G$  (GPa), Young's modulus  $E$  (GPa), Pugh's index  $B/G$ ,  $B/C_{44}$  ratio, Poisson's ratio  $\nu$ , anisotropic parameter  $A$ , Kleinman parameter  $\xi$ , and Vickers hardness  $H_v$  (GPa).

Structure		$B$	$G$	$E$	$B/G$	$B/C_{44}$	$C_{12} - C_{44}$	$\nu$	$A$	$\xi$	$H_v$
$L1_2$	present GGA	240.43	116	300	2.072	1.72	42.10	0.29	0.59	0.632	11.62
	present LDA	271.29	129.62	335.43	2.092	1.73	49.52	0.29	0.60	0.636	12.44
	other <sup>[24,27,39]</sup>	232 <sup>a</sup> , 275 <sup>b</sup>	105 <sup>a</sup> , 113 <sup>a</sup> , 129 <sup>b</sup>	274 <sup>a</sup> , 335 <sup>b</sup>	2.50 <sup>a</sup> , 2.13 <sup>b</sup> , 2.05 <sup>a</sup>		77 <sup>a</sup>	0.29 <sup>a</sup>			
$D0_{24}$	present GGA	232.04	86.13	229.35	2.69	3.29	107.65	0.33	$A_1 = 0.70, A_3 = 0.63$	0.623	6.99
	present LDA	258.14	98.04	261.07	2.63	3.35	142.36	0.33	$A_1 = 0.58$	0.647	7.86
	other <sup>[39]</sup>	280 <sup>a</sup>	106 <sup>a</sup>		2.64 <sup>a</sup>			0.31 <sup>a</sup>	$A_2 = 0.73$		

<sup>a</sup>Data from the PBE-GGA method. <sup>b</sup>Data from the LDA method.



### 3.3. Debye temperature

The Debye temperature  $\theta_D$  is a characteristic parameter of numerous thermal solid properties such as specific heat, thermal conductivity, melting temperature and lattice vibration. Moreover,  $\theta_D$  reflects the binding force between atoms. The higher the  $\theta_D$ , the stronger the covalent bonding. Here  $\theta_D$  can be calculated from the average acoustic velocity as follows:<sup>[60]</sup>

$$\theta_D = \frac{h}{k} \left[ \frac{3n}{4\pi} \left( \frac{N_A \rho}{M} \right) \right]^{1/3} v_m, \quad (16)$$

where  $h$  is Plank's constant,  $k$  Boltzmann's constant,  $N_A$  Avogadro's number,  $n$  the number of atoms per formula unit,  $\rho$  is the density,  $M$  the molecular mass per formula unit, and  $v_m$  the average acoustic velocity expressed as

$$v_m = \left[ \frac{1}{3} \left( \frac{2}{v_s^3} + \frac{1}{v_l^3} \right) \right]^{1/3}, \quad (17)$$

where  $v_s = \left( \frac{3B+4G}{3\rho} \right)^{1/2}$  and  $v_l = (G/\rho)^{1/2}$  are the shear and longitudinal acoustic wave velocities, respectively.<sup>[61,62]</sup>

**Table 4.** Calculated shear, longitudinal and average acoustic velocities (in m/s), i.e.,  $v_s$ ,  $v_l$ , and  $v_m$ , as well as Debye temperature  $\theta_D$  (in K), melting temperature (in K).

Structure		$v_s$	$v_l$	$v_m$	$\theta_D$	$T_m \pm 300$ K
L1 <sub>2</sub>	present GGA	2614.93	4826.08	2917.95	340.90	2665.16
	present LDA	2685.53	4972.83	2998.49	356.10	2926.02
	other <sup>[24,63]</sup>				342 <sup>b</sup>	2552 <sup>a</sup>
D0 <sub>24</sub>	present GGA	2257.23	4539.82	2532.69	295.52	
	present LDA	2342.46	4665.15	2627.15	312.25	
	other <sup>[24]</sup>					2427 <sup>a</sup>

<sup>a</sup>Data from the PBE-GGA method. <sup>b</sup>Data from the LDA method.

The calculated  $v_m$ ,  $v_l$  and  $v_s$  are displayed in Table 4. Acoustic velocities for the cubic structure are the highest, indicating that acoustical wave's propagation in the cubic structure is faster than that in the hexagonal structure. Debye temperature of cubic Pt<sub>3</sub>Zr is the largest. Large values of  $\theta_D$  indicate the strong covalent bond Pt–Zr of the cubic and hexagonal Pt<sub>3</sub>Zr compound. The melting temperature is a significant parameter in engineering science. For the cubic structure, the calculated value of  $T_m$  is 2665  $\pm$  300 K (2926  $\pm$  300 K) using the GGA (LDA) method, which makes Pt<sub>3</sub>Zr promising for high temperature applications.

### 3.4. Density of states

To better understand the structural stability and the bonding characteristics of the Pt<sub>3</sub>Zr compound, total density of states (TDOS) and partial density of states (PDOS) are calculated using the GGA and LDA methods. Figure 3 gives the TDOS and PDOS of the Pt<sub>3</sub>Zr compound in the D0<sub>24</sub> and L1<sub>2</sub> structures with the GGA approximation. The Fermi level is situated at 0 eV. The TDOS histogram of L1<sub>2</sub>-Pt<sub>3</sub>Zr (Fig. 3(a)) illustrates that the energy range from –10 eV to –0.67 eV at the bonding states is dominated by the Pt-5d states. However, in the above range the Fermi level from 0 to 9 eV at the

anti-bonding states is dominated by the hybridization of Pt-5d and Zr-4d states. This result agree very well with those obtained by Pan *et al.*<sup>[24,26,27]</sup> The contribution of Zr-s, p and Pt-s, p in the PDOS of L1<sub>2</sub>-Pt<sub>3</sub>Zr is negligible. Furthermore, the main bonding peak is situated at –3.66 eV and the main anti-bonding peak, coming from a strong hybridization between Pt-d and Zr-d states, is situated in the energy range 0.42–1.1 eV.

It is known that for the hexagonal structure, Pt and Zr atoms occupy two positions (Pt1, Pt2, Zr1 and Zr2). Figure 3(b) illustrates the TDOS and PDOS histograms of D0<sub>24</sub>-Pt<sub>3</sub>Zr. It shows that the energy range from –9.25 eV to –0.21 eV is dominated by Pt1-5d and Pt2-5d states while the energy range from 0.70 eV to 9.28 eV is dominated by the hybridization of Pt1-d, Pt2-d, Zr1-d, and Zr2-d states. Moreover, the PDOS curves show that the orbital  $d$  of Zr1 and Zr2 atoms split into three levels:  $d_z^2$ ,  $(d_{xy}, d_x^2 - d_y^2)$  and  $(d_{xz} - d_{yz})$ ; while Pt1-d and Pt2-d orbitals into five levels:  $d_z^2$ ,  $d_x^2 d_y^2$ ,  $d_{xy}$ ,  $d_{xz}$ , and  $d_{yz}$ .

Figures 3 illustrates the existence of a deep-valley-shaped pseudo gap separating the bonding and anti-bonding states. The pseudo gap is formed from the large hybridization between Zr-4d states and Pt-5d states. The existence of the pseudo gap reflects a strong metallic character of the Pt<sub>3</sub>Zr compound. Otherwise, The Fermi level is on the anti-bonding side for the cubic structure and exactly on the pseudo gap for the hexagonal system, indicating that D0<sub>24</sub>-Pt<sub>3</sub>Zr is predicted to be more stable than the L1<sub>2</sub>-Pt<sub>3</sub>Zr compound. This result is similar to that obtained by Popoola *et al.*<sup>[39,63]</sup> Furthermore, the total density of states at Fermi level,  $N(E_F)$ , reflects the material electronic conductivity. The values of  $N(E_F)$  of cubic and hexagonal Pt<sub>3</sub>Zr are listed in Table 5. It is shown that  $N(E_F)$  of D0<sub>24</sub>-Pt<sub>3</sub>Zr (0.52 states/eV) is lower than that of L1<sub>2</sub>-Pt<sub>3</sub>Zr (0.55 states/eV), indicating that the Pt<sub>3</sub>Zr hexagonal structure is slightly more stable than the cubic structure. Moreover, we can deduce that electrical conductivity in the cubic structure is better than that in the hexagonal structure.

Furthermore,  $N(E_F)$  is correlated to the electronic specific heat as follows:

$$\gamma = \frac{1}{3} \pi^2 k_B^2 N(E_F), \quad (18)$$

where  $k_B$  is the Boltzmann constant. At low temperature, the electronic specific heat has a large contribution in the material heat capacity. Table 5 regroups the calculated values of  $\gamma$  for cubic and hexagonal system. It is clear that  $\gamma$  of L1<sub>2</sub>-Pt<sub>3</sub>Zr is higher than that of D0<sub>24</sub>-Pt<sub>3</sub>Zr, indicating that the heat capacity of cubic structure is the highest. The values of DOS ( $N_{\min}$ ) in the minimum of pseudogap of L1<sub>2</sub>-Pt<sub>3</sub>Zr (0.01 states/eV) is smaller than that of D0<sub>24</sub>-Pt<sub>3</sub>Zr (0.47 states/eV), where this minimum is situated at  $E(N_{\min}) = -0.34$  eV and –0.08 eV for the cubic and hexagonal structures, respectively. The calculated values of  $N_{\min}$  and  $E(N_{\min})$  are listed in Table 3.

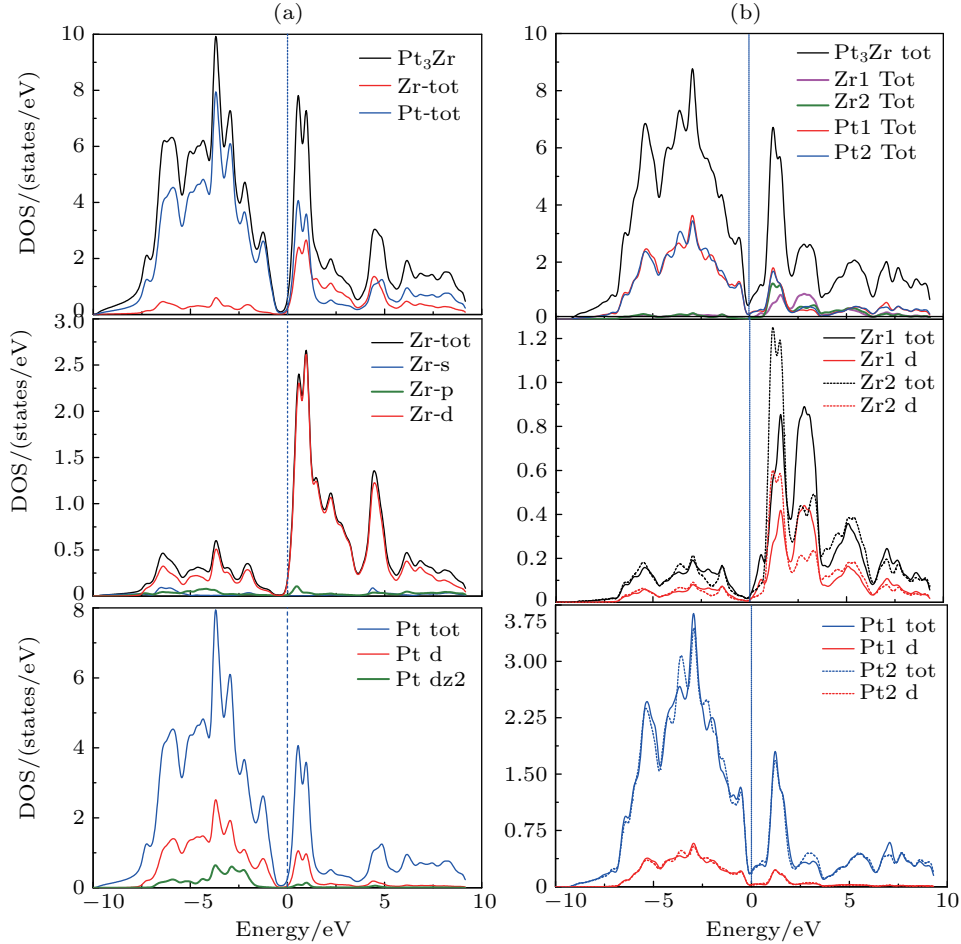


Fig. 3. Total and partial densities of states of  $\text{Pt}_3\text{Zr}$ : (a)  $\text{L1}_2$  structure, (b)  $\text{D0}_{24}$  structure.

Table 5. Total and partial density of states at Fermi level ( $N(E_F)$ ), minimum of DOS ( $N_{\min}$ ), energies at  $N_{\min}$  ( $E(N_{\min})$ ), number of bonding electrons ( $n_b$ ) and electronic specific heat ( $\gamma$ ) of cubic and hexagonal  $\text{Pt}_3\text{Zr}$ .

		$N(E_F)/(\text{states/eV})$	$N_{\min}/(\text{states/eV})$	$E(N_{\min})/\text{eV}$	Elect specific heat $\gamma/\text{mJ}\cdot\text{mol}^{-1}\cdot\text{K}^{-2}$	$n_b$
$\text{L1}_2$	Our GGA	$\text{Pt}_3\text{Zr}$ : 0.55	$\text{Pt}_3\text{Zr}$ : 0.1	−0.34	1,30	7.26
		Pt: 0.25	Pt: 0.06			
		Zr: 0.16	Zr: 0.02			
$\text{D0}_{24}$	Our GGA	$\text{Pt}_3\text{Zr}$ : 0.52	$\text{Pt}_3\text{Zr}$ : 0.47	−0.08	1.23	5.63
		Pt: 0.18	Pt: 0.16			
		Zr: 0.03	Zr: 0.02			

To further elucidate the bonding characteristics of the  $\text{Pt}_3\text{Zr}$  compound, the numbers of bonding electrons per atom for cubic and hexagonal  $\text{Pt}_3\text{Zr}$ ,  $n_b$ , have been calculated. Table 5 illustrates that the  $n_b$  values for  $\text{L1}_2\text{-Pt}_3\text{Zr}$  and  $\text{D0}_{24}\text{-Pt}_3\text{Zr}$  are 7.26 and 5.63, respectively.

### 3.5. Optical properties

Optical properties of materials permit to understand their nature and describe their response to the electromagnetic radiations. These properties are strongly related to the electronic transition between occupied and unoccupied states. Study of materials optical nature provides good insight for their usage in optoelectronic devices. The complex dielectric function  $\epsilon(\omega)$  is known to determine the material response to the electromagnetic field and consists of two parts:  $\epsilon(\omega) =$

$\epsilon_1(\omega) + i\epsilon_2(\omega)$ . The imaginary part  $\epsilon_2(\omega)$  describes the material's absorption behavior and related to the electronic band structure as follows:<sup>[64–67]</sup>

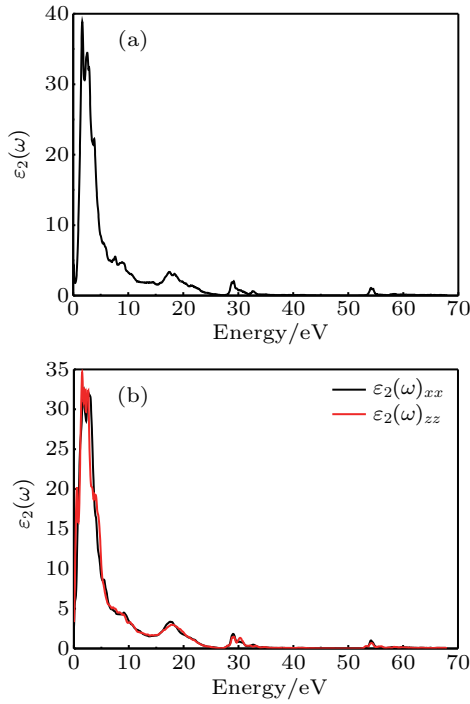
$$\epsilon_2(\omega) = \frac{4\pi^2 e^2}{m^2 \omega^2} \sum_{i,j} \int |\langle i|M|j \rangle|^2 f_i(1-f_j) \times \delta(E_f - E_i - \hbar\omega) d^3k, \quad (19)$$

where  $M$  is the dipole matrix,  $i$  and  $j$  are the initial and final states respectively,  $f_i$  is the Fermi distribution function for the  $i^{\text{th}}$  state,  $E_i$  is the energy of electron in the  $i^{\text{th}}$  state with wave vector  $k$ , and  $\omega$  denotes the frequency of the incident wave. The real part  $\epsilon_1(\omega)$  of the dielectric function gives the information about the polarizability of the material and can be calculated from the imaginary part using the Kramers–Kronig

relation:<sup>[67,68]</sup>

$$\varepsilon_1(\omega) = 1 + \frac{2}{\pi} P \int_0^\infty \frac{\omega' \varepsilon_2(\omega')}{\omega'^2 - \omega^2} d\omega', \quad (20)$$

where  $P$  stands for the principal value of the integral. There are two contributions to the dielectric function: interband transitions describing transitions between valence and conduction bands and intraband transitions describing transitions occurring inside the valence or conduction band.



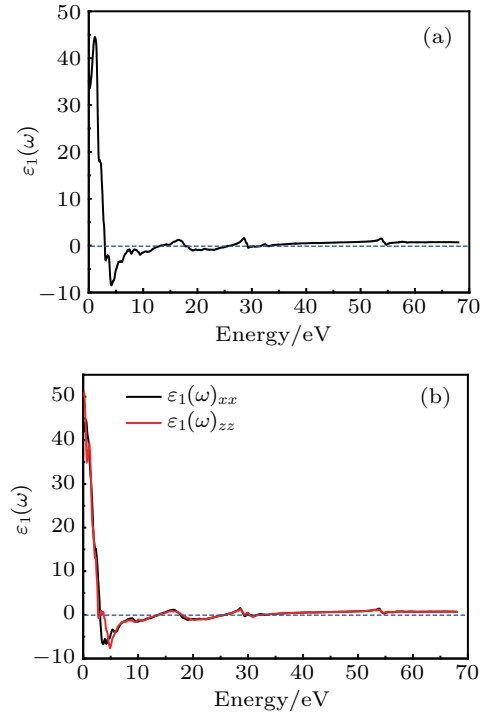
**Fig. 4.** Imaginary part of the dielectric function versus energy for the (a) cubic and (b) hexagonal  $\text{Pt}_3\text{Zr}$  intermetallic compound with the PBE-GGA method.

Optical properties of the  $\text{Pt}_3\text{Zr}$  intermetallic compound have been calculated using ab-initio calculations implemented in the wien2k code with the GGA exchange-correlation method for the cubic and hexagonal structures. To calculate the dielectric function, a dense  $k$ -mesh (365  $k$ -points) in the irreducible Brillouin zone has been used. This study has been carried out for a large range of energy (0–70 eV). For the hexagonal structure,  $\varepsilon(\omega)$  have two independent components:  $\varepsilon_{xx}(\omega)$  corresponding to a parallel phonon polarization to  $c$ -axis and  $\varepsilon_{zz}(\omega)$  corresponding to a perpendicular light polarization. Figures 4(a) and 4(b) illustrate the  $\varepsilon_2(\omega)$  spectra of  $\text{Pt}_3\text{Zr}$  as a function of photon energy for the cubic and hexagonal structures, respectively. We show that the threshold energy is 0 eV for  $\text{L}_{12}\text{-Pt}_3\text{Zr}$  and  $\text{D}_{024}\text{-Pt}_3\text{Zr}$ . For the cubic system,  $\varepsilon_2(\omega)$  exhibits seven peaks located at 1.61 eV, 2.61 eV, 7.70 eV, 17.5 eV, 29.10 eV and 54.11 eV, which indicate the high phonon absorption in the energy values. Obviously,  $\varepsilon_2(\omega)$  becomes zero in the energy ranges of 26.38–27.80 eV, 35.56–53.32 eV, and >62 eV, indicating that the cubic  $\text{Pt}_3\text{Zr}$  becomes transparent in these energy ranges. For the

hexagonal structure (Fig. 4(b)),  $\varepsilon_2(\omega)_{xx}$  and  $\varepsilon_2(\omega)_{zz}$  also exhibit seven peaks with a considerable anisotropy in the range 0–10 eV.

Moreover, the imaginary part reflects the electronic structure of the material. At low energies (0–10 eV), the imaginary part is characterized by considerable intraband transitions of free electrons, where the density of states of Pt-5d is dominant. However, the interband behavior is dominant in high energy area (< 25 eV) with a transition from Pt-5d states of valence band below the Fermi level to Zr-4d states of conduction band above the Fermi level.

The real part of the dielectric function  $\varepsilon_1(\omega)$  is displayed in Fig. 5. For the cubic system (Fig. 5(a)), the static value  $\varepsilon_1(\omega)$  at 0 eV is 35.79. From this value,  $\varepsilon_1(\omega)$  starts increasing and reaches its maximum of 44.28 at 1.11 eV (1117 nm) in infrared (IR) region, then it decreases and becomes zero at 2.85 eV (435 nm). For the ranges 2.98–12.88 eV and 18.32–25.41 eV,  $\varepsilon_1(\omega)$  takes negative values. The  $\varepsilon_1(\omega)$  spectra of the hexagonal  $\text{Pt}_3\text{Zr}$  is illustrated in Fig. 5(b). We show that the static constant value is 44.27 and 50.6 for  $\varepsilon_2(0)_{xx}$  and  $\varepsilon_2(0)_{zz}$ , respectively. The maximum values of  $\varepsilon_1(\omega)_{xx}$  and  $\varepsilon_1(\omega)_{zz}$  appear at 0.58 eV (2137 nm) and 0.11 eV (11271 nm), respectively. Moreover,  $\varepsilon_1(\omega)_{xx}$  becomes negative in the energy ranges 3.04–13.48 eV and 17.70–25.45 eV. In the energy ranges 3.71–13.48 eV and 18.05–25.45 eV,  $\varepsilon_1(\omega)_{zz}$  takes negative values. We observe a considerable anisotropic behavior in the region 0–10 eV.



**Fig. 5.** Real part of dielectric function versus energy of the (a) cubic and (b) hexagonal  $\text{Pt}_3\text{Zr}$  intermetallic compound with the PBE-GGA method.

Other optical parameters such as absorption coefficient  $\alpha(\omega)$ , refractive index  $n(\omega)$ , energy loss function  $L(\omega)$ , reflectivity  $R(\omega)$  and optical conductivity  $\sigma(\omega)$  can be calcu-

lated by knowing  $\varepsilon_1(\omega)$  and  $\varepsilon_2(\omega)$  as follows:<sup>[69,70]</sup>

$$\alpha(\omega) = \frac{2\pi\omega}{c} \sqrt{\frac{|\varepsilon| - \varepsilon_1(\omega)}{2}}, \quad (21)$$

$$n(\omega) = \left[ \frac{\varepsilon_1^2(\omega) + \varepsilon_2^2(\omega) + \varepsilon_1(\omega)}{2} \right]^{1/2}, \quad (22)$$

$$L(\omega) = \frac{\varepsilon_2(\omega)}{[\varepsilon_1^2(\omega) + \varepsilon_2^2(\omega)]}, \quad (23)$$

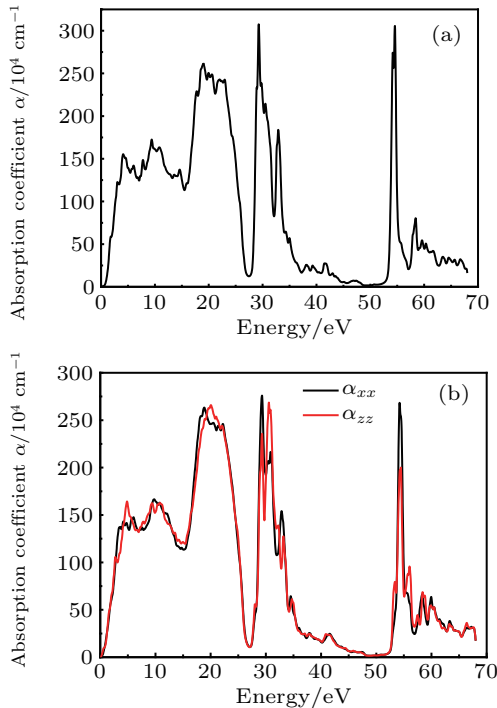
$$R(\omega) = \frac{[n(\omega) - 1]^2 + k(\omega)^2}{[n(\omega) + 1]^2 + k(\omega)^2}, \quad (24)$$

$$\text{Re}[\sigma(\omega)] = \frac{\omega}{4\pi} \varepsilon_2(\omega), \quad (25)$$

where  $K(\omega)$  is the extinction coefficient given by

$$K(\omega) = \left[ \frac{\varepsilon_1^2(\omega) + \varepsilon_2^2(\omega) - \varepsilon_1(\omega)}{2} \right]^{1/2}. \quad (26)$$

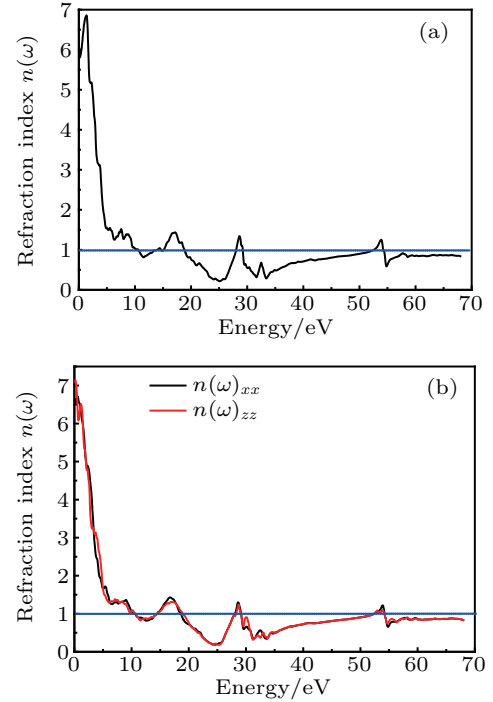
The absorption coefficient is an important optical parameter related to light intensity variation when light passes through the material. Here  $\alpha(\omega)$  is proportional to the imaginary part of the dielectric function. Peaks and valleys in the absorption spectra are corresponding to the possible transition between states from the valence band to the conduct band. Figure 6 illustrates the absorption curves of  $\text{Pt}_3\text{Zr}$  for the cubic and hexagonal structures. For the cubic system (Fig. 5(a)), the maximum absorption occurs in the ultraviolet (UV) region at 29.29 eV (42.32 nm) with a high absorption power of  $308.1 \times 10^4 \text{ cm}^{-1}$ . For the hexagonal phase (Fig. 5(b)), we show an anisotropic behavior in the energy ranges 2.6–22.60 eV, 28.74–49.90 eV and 53–70 eV. The maximum absorptions for  $\alpha(\omega)_{xx}$  and  $\alpha(\omega)_{zz}$  are 29.25 eV (42.38 nm) and 30.61 eV (40.50 nm), respectively, in the UV region.



**Fig. 6.** Absorption coefficient of the (a) cubic and (b) hexagonal  $\text{Pt}_3\text{Zr}$  intermetallic compound as a function of photon energy with the PBE-GGA method.

The refractive index  $n(\omega)$  (displayed in Fig. 7) is a significant physical parameter corresponding to the measurement of the phase velocity and the attenuation of electromagnetic wave in a medium. At  $\omega = 0$ , the static refractive index  $n(0)$  can be determined by<sup>[71]</sup>  $n(0) = [\varepsilon(0)]^{1/2}$ . For  $\text{L1}_2\text{-Pt}_3\text{Zr}$ , the refractive index increases with lower energies (0.1–1.35 eV) and attains a maximum value of 6.86 at 1.35 eV (918.40 nm) in IR region, while it exhibits decreasing tendency for higher energy values. Here  $n(\omega)$  takes the values less than unity for energy ranges: 10.69–13.40 eV, 18.84–28 eV, 30–52.40 eV and above 54.23 eV. Furthermore, the obtained value of  $n(0)$  is 6.08.

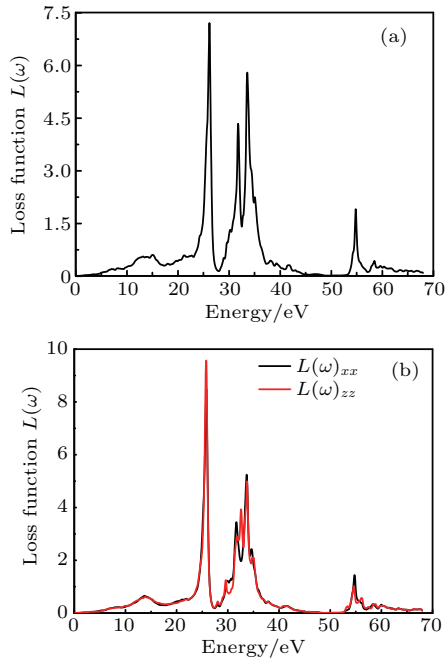
For  $\text{D0}_{24}\text{-Pt}_3\text{Zr}$ , the maximum values of  $n(\omega)_{xx}$  and  $n(\omega)_{zz}$  are 7.15 and 6.73 given at 0.49 eV (2530.28 nm) and 0.10 eV (12398.42 nm) in IR region, respectively;  $n(0)_{xx}$  and  $n(0)_{zz}$  are 6.63 and 7.08, respectively. Moreover, the energy ranges corresponding to refractive index values less than 1 are 10.63–14.49 eV,  $\sim 18.70$ – $\sim 28$  eV, 29.13–52.5 eV and above 54 eV.



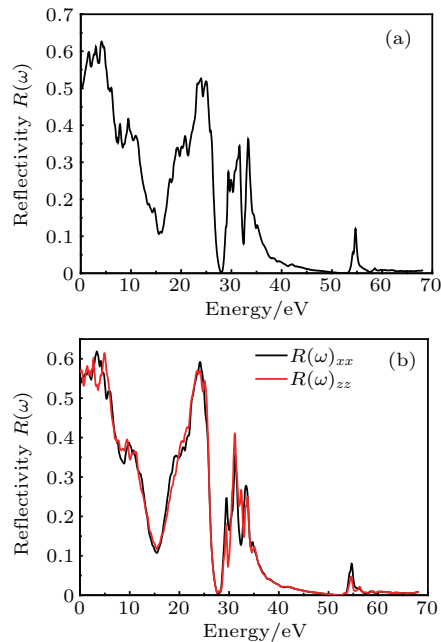
**Fig. 7.** Refractive index of the (a) cubic and (b) hexagonal  $\text{Pt}_3\text{Zr}$  intermetallic compound as a function of photon energy with the PBE-GGA method.

The electron energy loss function is shown in Fig. 8. This important optical parameter is proportional to the energy, in a unit of length, of a fast electron transverse in a material. The main peak in the loss function spectra is known as the plasmon peak, corresponding to the plasma resonance. The maximum values of  $L(\omega)$  is given in UV region at 26.20 eV ( $6.33 \times 10^4 \text{ Hz}$ ) for the cubic structure. However, the resonant energy loss for the hexagonal system is seen at 25.78 eV ( $6.23 \times 10^{15} \text{ Hz}$ ) in UV region. The resonant energy indicates the transition energy from metallic to dielectric properties (starting energy of interband transitions).





**Fig. 8.** Loss function of the (a) cubic and (b) hexagonal  $\text{Pt}_3\text{Zr}$  intermetallic compound as a function of photon energy with the PBE-GGA method.

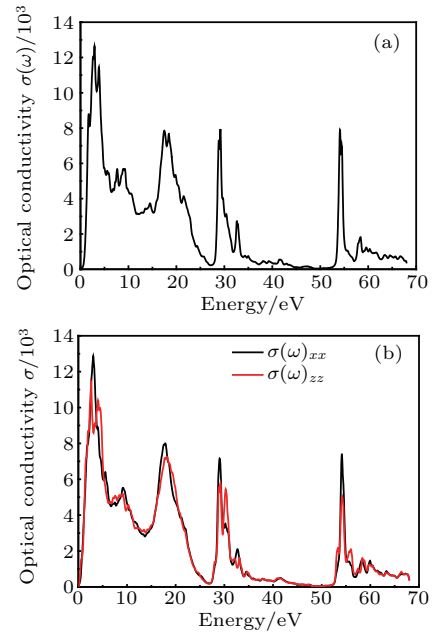


**Fig. 9.** Reflectivity of the (a) cubic and (b) hexagonal  $\text{Pt}_3\text{Zr}$  intermetallic compound as a function of photon energy with the PBE-GGA method.

The optical reflectivity  $R(\omega)$  is the ratio between the reflected wave energy to the incident wave energy.  $R(\omega)$  spectra of  $\text{Pt}_3\text{Zr}$  are displayed in Fig. 9. For the cubic structure, the maximum value of  $R(\omega)$  is about 0.62, which occurs at 4.22 eV (293.80 nm) in UV region. Reflectivity becomes zero at 27.92 eV (44.40 nm) and in the region from 51 eV to 53 eV (24.31–23.39 nm), indicating that the material becomes transparent in these energies values. For the hexagonal structure, we observe an anisotropic structure. The main peak of  $R(\omega)_{xx}$  is obtained at 3.41 eV (363.6 nm) with a reflectivity of 0.61. The same reflectivity value for  $R(\omega)_{zz}$  occurs at 4.97 eV

(249.46 nm).  $R(\omega)_{xx}$  and  $R(\omega)_{zz}$  tend to zero at 27.72 eV (44.72 nm). We can conclude that  $\text{Pt}_3\text{Zr}$  with a strong reflectivity (of 60%) in UV region can be considered as a promising material for coatings in this range.

Plots of the optical conductivity versus energy are shown in Fig. 10. It is shown that optical conductivity starts from zero, indicating that  $\text{Pt}_3\text{Zr}$  has no band gap. For the  $L1_2$  system, the highest peak is obtained at 2.93 eV (423.15 nm) with a magnitude of  $12608.09 \Omega^{-1}\cdot\text{cm}^{-1}$ . For the  $\text{D0}_{24}$  structure, the maximum photoconductivity is  $12883.24 \Omega^{-1}\cdot\text{cm}^{-1}$  and  $11410.40 \Omega^{-1}\cdot\text{cm}^{-1}$  for  $\sigma(\omega)_{xx}$  and  $\sigma(\omega)_{zz}$ , respectively, obtained at 3.04 eV (407.84 nm) and 2.65 eV (467.86 nm) energies.



**Fig. 10.** Conductivity of the (a) cubic and (b) hexagonal  $\text{Pt}_3\text{Zr}$  intermetallic compound as a function of photon energy with the PBE-GGA method.

Furthermore, intraband transitions of free electrons at low photon energies correspond to the large values of the optical reflectivity, absorption coefficient and photoconductivity. When  $\epsilon_2(\omega)$  attains a minimum, optical properties come from Pt-5d states with intraband transitions to interband transitions of Pt-5d states below the Fermi level to Zr-4d states at the Fermi level. This indicates the optical properties for transitions of metallic-to-dielectric behavior. Unfortunately, there are no experimental or theoretical data available in the literature for the optical properties of the  $\text{Pt}_3\text{Zr}$  compound for comparison.

#### 4. Conclusion

In summary, we have investigated structural, elastic, electronic and optical properties of the  $\text{Pt}_3\text{Zr}$  intermetallic compound in cubic and hexagonal structures with the FP-LAPW method. The results predict that the hexagonal phase is more stable than the cubic phase. The calculated elastic constants illustrate the mechanical stability of our compound. Values

of Young's modulus indicate that cubic Pt<sub>3</sub>Zr is much stiffer than hexagonal Pt<sub>3</sub>Zr. Calculated bulk modulus, shear modulus and Vickers Hardness show that hexagonal Pt<sub>3</sub>Zr has the highest hardness. Poisson's ratio reveals the metallic bonding behavior of cubic and hexagonal Pt<sub>3</sub>Zr. Pugh's index and Cauchy pressure indicate the ductile nature of our material. Our compound exhibits an anisotropic character. Cubic Pt<sub>3</sub>Zr has the largest Debye and melting temperature, indicating the strong covalent nature of this compound. Computed density of states shows that hexagonal Pt<sub>3</sub>Zr electronically is more stable than cubic Pt<sub>3</sub>Zr. Considering  $N(E_F)$  and electronic specific heat values, we can deduce that electrical conductivity, melting temperature and heat capacity in the cubic structure are better than those in the hexagonal structure. Optical properties of the Pt<sub>3</sub>Zr compound have been investigated using the real and imaginary parts of dielectric function. Maximum absorption and reflectivity are obtained in UV region for cubic and hexagonal Pt<sub>3</sub>Zr. The refractive index of hexagonal Pt<sub>3</sub>Zr (in IR region) is the highest. The electron energy loss function has also been computed. Optical conductivity  $\sigma(\omega)$  spectrum illustrates that highest values of  $\sigma(\omega)$  are obtained for the hexagonal structure according to the  $zz$  direction. Moreover, intra and inter-band transitions have been discussed. We can conclude that our study is valuable for the future applications of the Pt<sub>3</sub>Zr intermetallic compound as a structural material.

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